



# Hamlet of Kimmirut Master Drainage Plan



### PRESENTED TO

# Department of Community and Government Services (CGS) Government of Nunavut

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# **ACRONYMS & ABBREVIATIONS**

| Acronyms/Abbreviations | Definition                        |
|------------------------|-----------------------------------|
| DEM                    | Digital Elevation Model           |
| GIS                    | Geographic Information System     |
| GPS                    | Global Positioning System         |
| SWMM                   | Stormwater Management Model       |
| AES                    | Atmospheric Environmental Service |
| GN                     | Government of Nunavut             |





#### LIMITATIONS OF REPORT

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# **1.0 INTRODUCTION**

Tetra Tech Canada Inc. (Tetra Tech) was retained by the Department of Community and Government Services (CGS), Government of Nunavut to develop a Master Drainage Plan (MDP) for the Hamlet of Kimmirut (Kimmirut). CGS and Kimmirut require that an MDP be conducted in Kimmirut, for both the existing town site and planned future subdivisions identified in the Community Plan.

The Terms of Reference (ToR) developed by CGS confirmed the fact that Kimmirut has in-force a Community Plan (By-law No. 127) and a Zoning By-law (By-law No. 128). These by-laws are due for a statutory five-year review sometime in 2019 or 2020. To make sure the community plans are developed in harmony with the local site drainage limitations, it was recommended that a complete review of the local drainage system be completed. In addition to a detailed review of the community plans and its impacts on the exiting stormwater system, CGS identified the need to review and evaluate the conditions of the existing drainage system. Based on anecdotal information and details provided by CGS, a number of pre-existing drainage issues are present within the existing townsite.

The 2016 census revealed the population of Kimmirut to be 389 persons (which is a decline from 455 persons in the 2011 census), distributed in 139 dwellings. Development of the community of Kimmirut is restricted by the topography of the land; as a result, any of the proposed subdivisions need to be constructed away from the core area of the community. In order to ensure that the Hamlet of Kimmirut has sufficient and suitable developable land to accommodate population growth forecast in the Community Plan, it is necessary that a qualified team of professionals complete a detailed drainage review of the potential development sites.

The drainage study has been staged in two phases. Tetra Tech's previous memo dated March 21, 2019 concluded the first phase which encompassed a review of all available background material, development of inputs to a hydrologic model, and development of the preliminary drainage recommendations.

The second phase of this project included the following tasks:

- Complete a site visit to Kimmirut by a team of water resource engineers to identify, assess, and document all drainage infrastructure and known drainage issues;
- Develop an inventory of existing drainage issues;
- Update the stormwater model to assess the drainage system for existing and proposed development conditions; and
- Complete the Kimmirut Master Drainage Plan.



# 2.0 REVIEW OF BACKGROUND INFORMATION

Tetra Tech collected, compiled and processed all information related to the drainage system of the Hamlet of Kimmirut, made available by officials from the Government of Nunavut and the Hamlet, and from publicly available reports and data.

The initial background review process provided Tetra Tech with an understanding the terrain, climate, long-term land-use plans, and known drainage issues in Kimmirut.

Reviewed background data has included the following:

- 2017 Satellite Imagery (.tif);
- 2017 Digital Elevation Models (Bare earth and surface models available in .tif and .asc formats);
- 2017 Building footprint, infrastructure, and transportation vector datasets (AutoCAD .dwg and ESRI File Geodatabase or Shapefile formats);
- 2017 Hydrology (water bodies and watercourses) vector datasets (AutoCAD .dwg and ESRI File Geodatabase and Shapefile formats);
- 2017 Contours vector datasets (AutoCAD .dwg and ESRI File Geodatabase and Shapefile formats);
- 2014 Community Plan and Community Plan By-law;
- 3vGeomatics 2016 ground movement report entitled: Nunavut Terrain Analysis Final Report 2015-16;
- Tetra Tech EBA 2015 geotechnical memo entitled: Desktop Geotechnical Evaluation for Duplex, Kimmirut, NU;
- National Topographic Survey (NTS) 1:50,000 Topography Map of Kimmirut;
- Google Earth 2016 Satellite Imagery;
- Historical climate data for Kimmirut, Cape Dorset, and Iqaluit Airports, monitored and made available by Environment Canada; and
- Online data sources (CBC news).

Additional anecdotal background information was collected through informal discussions with Hamlet staff and local residents during the 2019 field visit.

## 2.1 Community Plan, Population and Expansion Plans (Land Use)

The Government of Nunavut CGS division maintain and regularly update community plan maps for each community within the Territory. The purpose of these community plans are to outline Council's policies for managing the physical development of each Hamlet for the next 20 years. The community plan for the Hamlet of Kimmirut was updated in 2014 (included as Appendix B).

The community plan includes existing land parcels as well as proposed parcels of land allocated for future community growth. This combination of existing and proposed development forms the scope of our Master Drainage Plan, which aims to provide feedback not only on how to improve the existing drainage system, but also prescribe how the drainage features of the future area should be designed.



Based on discussions with CGS staff we understand that multiple changes have been made to the plan since its 2014 publication. These changes primarily relate to the location of lots for future development and are reflected in the 2019 update of the community plan. The results of this community drainage study should be incorporated within the same 2019 community plan update.

Through the development of this report, Tetra Tech has identified sections of the community plan which should not be developed. Instead, Tetra Tech is recommending that CGS consider revising the community plan so to develop a plan which is less prone to drainage issues. For consideration, Appendix B includes a revised community plan.

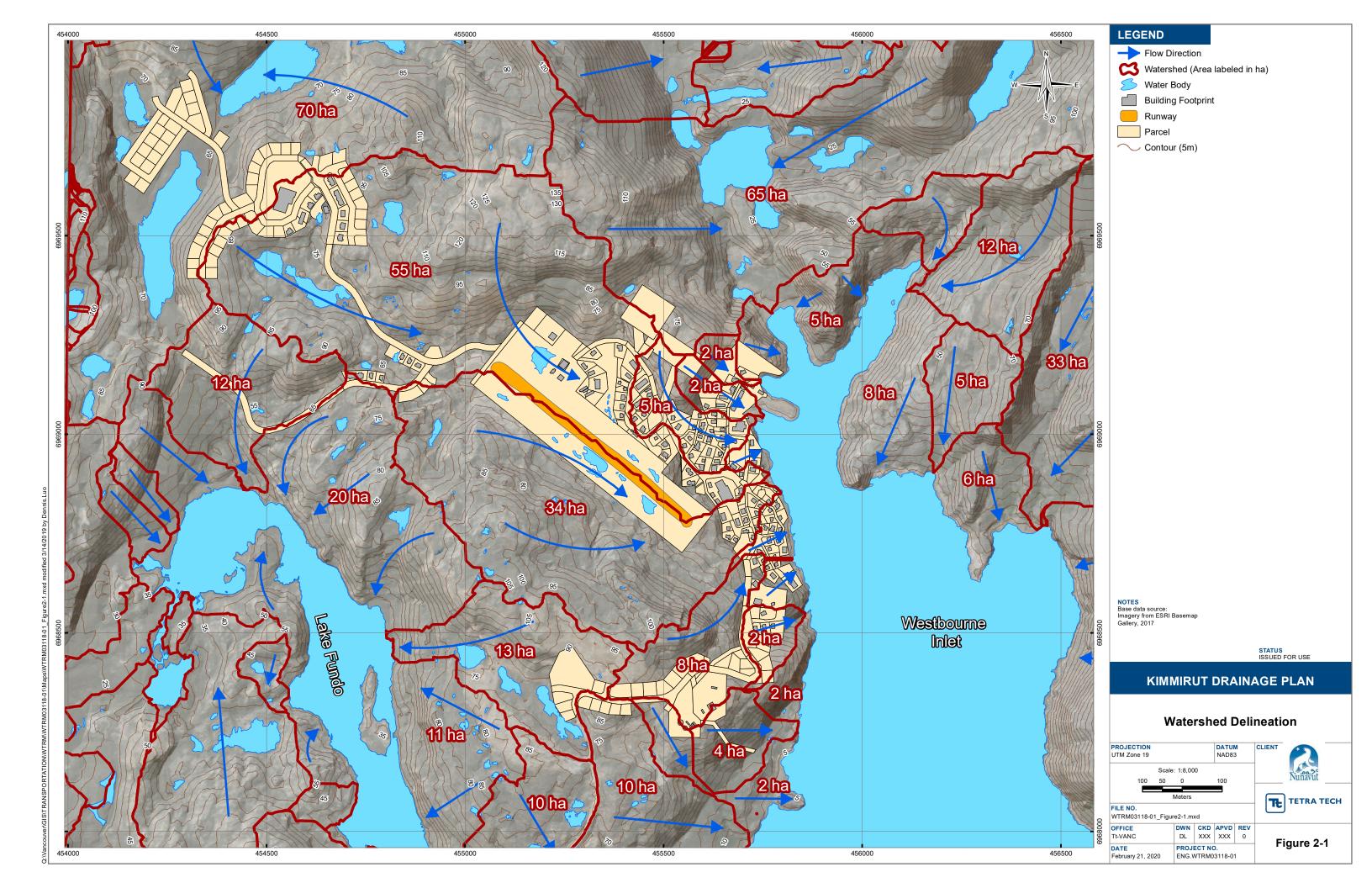
# 2.2 Terrain

The Hamlet of Kimmirut is founded upon undulating bedrock on the southern coast of Baffin Island. The community itself is situated on the shores of Glasgow Inlet, set in a valley created by bedrock ridges rising over 100 metres in elevation to the northwest and southwest.

## 2.2.1 Topography and Watershed Delineation

A Digital Elevation Model (DEM) of the Kimmirut area was developed to represent the topography of the project area. The DEM was derived from aerial photographs used to extract elevation information through a technique called photogrammetry. The use of measurements from photographs is of sufficient accuracy for use within a drainage planning exercise.

Tetra Tech has reviewed this DEM in conjunction with NTS 1:50,000 topography maps of the area and has performed a watershed delineation analysis to identify drainage patterns in the Kimmirut area. The existing drainage patterns are presented in Figure 2-1, and were confirmed during the 2019 freshet field visit. Note that several paths are impacted by the presence of other surficial obstructions such as buildings and conveyance systems such as culverts and ditches.





## 2.2.2 Surficial and Subsurface Geology

Based on investigation conducted by Tetra Tech, bedrock is exposed throughout the Kimmirut region. The surficial vegetation in the area is sparse and treeless. The region's terrain is characterized as tundra, and the soil is locked in permafrost apart from a thin surficial layer that thaws during the summer months (Kikkert, 2019). The area is assumed to have very low permeability, producing low infiltration rates and high runoff rates.

## 2.2.3 Land Stability

3VGeomatics completed a terrain analysis of the Kimmirut area in 2015 using Synthetic Aperture Radar to determine landmasses prone to movement. The project was undertaken in order to identify areas in the Kimmirut area suitable for development.

The results of their analysis concluded that displacement is expected to occur predominantly on steep sided slopes and scattered small pockets located in flatter areas. Almost all existing buildings are located on suitable terrain with little expected ground movement; however, we note that the proposed expansion of Kimmirut, as outlined in the 2014 Community Plan, does overlap portions of terrain which 3VGeomatics has flagged as being unsuitable or only marginally suitable for development. Further site inspection of these lots will need to be conducted to determine if they will be developed. Tetra Tech recommends that the 2019/2020 update of the Kimmirut Community Plan will include a revised layout to account for the recommendations proposed by 3VGeomatics.

## 2.3 Climate

The climate in Kimmirut is typical of the sub-arctic region, characterized by low precipitation and winter temperatures predominating for eight months of the year (Beckstead, G. & L.B. Smith 1985). Using data from Atlas Canada (The Prairie Climate Centre, 2019), Figure 2-2 shows the climate normals for the period between 1976 and 2005. The average daily maximum, mean, and minimum temperatures in February are -21.5°C, -25.1°C, and -28.8°C respectively. The same temperatures in July are 10.6°C, 6.9°C, and 3.2°C respectively. The annual mean daily temperature is -8.8°C. Extreme maximum and minimum temperatures are 25.5°C and -43.0°C respectively. The annual average warmest maximum temperature is 17.4°C and the annual average coolest minimum temperature is -39.0°C. Total annual precipitation is 422 mm (The Prairie Climate Centre, 2019). The maximum daily rainfall on record is 35 mm, which occurred on August 16, 2004.





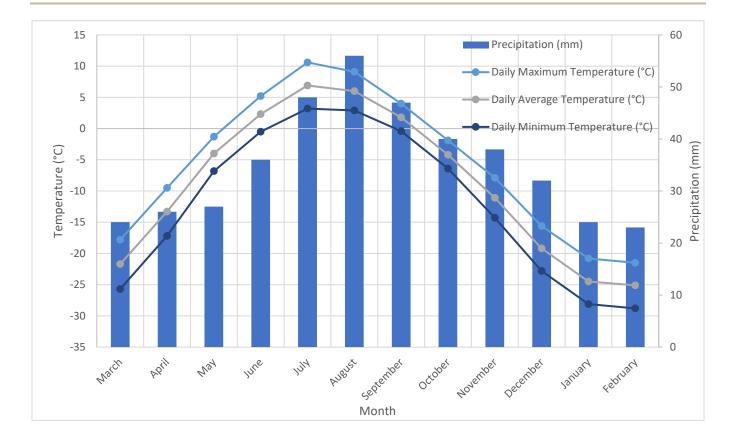


Figure 2-2: Average Temperature and Precipitation (1976-2005). Kimmirut

## 2.3.1 Climate Change

Due to limited climate change research available for the region covering the Hamlet of Kimmirut, relevant findings from Lewis and Miller's "*Climate Change Adaptation Action Plan for Iqaluit*" (2010) was utilized for this section of the report. Lewis and Miller (2010) presented a summary of perceived sensitivities to climate change in Iqaluit, including the following:

## Infrastructure

- 1. Damage to infrastructure is expected to increase due to increases in climate variability and extreme events.
- 2. A decrease in the permafrost layer was identified as the most significant climate-related concern for infrastructure.
- 3. The following may be particularly at risk: buildings with shallow foundations; buildings, roads and buried pipes along steep south facing slopes and/or in areas of high snow accumulation; any building or road in areas of poor drainage where water may pool.
- 4. The following infrastructure may be vulnerable to other climate change impacts: buildings or piping in poor condition due to age, absence of regular maintenance, outdated design or over-extended use; infrastructure located along the coast which may be susceptible to damage from flooding or storm surges; the drainage system which may be impacted by changes in precipitation; and the City's water supply.



- 5. All new municipal infrastructure shall be designed and constructed to specifications that withstand projected changes in climate over their expected design life and meet sustainable development standards.
- 6. City outfalls should be designed to fall outside the range in tidal variability.

### Buildings

- 1. With an increase of the active layer of permafrost, many existing building foundations could experience structural damage.
- 2. With a change in weather patterns such as extreme storm events, more extreme temperature variations, increased humidity in snow and more rain, buildings will be more susceptible to weathering and moisture damage.
- 3. Some waterfront buildings are vulnerable to flooding at extreme high tides or under storm surge conditions and minimum foundation levels may need to be established.

### Water Supply System

- 1. Changes in permafrost will have implications for both existing and new underground piping.
- 2. Warmer air temperatures could cause surface evaporation of the City's water supply and could eventually reach temperatures that allow algae and other micro-organisms to grow, thereby compromising water quality.
- 3. Increased rainfall could potentially put the municipal water supply at risk by washing contaminants and soil into the reservoir.

### Wastewater Treatment System

1. Increased precipitation, in the form of heavy rainfall, could overwhelm the system and cause failure or overflow, which could contaminate adjacent water bodies.

### Waste Disposal System

1. Increase in the active layer of permafrost could lead to changes the freeze-thaw cycle, drainage and water flow around the landfill. Design and operation of the landfill needs to take this into consideration.

## 2.3.1.1 Short Duration Rainfall Events

Regarding climate change effects on short duration rainfall events, IDF\_CC Online Tool v3.5 developed by Western University (Simonovic, Schardong, Gaur, & Sandink, 2018) provides projected rainfall intensity-duration-frequency (IDF) data under climate change. The IDF curves are calculated using historical data combined with data from Global Circulation Models (GCM) projected from 2050 to 2100. The tabular data is listed in Table 2-1. Detailed hydrological modelling of Kimmirut was conducted based on these climate change adjusted rainfall volumes.



|           | -     |       | -     | -     |       |       |
|-----------|-------|-------|-------|-------|-------|-------|
| T (years) | 2     | 5     | 10    | 25    | 50    | 100   |
| 5 min     | 1.31  | 1.89  | 2.42  | 3.36  | 4.24  | 5.16  |
| 10 min    | 1.92  | 2.95  | 4.02  | 6.20  | 8.53  | 11.38 |
| 15 min    | 2.62  | 4.07  | 5.52  | 8.32  | 11.17 | 14.36 |
| 30 min    | 4.68  | 6.73  | 8.32  | 10.81 | 12.75 | 14.36 |
| 1 h       | 7.21  | 9.90  | 12.32 | 16.65 | 20.60 | 24.64 |
| 2 h       | 11.12 | 14.53 | 17.48 | 22.60 | 27.05 | 31.31 |
| 6 h       | 21.50 | 28.46 | 32.89 | 38.76 | 42.28 | 43.89 |
| 12 h      | 30.91 | 40.46 | 45.76 | 52.11 | 55.29 | 39.79 |
| 24 h      | 37.50 | 49.75 | 56.42 | 64.42 | 68.54 | 69.44 |

## Table 2-1: Projected IDF at Kimmirut (Ungauged Location, Total mm)

## 2.3.1.2 Kimmirut Regional Climate Projections

Atlas Canada (The Prairie Climate Centre, 2019) climate change projections were analysed for the region surrounding the Hamlet of Kimmirut. Atlas Canada projects changes over the 30-year time periods of 1976-2005 and 2021-2050 for the RCP8.5 climate change scenario. Between these two time periods, the annual mean temperature is expected to increase by 2.8 °C from -8.8 °C to -6.0 °C. Annual precipitation is expected to increase by 12 percent from 422 mm to 472 mm. The maximum 1-day precipitation is expected to increase by 14 percent from 18 mm to 20 mm between the same time periods. Seasonal mean temperature and precipitation projections are shown in Table 2-2 below.

### Table 2-2: Atlas Canada RCP8.5 Climate Change Projections

| Metric                      | Projected Increase | 1976-2005<br>Mean Value | 2021-2050<br>Mean Value | Unit |
|-----------------------------|--------------------|-------------------------|-------------------------|------|
| Spring Mean Temperature     | 2.2 °C             | -13                     | -10.7                   | °C   |
| Summer Mean Temperature     | 1.6 °C             | 5.1                     | 6.7                     | °C   |
| Fall Mean Temperature       | 2.3 °C             | -4.5                    | -2.1                    | °C   |
| Winter Mean Temperature     | 4.7 °C             | -22.9                   | -18.2                   | °C   |
| Spring Precipitation        | 9 %                | 77                      | 84                      | mm   |
| Summer Precipitation        | 9 %                | 141                     | 153                     | mm   |
| Fall Precipitation          | 11 %               | 125                     | 139                     | mm   |
| Winter Precipitation        | 21 %               | 79                      | 96                      | mm   |
| Maximum 1-Day Precipitation | 14 %               | 18                      | 20                      | mm   |

As a result of the projected increase in spring temperatures for the 2021-2050 time period, the timing of the spring snowmelt event is expected to occur approximately 6 days earlier in the spring season. The timing of the start of snowfall in the fall season is expected to be delayed by approximately 10 days compared to the 1976-2005 time period due to the projected increase in fall temperatures.



As a result of the projected change in spring melt and fall freeze dates, the duration of winter is expected to decrease for the 2021-2050 time period by approximately 16 days. Due to the expected shorter winter duration, an approximate 8% reduction in precipitation as snowfall is estimated; conversely, as a result of the projected monthly precipitation increases, snowfall in the Kimmirut area is expected to increase by approximately 11%. The combined net effect of a shorter winter and the increase in precipitation is estimated to result in a 3% increase in annual snowfall for the 2021-2050 time period.

In the spring, despite the timing of the freshet being expected earlier, the 2021-2050 warming rate is projected to be very similar to the average warming rate on record in the 1976-2005 time period. A projected precipitation increase of approximately 0.1 mm per day during the spring snowmelt period results in an estimated increase of approximately 1 to 3 mm of rainfall during the spring snowmelt period. Therefore Tetra Tech estimates the springtime snowmelt runoff rates for the 2021-2050 time period to increase by a marginal amount.

During the part of the year when temperatures in Kimmirut are above-freezing, an increase of approximately 10% rainfall, from 195 mm to 214 mm is projected for the 2021-2050 time period. Due to the projected increased rainfall, larger and more severe summer precipitation events are expected for the Kimmirut region in the 2021-2050 time period. Figures 2-3 and 2-4 below show the Atlas Canada temperature and precipitation projections discussed in this section.

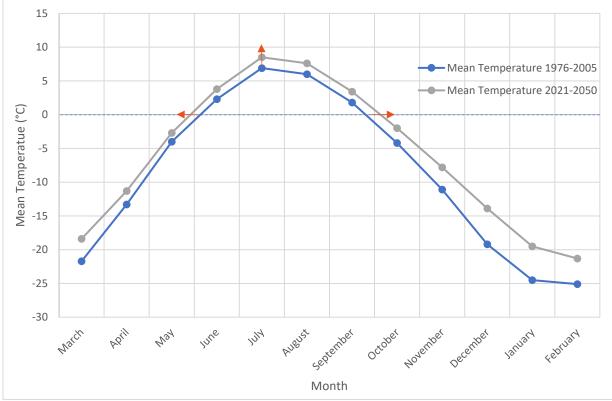


Figure 2-1: Atlas Canada Projected Monthly Mean Temperature





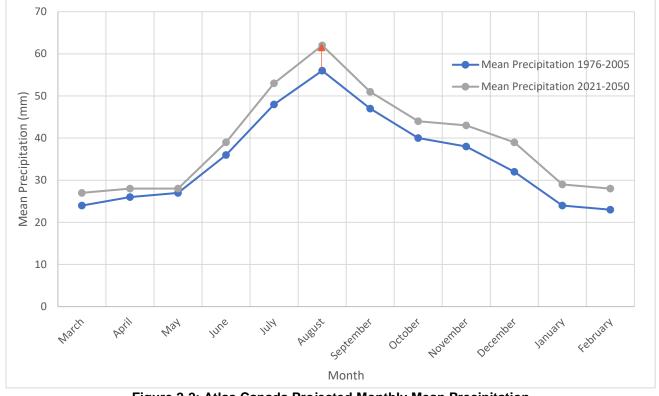


Figure 2-2: Atlas Canada Projected Monthly Mean Precipitation

# 3.0 INVENTORY OF EXISTING DRAINAGE SYSTEM AND ISSUES

A critical task in the development of a Drainage Master Plan is to identify, assess, and log all critical drainage infrastructure and known deficiencies. This process included the location and description of the physical assets that compose the drainage system, including key geometric characteristics and conditions. Using field and desktop data, this information was used to build a georeferenced map of the drainage system. The inventory also includes the location and description of existing issues such as ponding and damaged culverts. The following sections describe the activities conducted during the site visit, and the development of the georeferenced map of the drainage system.

# 3.1 Site Visit

A site visit was conducted from May 29-30, 2019 by two Tetra Tech staff, Mark Aylward-Nally and David Moschini. The purpose of the site visit was to:

- Discuss ongoing drainage issues and maintenance practices with the Kimmirut foreman, Miki Lyta;
- Conduct a walkthrough inspection of the drainage system of the Hamlet; and
- Conduct informal interviews with local residents regarding known drainage issues.



## 3.1.1 Walkthrough Inspection

A walkthrough of Kimmirut was conducted from May 29 to May 30, 2019. The objective of the site visit was to:

- Develop an understanding of the drainage patterns through the town;
- Identify main drainage routes and key infrastructure assets;
- Get GPS points of key infrastructure locations, for instance upstream and downstream culvert ends;
- Measure culvert dimensions and document culvert conditions;
- Identify areas of ponding;
- Record a photo inventory of key elements of the drainage system;
- Identify drainage outlet locations; and
- Conduct Informal Interviews with Hamlet residents.

Based on the walkthrough inspection, Tetra Tech has observed the following:

- 1. Aside from the main drainage corridor within Kimmirut (which runs from the arena, past the airport, and through town) the remainder of the Hamlet is lacking a formal drainage system.
- 2. This remaining area is plagued by nuisance ponding, roadway rutting, and has the potential for roadway washouts during heavy rainfall events or snowpack years.

Photographs of the existing system components and their condition are included in Appendix E.

## 3.1.2 Development of the Georeferenced Map

Using the GPS points, field notes and photographs obtained during the site visit, the topology of the drainage network was put together in a GIS shapefile. The shapefile includes locations of open channels (ditch or swale) or culverts. A naming convention was developed and every asset was named in the shapefile. Connectivity of the drainage system was developed using data from the site visit, and supplemented by mapping data provided by the government. A separate shapefile was created to mark areas with drainage issues identified during the site visit. The drainage issues identified included ponding areas, damaged culverts, uncontrolled overland flow and erosion issues. Figures 3-2 to 3-5 in Section 3.4 highlight the documented drainage issues.

## 3.2 Drainage

The drainage patterns of the Hamlet of Kimmirut follow the natural relief, however the construction of fill pads for buildings and road embankments have modified the natural drainage trends, leading to an increase in surface runoff volume and peak flows. The majority of runoff passing through the community is confined to a single watercourse, with its headwaters located within the ridges which flank the community. Runoff from these ridges collects in a channel alongside the airstrip before flowing east through the community and into Glasgow Inlet. It is this watercourse which endured a flash flood during the 2012 freshet, flooding a home just east of the airstrip. We estimate this watercourse to have a watershed area of approximately 89 hectares at its confluence with the inlet.



Tetra Tech have completed a delineation of the existing drainage patterns within Kimmirut using the 2015 Aerial Photograph derived DEM as well as from observations and photographs collected during the site visit. Drainage areas and flow paths are presented on Figure 2-1 in Section 2.2.1.

Land allocated for future expansion of the community is located up the valley to the northwest based on the 2014 Community Plan. These lots are located at a local high point and are anticipated to drain in a variety of directions, including into Lake Fundo and Soper Lake. Developing drainage paths and proposed drainage infrastructure for these future development areas is included within the scope of the Master Drainage Plan.

## 3.3 Drainage Infrastructure

During the 2019 freshet site visit, existing ditches, swales, and natural streams were observed. Additionally, 32 culverts were assessed. The diameter of the culverts ranged from 300 mm to 1200 mm, with the majority having a diameter of 500 mm or 600 mm. Most of the culverts were damaged or partially or fully buried, and some were more functional than others. An Inventory of Existing Culverts is included in Appendix E. Naturally formed swales and streams were observed throughout the community including few formal ditches.

## 3.4 Drainage Issues

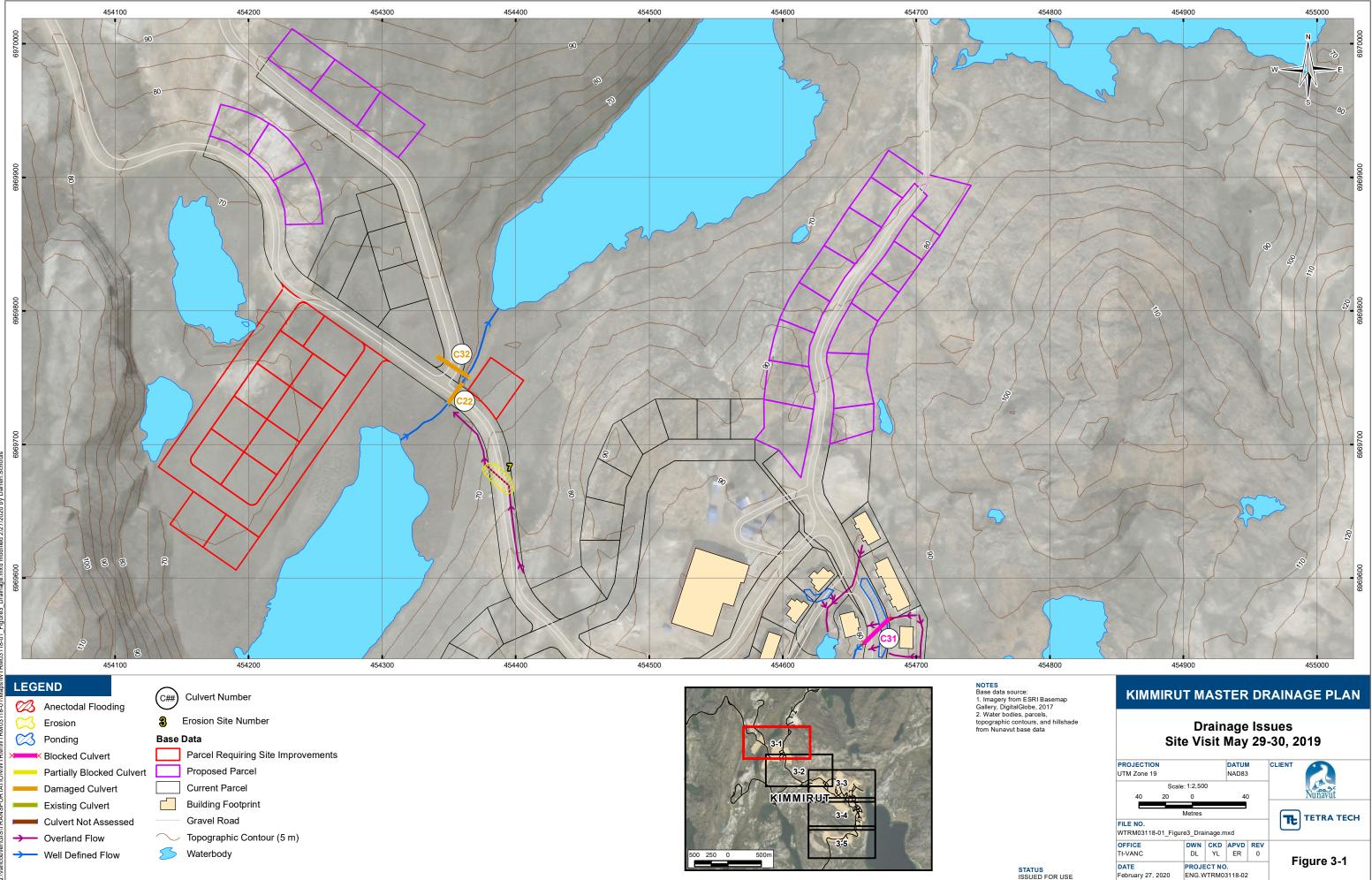
Developing and maintaining a well-functioning drainage system is an ongoing concern within most northern communities. From Tetra Tech's 2019 freshet site visit, several types of drainage issues in Kimmirut were identified. Many of the existing culverts were damaged, buried, and/or blocked with sediment, rocks, and debris. Ice blockages were also noted. A lack of formalized ditches was an issue which resulted in ponding and flow paths across roadways which can cause washouts and rutting during a larger rainstorm or snowmelt event.

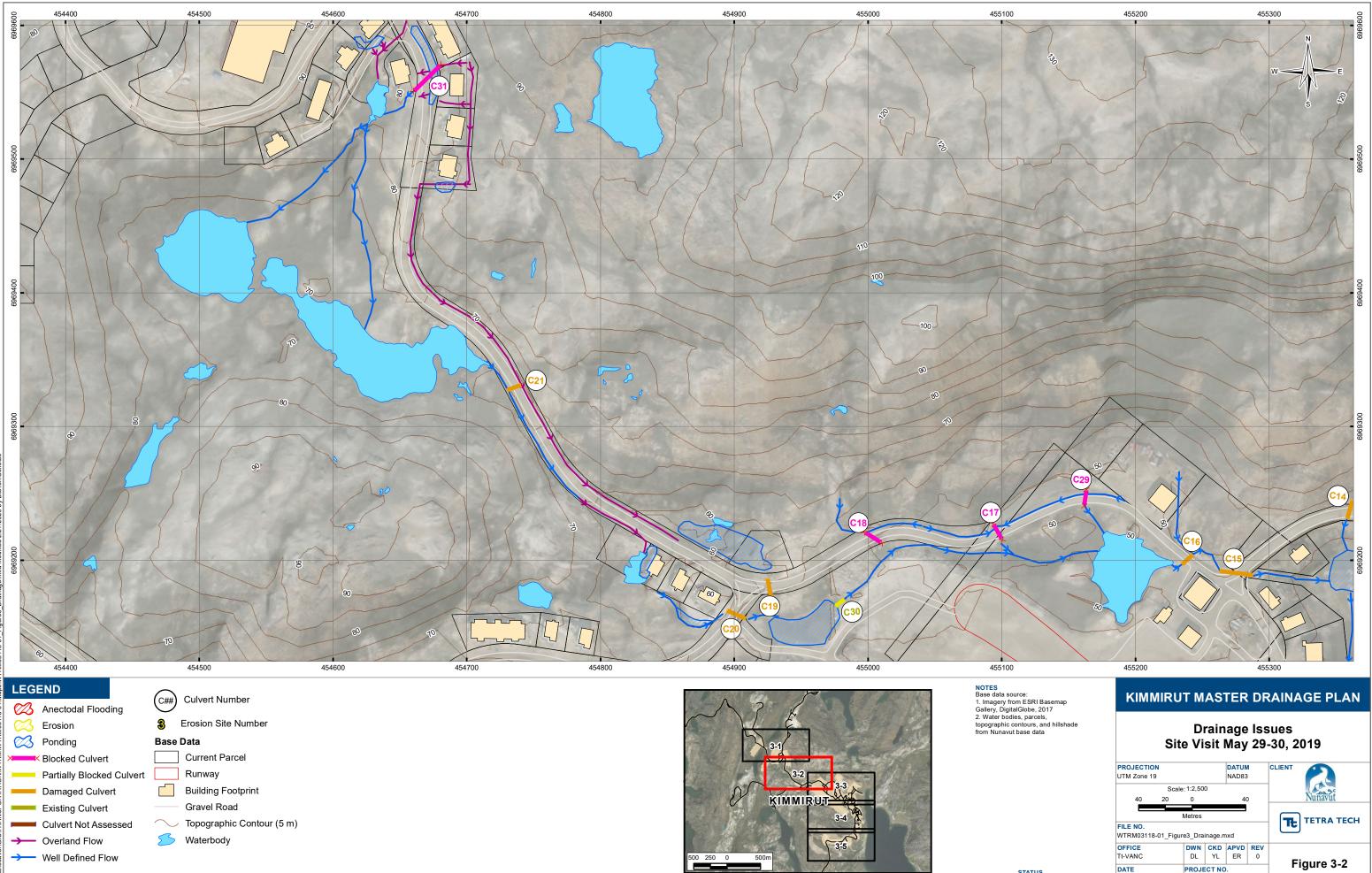
Typical drainage issues identified within the community of Kimmirut are detailed in Table 3-1.

|   | •  |
|---|--|
| Issue                                     | Cause  |
| Spring flooding                           | Culvert blocked by ice/snow  |
| Damaged culvert<br>inlet/outlet           | Damage caused by excavator cleaning snow<br>and/or ice during spring                                   |
| Buried or blocked culvert<br>inlet/outlet | Culvert inlet and/or outlet blocked due to sediment, rock, and debris deposition, and/or ice blockage. |
| Ponding                                   | Blocked culverts, poor grading, vegetation overgrowth, lack of an outlet.                              |
| Erosion                                   | Velocity threshold for erosion is exceeded   |

## Table 3-1: Kimmirut Drainage Issues

Figures 3-1 to 3-5 below depict the drainage issues and existing infrastructure identified in Kimmirut and include the anecdotal flooding event that occurred downstream of the airport on May 6, 2012, which damaged a public housing duplex (CBC News, 2012). Figures 3-6 to 3-12 show examples of the typical drainage issues identified during Tetra Tech's site visit. Appendix E includes a summary of the existing culverts and erosion sites identified within the community.



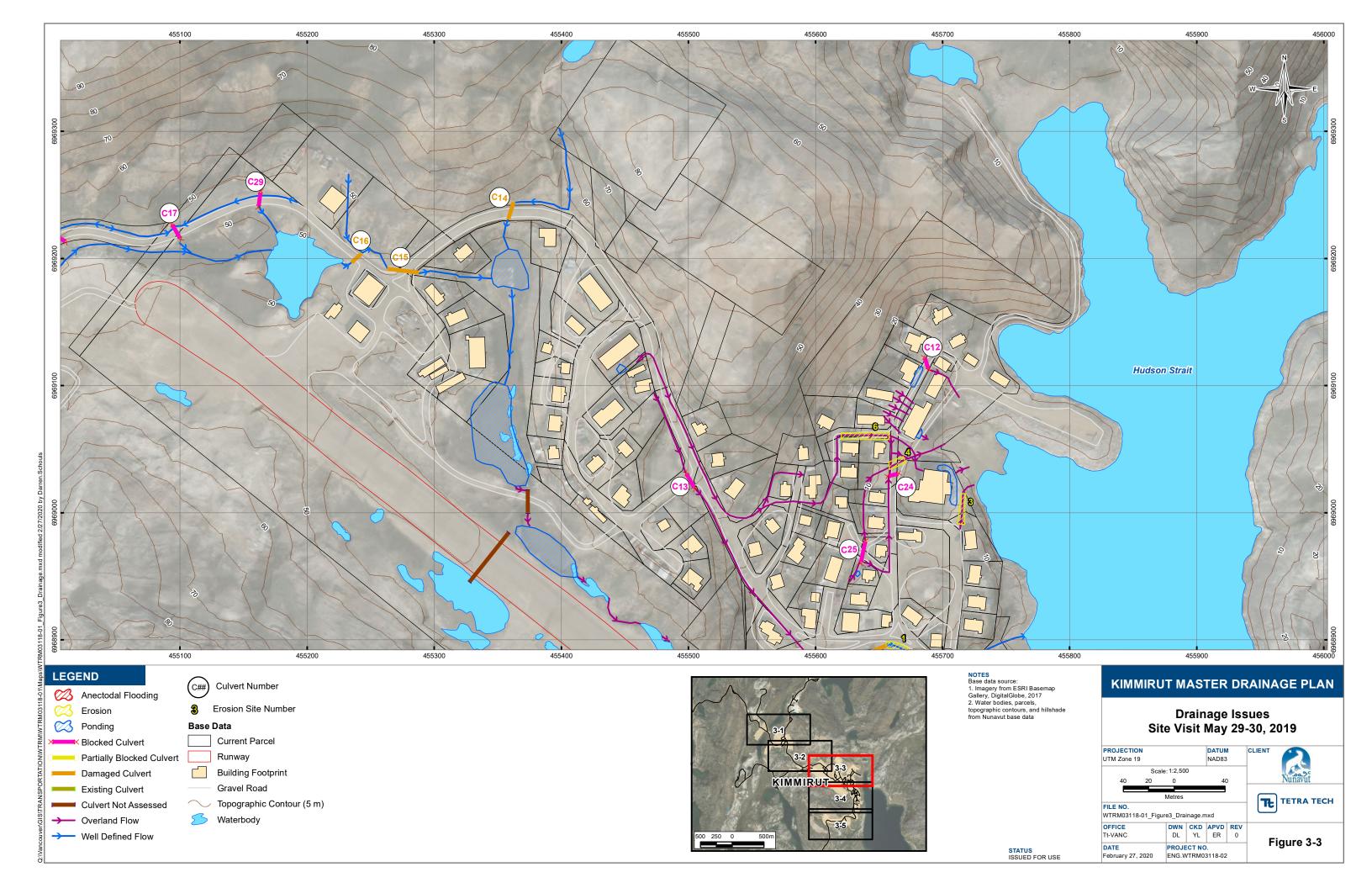


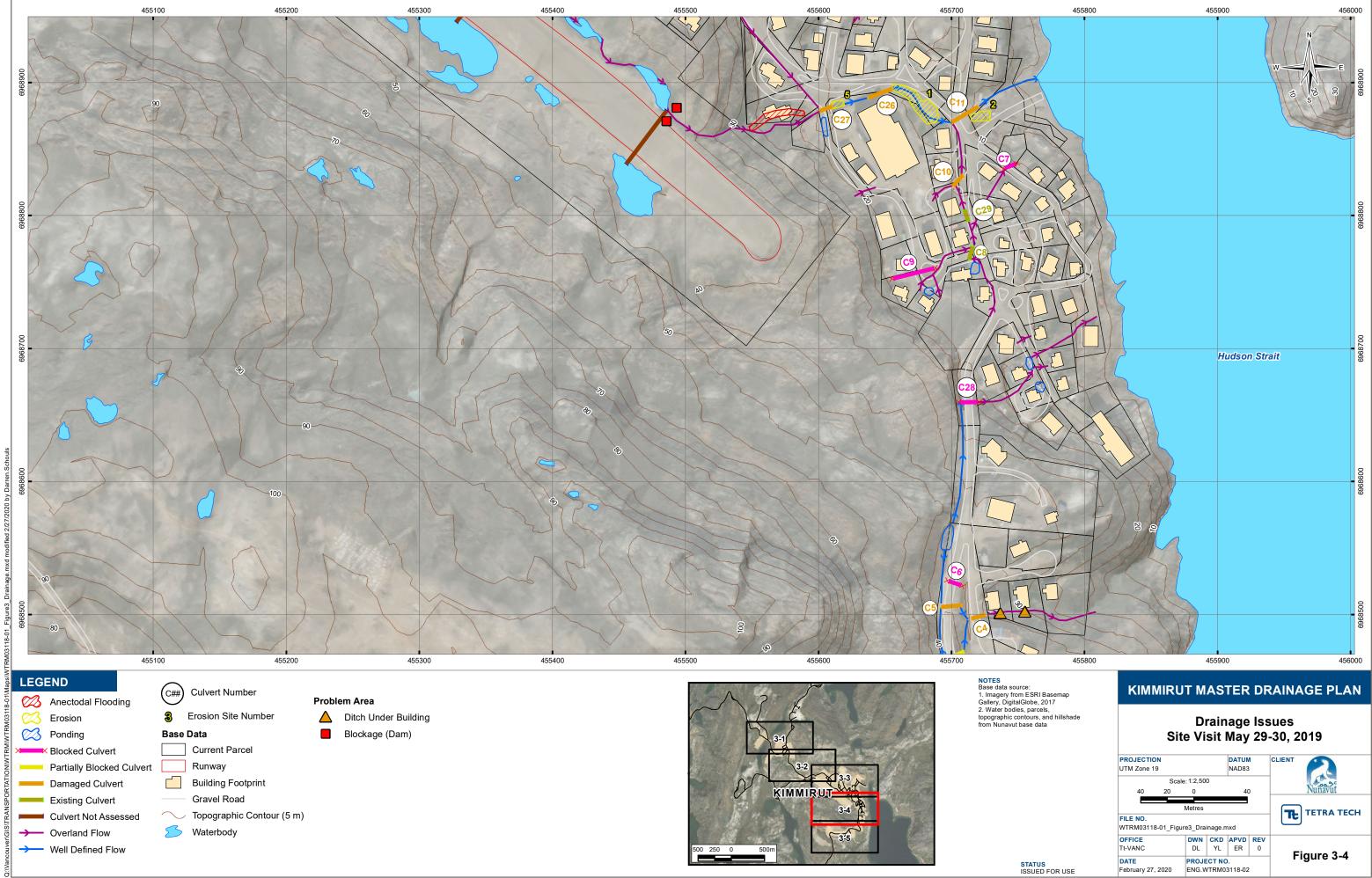
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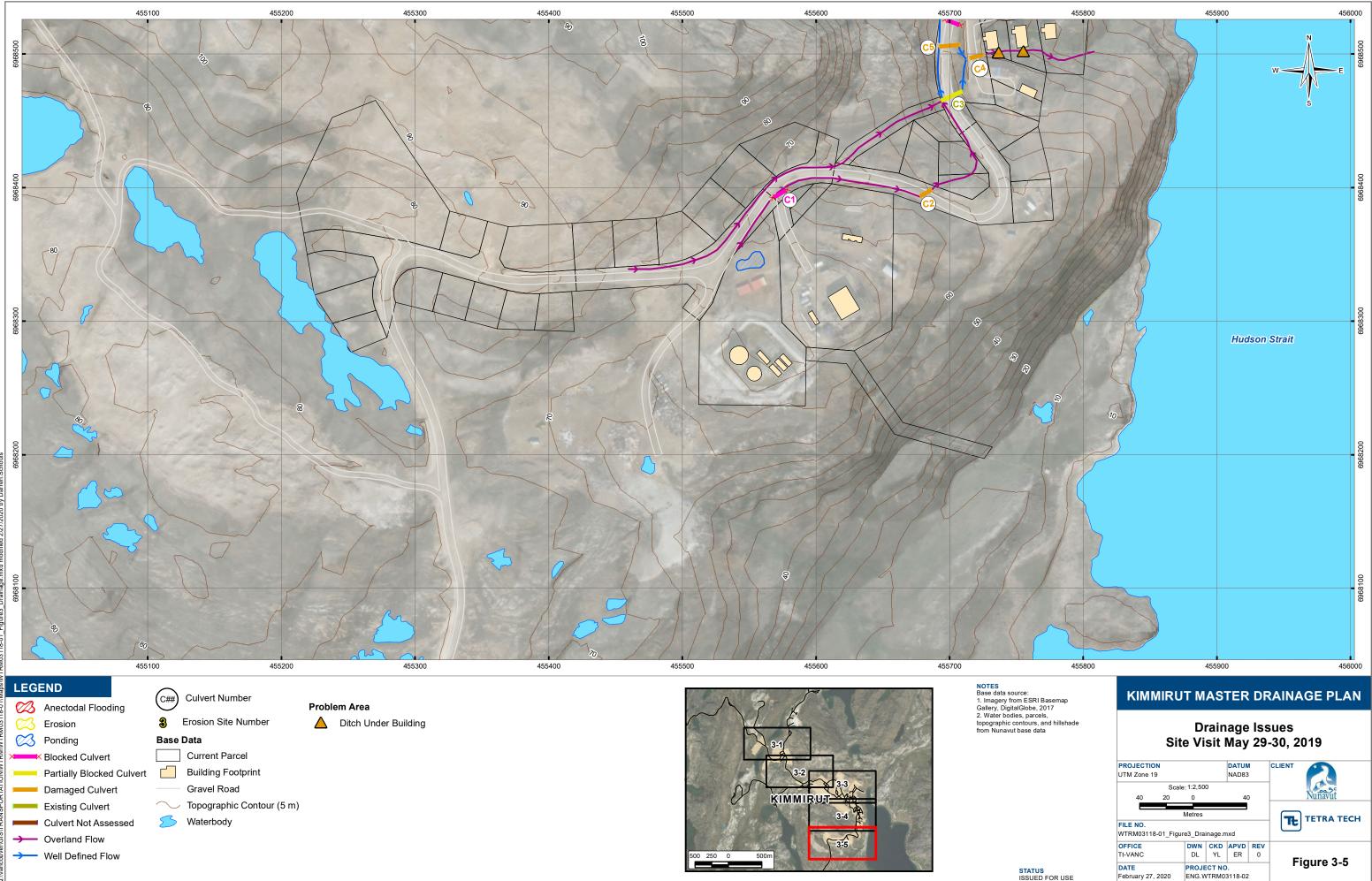
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| Figure<br>No. | Description                                     | Image    |
|---------------|---|----------|
| 3-6           | Typical damaged<br>culvert inlet.<br>Culvert 20 |          |
| 3-7           | Ponding water<br>near building                  |          |
| 3-8           | Overland flow                                   | <image/> |





| Figure | Description   |       |
|--------|---|-------|
| No.    | Description   | Image |
| 3-9    | Typical damaged<br>culvert outlet.<br>Culvert 10                                      |       |
| 3-10   | Main<br>watercourse<br>through<br>Kimmirut. Site of<br>May 6, 2012<br>flooding event. |       |
| 3-11   | Overland flow<br>around house   |       |





| Figure<br>No. | Description                   | Image |
|---------------|-------------------------------|-------|
| 3-12          | Ponding water<br>around house |       |

Figures 3-6 to 3-12: Kimmirut Drainage Issues – Site Visit May 29-30, 2019

# 3.5 Site Equipment

During the site visit, an inventory of the available equipment within the community of Kimmirut was developed. The following non-exhaustive list of equipment was noted in Kimmirut:

- Excavator: CAT 320E
- Bulldozer: CAT D6T
- Backhoe: CAT 420D
- Front-loader: Deere 624K
- Rock Crusher: Lokotrack LT96
- Grader: Volvo grader
- Dump Trucks

# 4.0 ANALYSIS OF DRAINAGE SYSTEM

Drainage principles, design criteria, and design scenarios used to develop the proposed drainage system for the Hamlet of Kimmirut are detailed in this section of the report, as well as modelling results and recommendations.

## 4.1 Drainage Principles

According to the guidelines for community drainage system planning, design, and maintenance in northern communities (CSA Group, 2015), drainage systems should be designed in accordance with the level of risk that is established during the planning process. The CSA Group also noted that:





- "It is recognized that the capacity of any drainage system might be exceeded at some point;
- The design will be impacted by physical constraints present within communities;
- The desired acceptable level of risk might not be achievable in any given community due to physical (spatial) limitations, resources, subsurface conditions, and topography, among other factors;
- The acceptable level of risk established might be impacted by the changing climate, for example, due to the changing climate, what was previously considered to be a 1-in-10 year event might occur on average every five years in the future."

In addition to the CSA Group's design principles, the development of the proposed upgrades was based on Tetra Tech's practical principles as follows:

- 1. Effectively capture and route water around populated areas to protect buildings and communities;
  - a. Where possible, minimize the imposition of waterways through populated areas by restricting use of large ditches to areas outside of the populated areas;
- 2. Utilize shallow swales for driveway crossings and roadside drainage;
- 3. Minimize complexity for drainage system construction, maintenance, and management by:
  - a. Minimizing the number of different culvert diameters specified;
  - b. Minimizing the number of new culverts, which would not only need to be barged to Kimmirut for installation, but also need to be maintained once installed;
  - c. Minimizing the number of different ditch and swale dimensions specified;
  - d. Keeping the design simple such that the Hamlet foreman and crew can not only construct but also maintain the new drainage systems with ease;
- 4. Capture and immediately convey water towards the nearest major watercourse/waterbody (i.e. ocean, lake, river, or stream);
- 5. Use multiple outlets to add redundancy at critical locations throughout the system;
- 6. Design using projected precipitation trends to account for future climate change;
- 7. Select culvert sizes based on available roadway embankment cover;
- 8. Design drainage swales through driveways to comfortably accommodate the tires and undercarriage of vehicles; and
- 9. Develop plans recognizing the land use limitations, for example remove nuisance ponding from the front of the Northern Store and from the foot of exterior staircases leading to residences.



# 4.2 Design Criteria

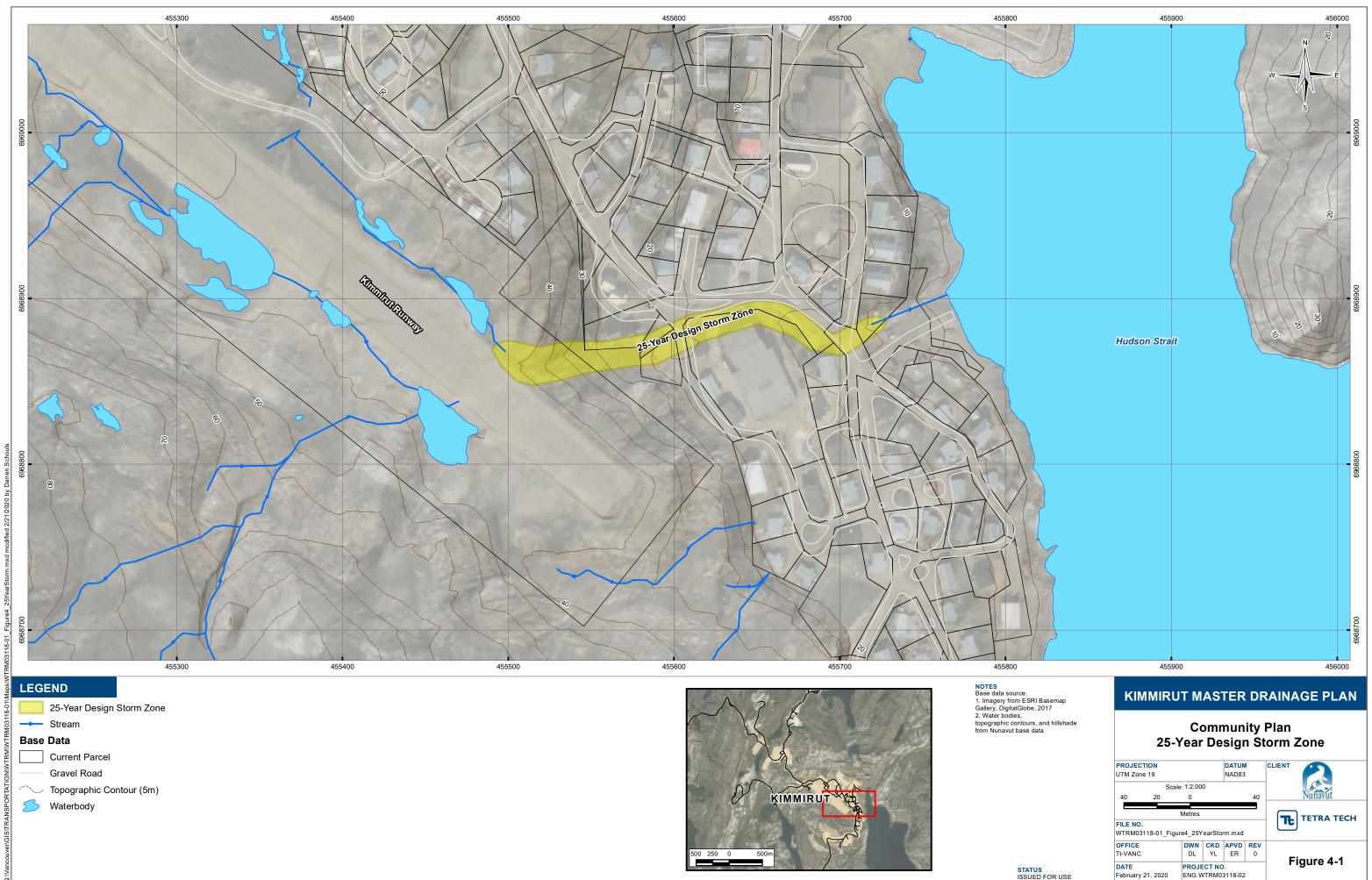
As per the guidelines for community drainage system planning, design, and maintenance in northern communities (CSA Group, 2015), the culvert design capacity prescribed by the CSA Group is:

- Size culverts to accept design flow at 80% capacity under free flow condition (1:10 year event).
- Size culverts to accept 1:100 design flow at 80% of available head at entrance.

In addition to the above requirements the proposed drainage system was developed to meet the following general criteria:

- Ditches and swales were sized to convey the 10-year 1-hour storm event. The duration of the 1-hour storm was selected as the critical event following a review of a number of storm durations ranging from 1 hour to 24 hours. The goal was to provide sufficient capacity to handle the critical event. Tetra Tech has further upsized the culverts to add additional capacity to compensate for debris deposition blocking the culverts and limiting their capacity. Buried culverts and significant deposition was noted in the majority of culverts noted in the field visit described in Section 3.1.
- 2. Along the main stream draining the airport through the main part of town (see Figure 4-1), culverts were sized to convey the 25-year 1-hr event. Selection of the more severe storm event was based on the critical nature of this portion of the drainage system and proximity to the school.
- 3. Ditches were sized to maintain at least 100 mm of freeboard during the 10-year 1-hour storm event.
- 4. Swales were sized to maintain at least 50 mm of freeboard during the 10-year 1-hour storm event.







# 4.3 Design Scenarios

Kimmirut's geology promotes low rates of infiltration and in turn yields high runoff volumes, even during small rainfall or snowmelt events. The shallow surficial bedrock covered by a shallow overburden common to the area limits the amount of infiltration and groundwater recharge.

Based on the limited anecdotal information we have, we understand that historical flooding has occurred due to snowmelt events. However, we believe that the critical event likely to have the greatest impact on Kimmirut's drainage system is a severe rainfall event. Historical flooding noticed within the community is caused by the non-existent drainage system and poor snow management.

The model was run with six design storm scenarios: the 10-year 1-hr, 10-year 24-hr, 25-year 1-hr, 25-year 24-hr, 100-year 1hr, and 100-year 24hr event. Using historical data extracted from the Inuvik weather station, a synthetic distribution was developed to represent the rainfall pattern likely to develop over the course of a 24 hour event.

The 1-hr storm distributions were developed using the AES distribution for Northern Quebec. Climate change adjusted precipitation volumes for each of the scenarios were obtained using the IDF\_CC Tool 3.5 developed by Western University as described in Section 2.1 of this report, and the volumes are summarized in Table 4-1.

As the IDF\_CC tool is reporting data for the Kimmirut community as ungauged, Tetra Tech has verified the quality of the rainfall estimates using data extracted from both the Kimmirut weather station (1994 to 2004) and nearby weather stations (Cape Dorset, 1971 to 2019).

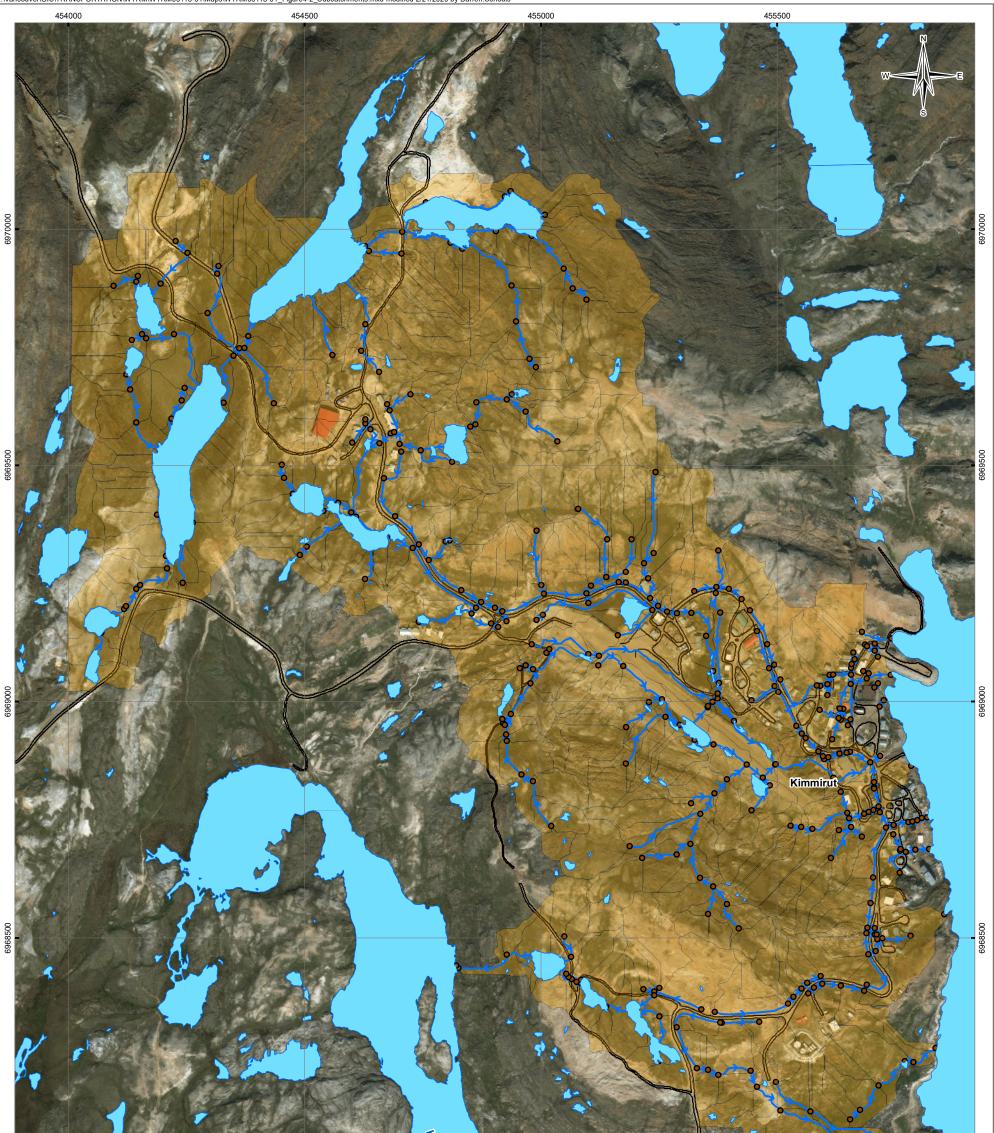
| Design Storm Scenarios | Volume (mm) |
|------------------------|-------------|
| 10-year 1-hr           | 12.3        |
| 10-year 24-hr          | 56.4        |
| 25-year 1-hr           | 16.7        |
| 25-year 24-hr          | 64.4        |
| 100-year 1-hr          | 24.6        |
| 100-year 24-hr         | 69.4        |

## Table 4-1: Kimmirut Design Storm Scenarios

## 4.4 Modelling of System

A systems analysis approach was adopted to design the proposed drainage system for the Hamlet of Kimmirut. PCSWMM, a state-of-the-art stormwater program was used to develop the model of the drainage system. The model uses a node-link arrangement where links represent conduits, such as ditches and culverts; and junctions represent a point where two or more links are joined, according to how the drainage network operates.

In addition, the drainage area is split into subareas or subcatchments, which are the hydrological units used to calculate flows. Flows calculated from a subcatchment are assigned to a junction, and then hydraulically routed through the drainage network. Through this approach, flows are aggregated through the system until discharged to an outfall point. Figure 4-2 shows the sub-catchments, junctions and conduits represented in the model. Input parameters for the subcatchments, junctions and conduits are presented in Appendix G.





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### LEGEND

Junction

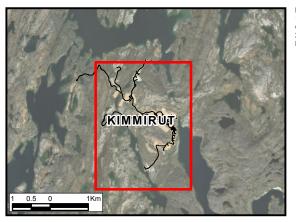
---- Conduit

Subcatchment

#### Base Data

— Gravel Road



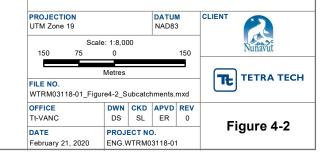


NOTES Base data source: 1. Imagery from ESRI Basemap Gallery, DigitalGlobe, 2017 2. Water bodies from Nunavut base data

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## KIMMIRUT MASTER DRAINAGE PLAN

## **PCSWMM Model of Kimmirut**



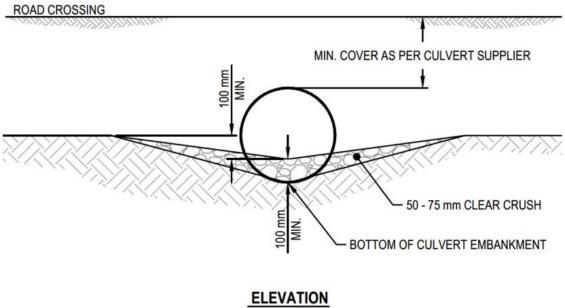


# 4.5 Modelling Results

Although the typical process followed in developing a stormwater management plan includes development of a hydrologic/hydraulic model of the existing system, the absence of a proper drainage system within the community has forced Tetra Tech to shortcut directly towards modelling of the proposed system and then use the modelling results to size and identify the type of infrastructure required to convey the estimated flows.

After modelling the scenarios described in Section 4.3, Tetra Tech proposes that 27 of the existing culverts be upgraded and that 18 new culverts be added to the system. In addition, Tetra Tech is also recommending that a formal system of swales and ditches be integrated into the community allowing for the safe conveyance of runoff. Table 1 in Appendix F shows the specifications and modelled performance of the 45 proposed culverts for the 10-year 1-hour design storm scenario. As detailed, Tetra Tech is recommending that the proposed culverts range in size between 450 mm to 1400 m.

As the CSA recommends that culverts be sized to a minimum of 450 mm in diameter, Tetra Tech has opted to maintain this minimum size requirement. It should be noted that in certain cases the swale profiles and site limitations will force the embedment of some culverts so to meet the minimum depth of cover requirements set by the supplier of the selected culvert. The minimum cover requirements are needed to structurally support the integrity of the culverts. Figure 4-3 provides a schematic representation of the typical installation details where the integration of the minimum depth of cover requires culvert embedment.



SCALE: NTS

Figure 4-3: Typical Embedded Culvert Details





As noted in the proposed plans, a number of swales are being proposed in recognition of the narrow roadways in Kimmirut. Throughout numerous areas within the community, the buildings are very close to the edge of the road network. The alternative to swales of adding deep/wide ditches will inevitably impact the ability of the hamlet residents to access their properties and will likely impact traffic movement. Figure 4-4 below provides an overview of the typical challenges a deep drainage system would have to contend against.



Figure 4-4: Typical Narrow Laneway in Kimmirut

# 4.6 Drainage Recommendations

This section presents a summary of recommended actions needed to upgrade the Level of Service of the drainage system of the Hamlet of Kimmirut. Currently, there are a number of deficiencies as identified in Section 3.0. Tetra Tech has developed the following series of recommendations which, when implemented will remedy the issues identified throughout the community.

The proposed upgrades for the community include the upgrading of culverts, ditches and swales.



## 4.6.1 Culverts

- 1. The minimum culvert size should be 450 mm. The minimum culvert size recommendation from CSA Group (2015) is 450 mm for de-icing purposes.
- 2. Cover over culverts shall meet the structural requirement set by the supplier of the selected pipe type. A recommended minimum of 300 mm should be included where vehicular traffic is likely to be present.
- 3. For long-term durability, the proposed culvert material should be Smooth Wall Steel Pipe (SWSP). The use of SWSP including a wall thickness of 10 to 12 mm will afford the community a very long service life. As detailed in Appendix E, most if not all corrugated steel pipes in Kimmirut have failed to retain their structural integrity and have likely been damaged by maintenance equipment or road traffic. If however CSP culverts are preferred, Tetra Tech recommends the use of culvert end stiffeners or sleeves to better support the structural integrity of the ends of the culverts. A sample photo of a culvert end stiffener is included in Appendix H. Note that Tetra Tech recommends a wider stiffener covering 2 times the culvert diameter. Details of a culvert end stiffener and sleeve are included in Figure 5-11 in Section 5.4.1.
- 4. Inlet grates are recommended for the three proposed 1400 mm diameter culverts.
- 5. Culverts should be provided with high visibility markers to prevent damage during spring cleaning activities.
- 6. An annual maintenance program should be implemented to prepare the system for the spring freshet. This may include the steaming of specific culverts and/or the removal debris limiting the capacity of the culvert crossings.
- 7. Table 1 in Appendix F includes the proposed culvert upgrades throughout the hamlet.
- 8. Based on the areas of erosion noted during our site visit and on water velocities modelled using PCSWMM, Tetra Tech recommends the use of riprap aprons for culvert inlets and outlets. Appendix E includes riprap recommendation for all culvert aprons.
- 9. Culverts are to extend a minimum of one culvert diameter past the embankment as shown in Figure 5-17 in Section 5.4.3.
- 10. Headwall and endwall side slopes are to be 1.5H:1V to 2H:1V. Side slopes of 2H:1V are preferred where space allows.
- 11. Where space does not allow for a riprap protected side slope culvert inlets and outlets should include a concrete headwall as a recommended alternative option.

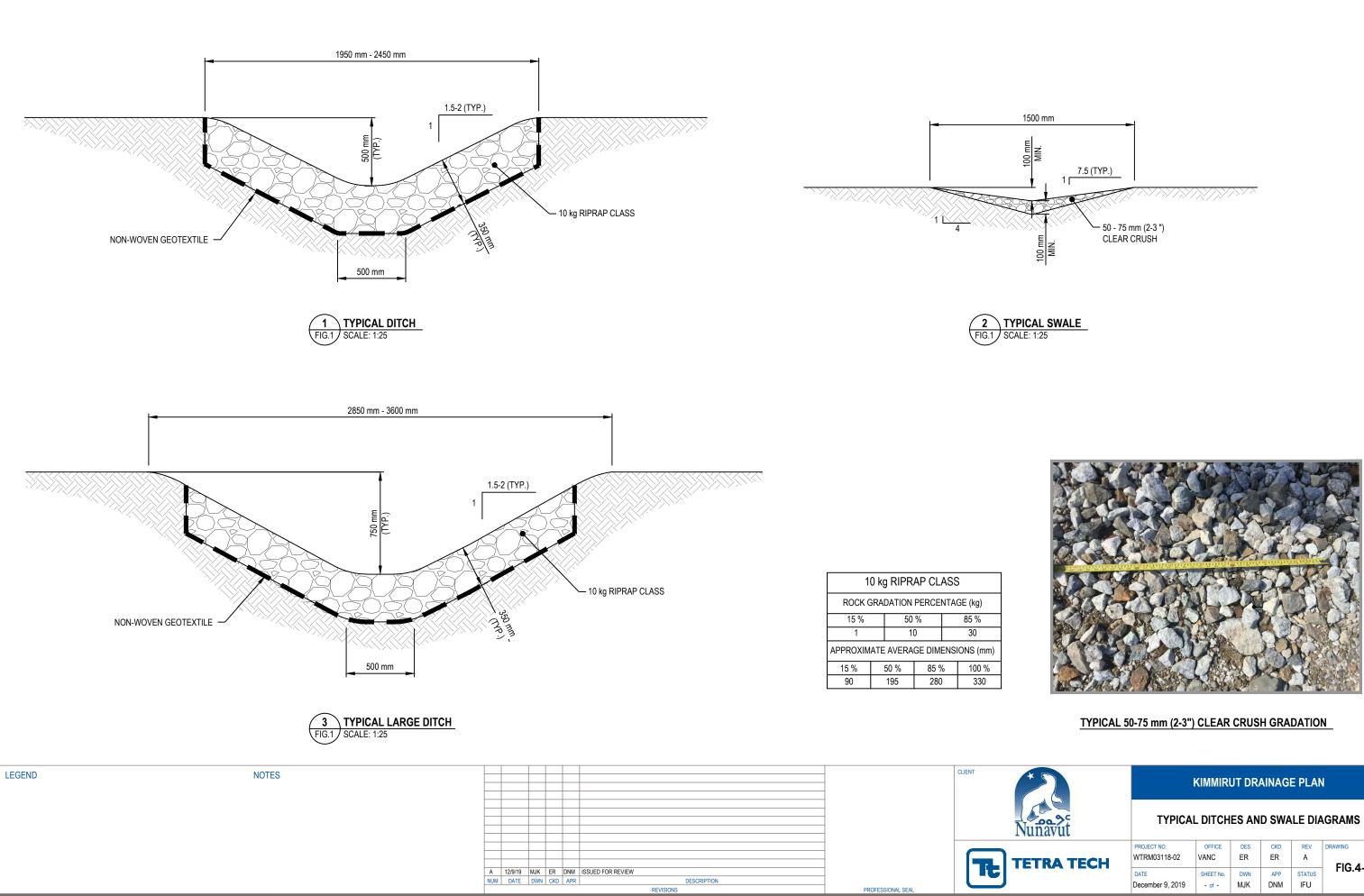
## 4.6.2 Ditches and Swales

- 1. Open channels must include a revetment system for erosion protection, particularly in areas where permafrost can be impacted. Failure to do so may lead to hydraulic erosion, which in turn may lead to thermal degradation of the permafrost layer.
- 2. Ditches and swales should be as flat as possible, but not flatter than 0.5%.
- 3. Ditches to have a minimum bottom width of 500 mm, a minimum depth of 500 mm and side slopes ranging between 1.5H:1V to 2H:1V.
- 4. Ditches in the 25-Year Design Storm Zone as shown in Figure 4-1 to have a minimum bottom width of 500 mm, a minimum depth of 750 mm, and side slopes ranging between 1.5H:1V to 2H:1V. Side slopes of 2H:1V are preferred where space allows. Flatter side slopes should be considered near schools and



children's playgrounds. Figure 4-5 includes typical cross section details for the proposed ditches and swales.

- 5. Ditches to be lined with a non-woven geotextile between the existing soil and the specified riprap layer.
- 6. Ditches are to be lined with a 10 kg class riprap layer having a minimum thickness of 350 mm.
- 7. Swales are to include a minimum depth of 100 mm. Swale side slopes are to be 7.5H:1V minimum to allow for vehicular traffic to safely cross without damage. Swales are to be lined with a 50-75 mm (2-3") clear crush layer having a minimum thickness of 100 mm in the centre of the swale. Figure 4-5 includes typical cross section details for the proposed swales.
- 8. The community of Kimmirut may wish to increase the active depth of the existing swales throughout the community by raising the road profiles. This may be necessary to formalize the proposed swale sections detailed in Figure 4-5.
- 9. To the extent possible, ponding water nearby and underneath of buildings should not be promoted. Grading practices underneath building should promote the movement of water away from the footprints of buildings.



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# 5.0 MASTER DRAINAGE PLAN

Based on the issues identified in the field, and on the modeling results, a number of upgrades are proposed for the existing drainage system, as well as for the proposed community expansion areas. The system being proposed is composed of ditches, swales and culverts, with outlet locations as shown in Figures 5-1 to 5-5. With the proposed upgrades combined with a proper maintenance program including removal of debris/sediments and de-icing, the proposed system will handle the design flows identified in Section 4.3 of this report.

# 5.1 Community Plan (Proposed Development Areas)

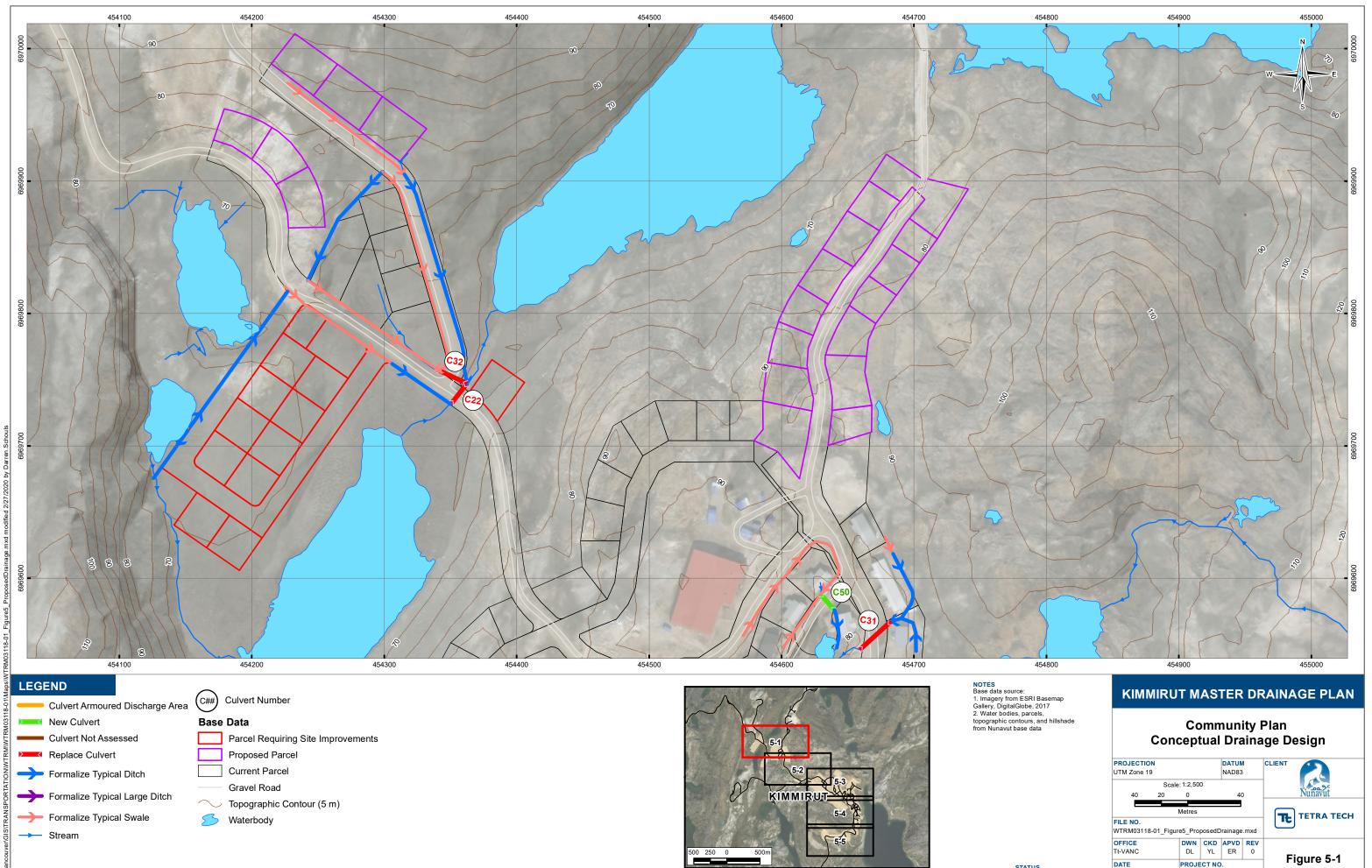
The 2014 Kimmirut Community Plan included in Appendix B outlines proposed developments which will allow for future community growth. Existing topography and drainage conditions were reviewed and a preliminary design of drainage infrastructure for the proposed development areas was developed.

Appendix B also includes a revised development plan for CGS to consider. Parcels outlined in red are recommended to be relocated due to observed poor drainage conditions. Tetra Tech recommends relocating the following proposed development areas:

- The 12 lots outlined in red in the northwest region due to the poor drainage conditions observed in the field. The proposed lots are downstream of a ridge and are within the natural drainage path draining into a lake downstream of the proposed development footprint. However, should CGS wish to develop this area, Tetra Tech recommends raising the building pad elevations above existing grade with suitable fill material as well as implementing the proposed perimeter ditch and swale system shown in Figure 5-1 to mitigate against drainage issues. The site would have to be raised to an elevation which is topographically higher than the crown of the road. That way, if the culvert is plugged, water will be able to overtake the road without impacting the proposed lots.
- The lot outlined in red beside Culvert 22 due to its proximity to the culvert crossing which imposes a risk of flooding. Should CGS wish to develop this lot, Tetra Tech similarly recommends raising the building pad elevation above existing grade with suitable fill material as well shifting the lot up the road further away from the flood plain area. The toe of the proposed embankment will need to be protected from erosion. The use of appropriately sized riprap will provide the necessary protection.

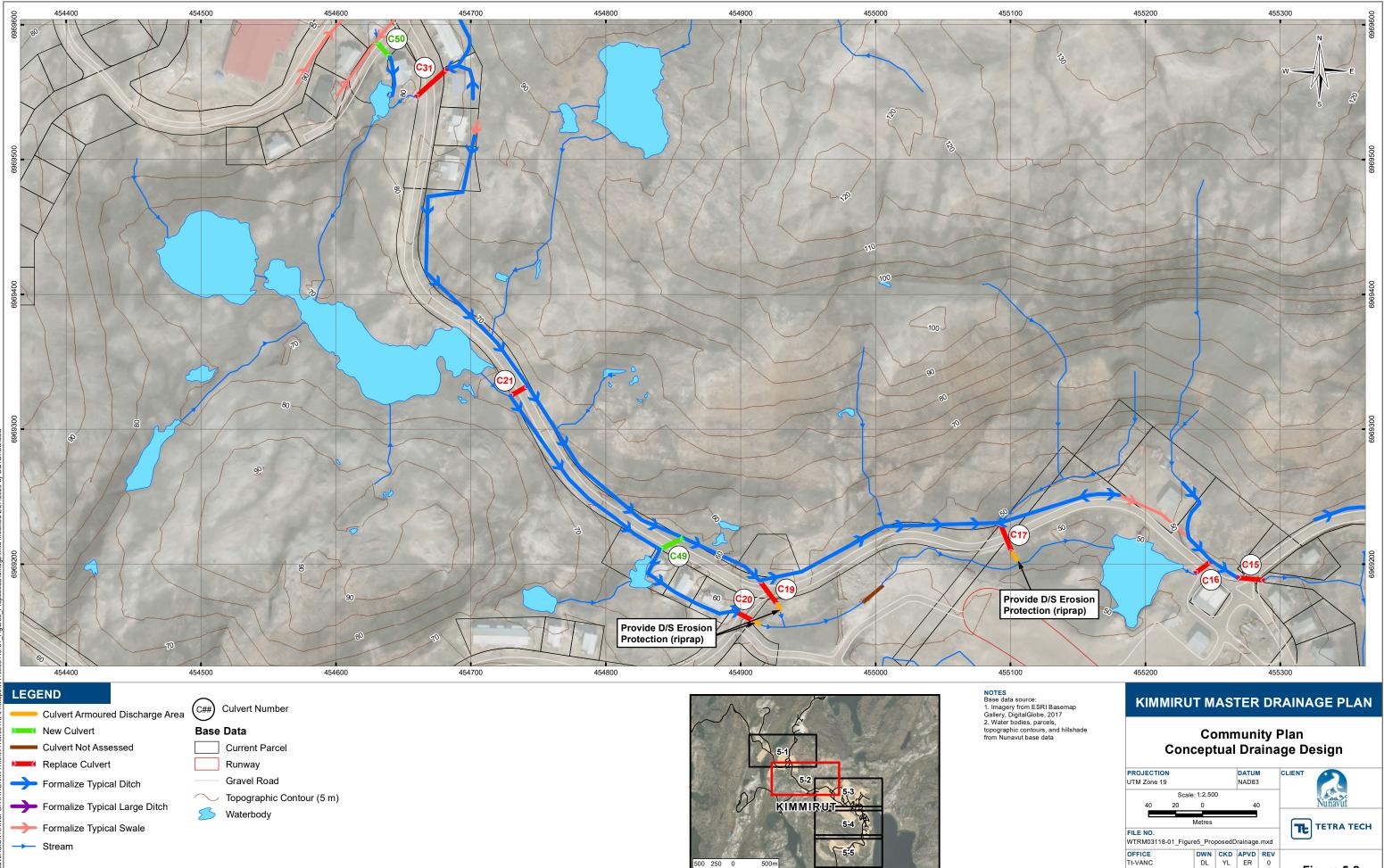
Parcels outlined in purple are proposed relocation lots for the lots outlined in red and are strategically located in areas which appear to be well-drained, as well as suitable for construction. The proposed revisions are intended to protect future development from potential drainage issues. The community expansion lots on the ridges surrounding the ice rink appeared to be in suitable locations with respect to drainage considerations. Grading of these lots should promote movement of surface water away from the buildings and access roads. It should be noted that this report did not review the geology or permafrost conditions within the community.





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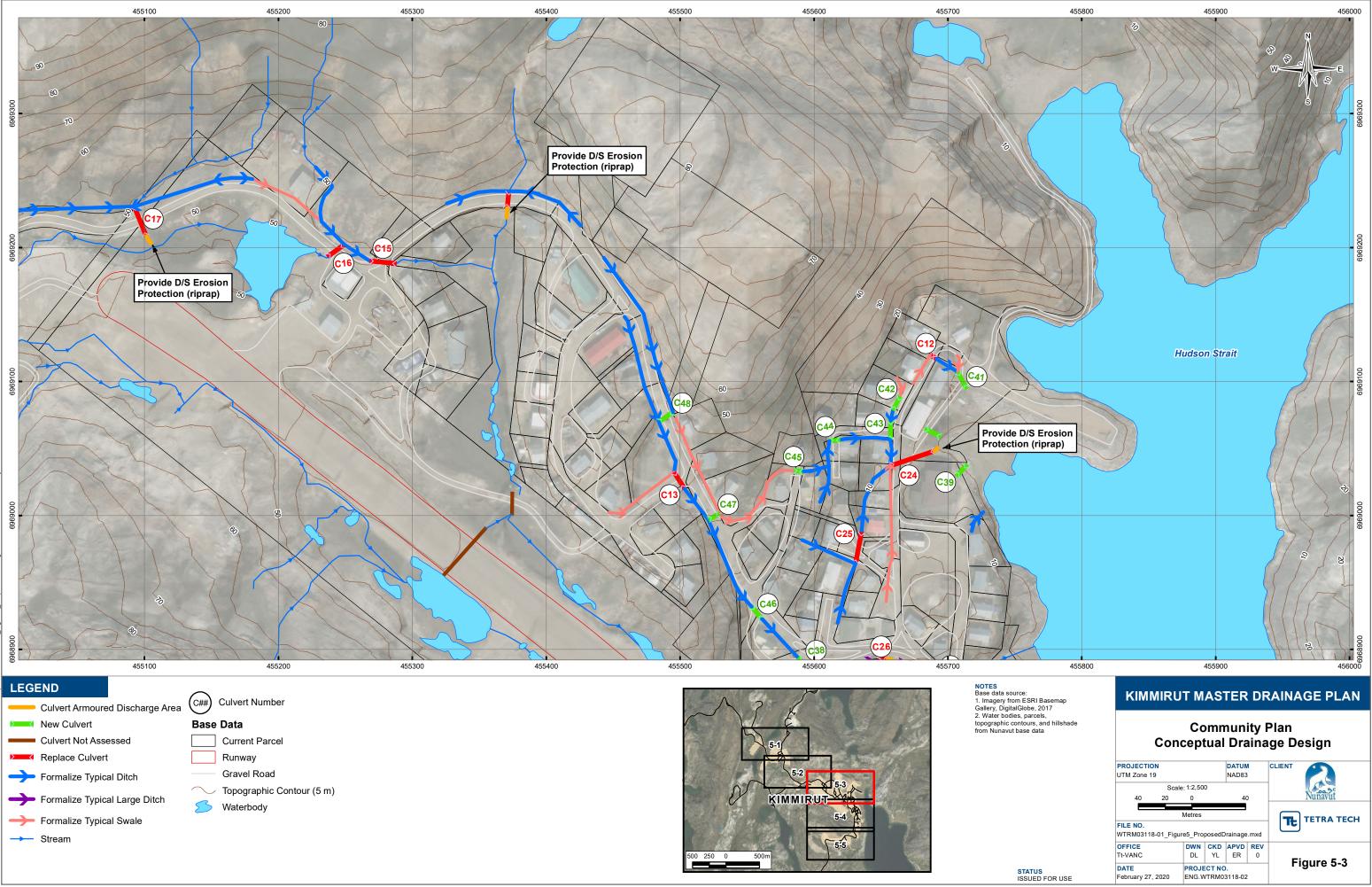


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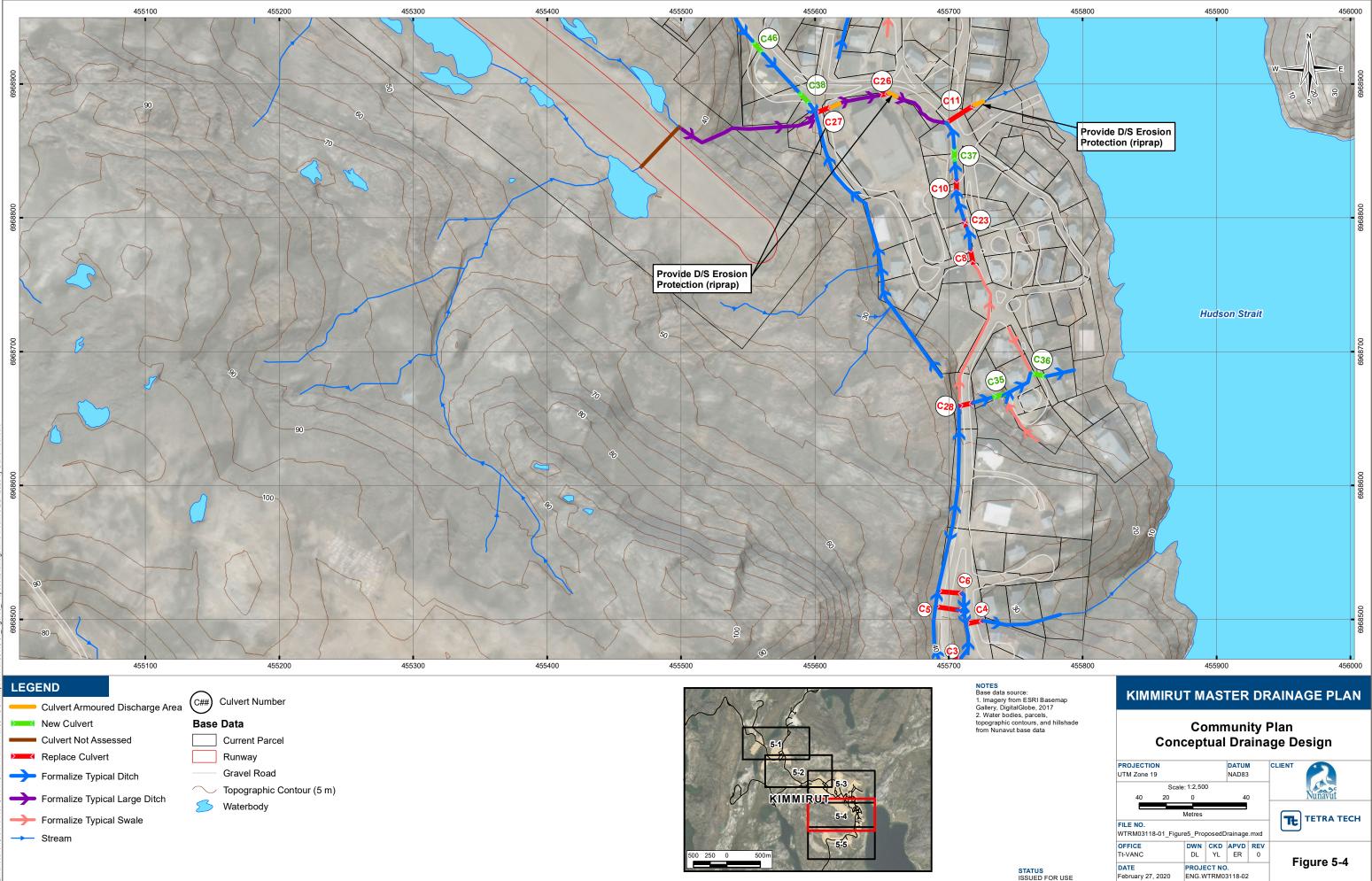
Figure 5-2

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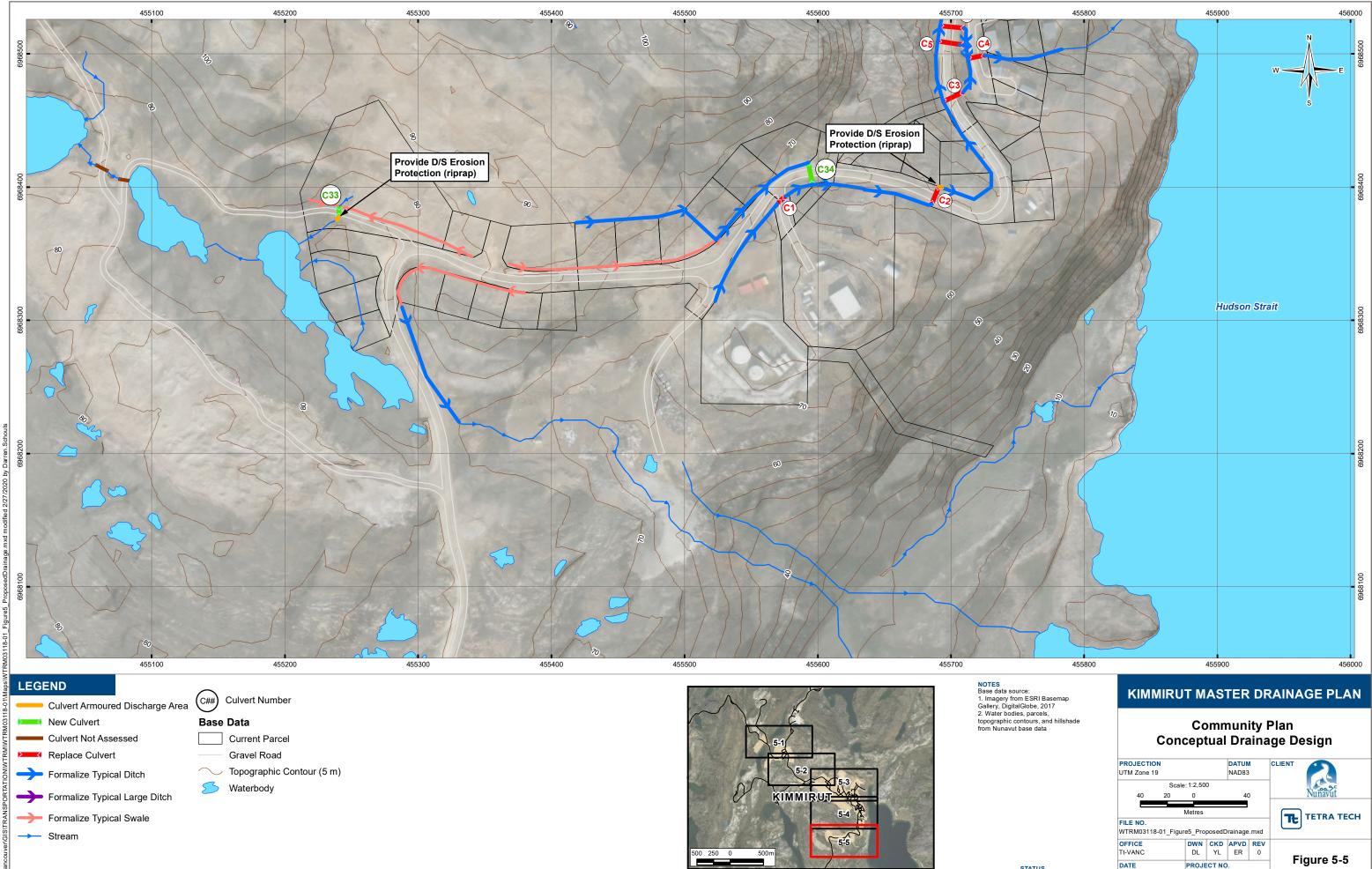
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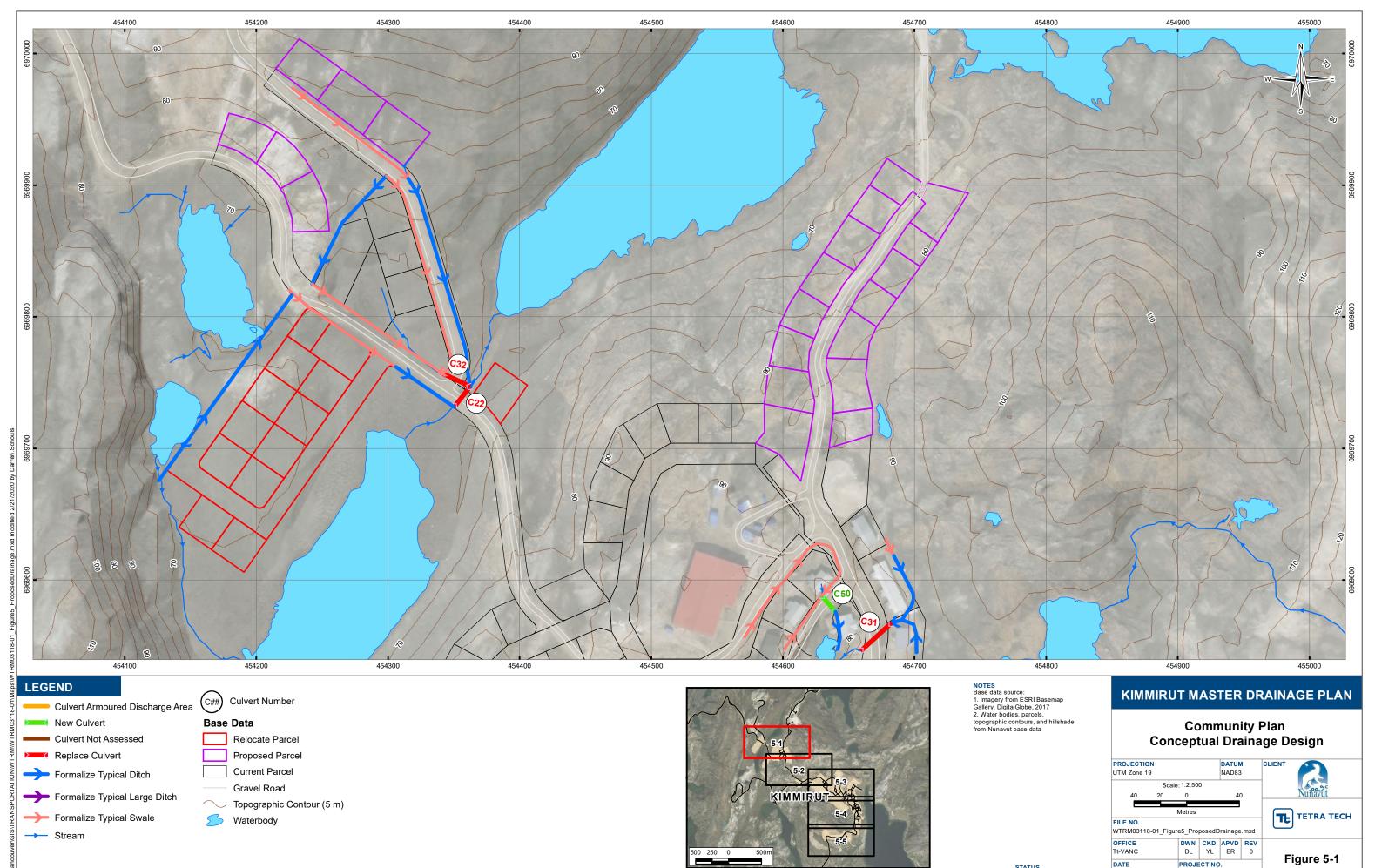


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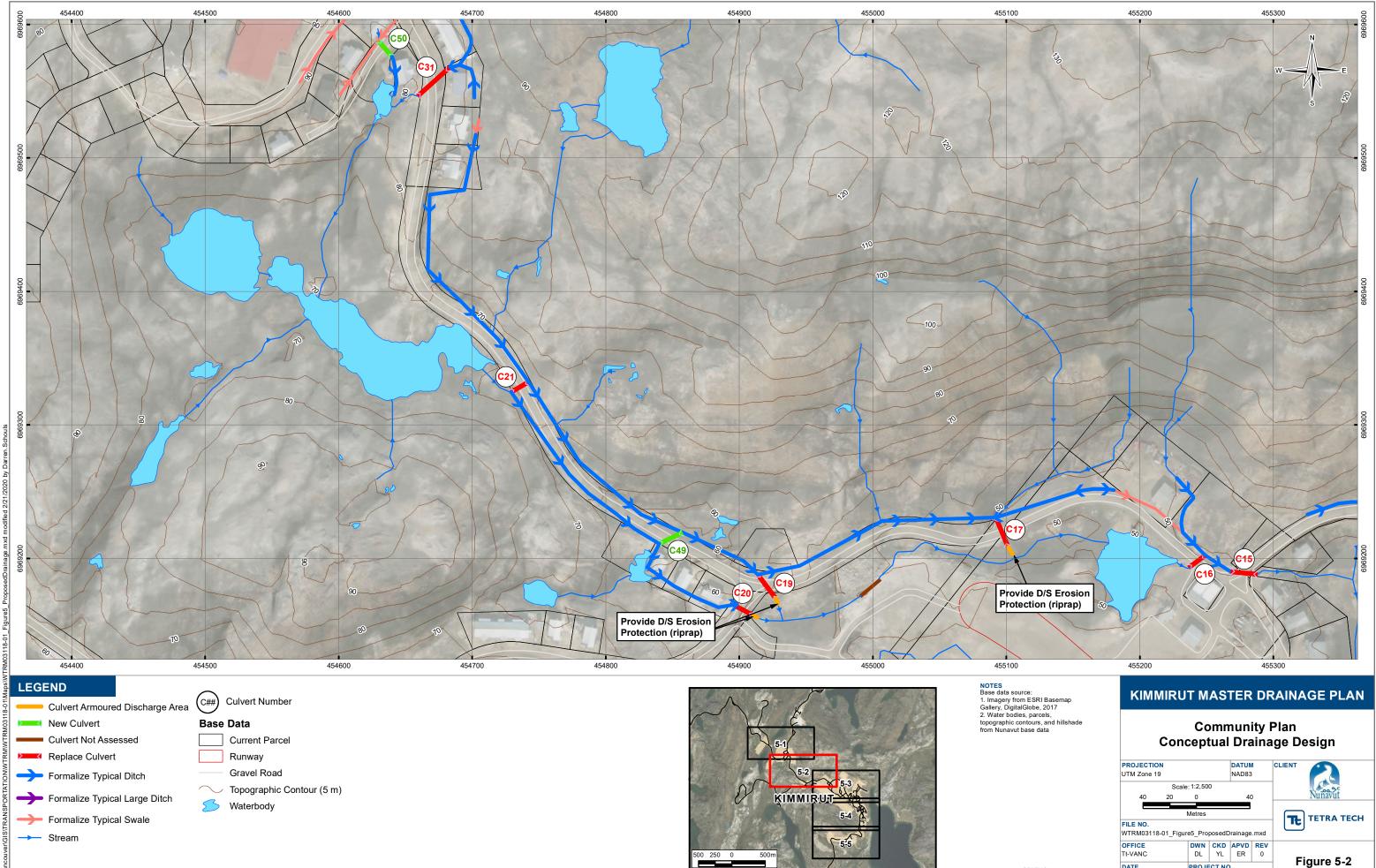
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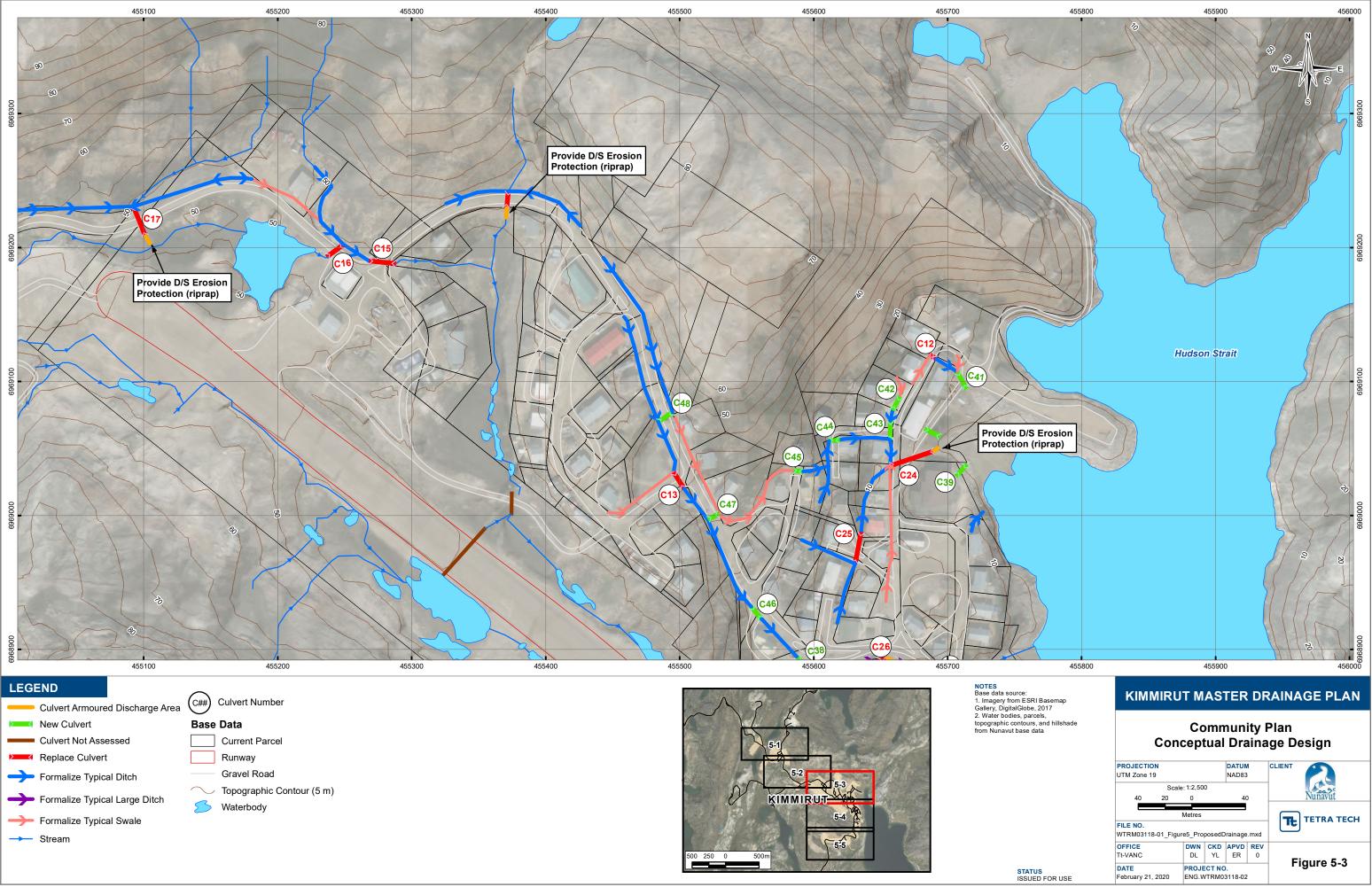


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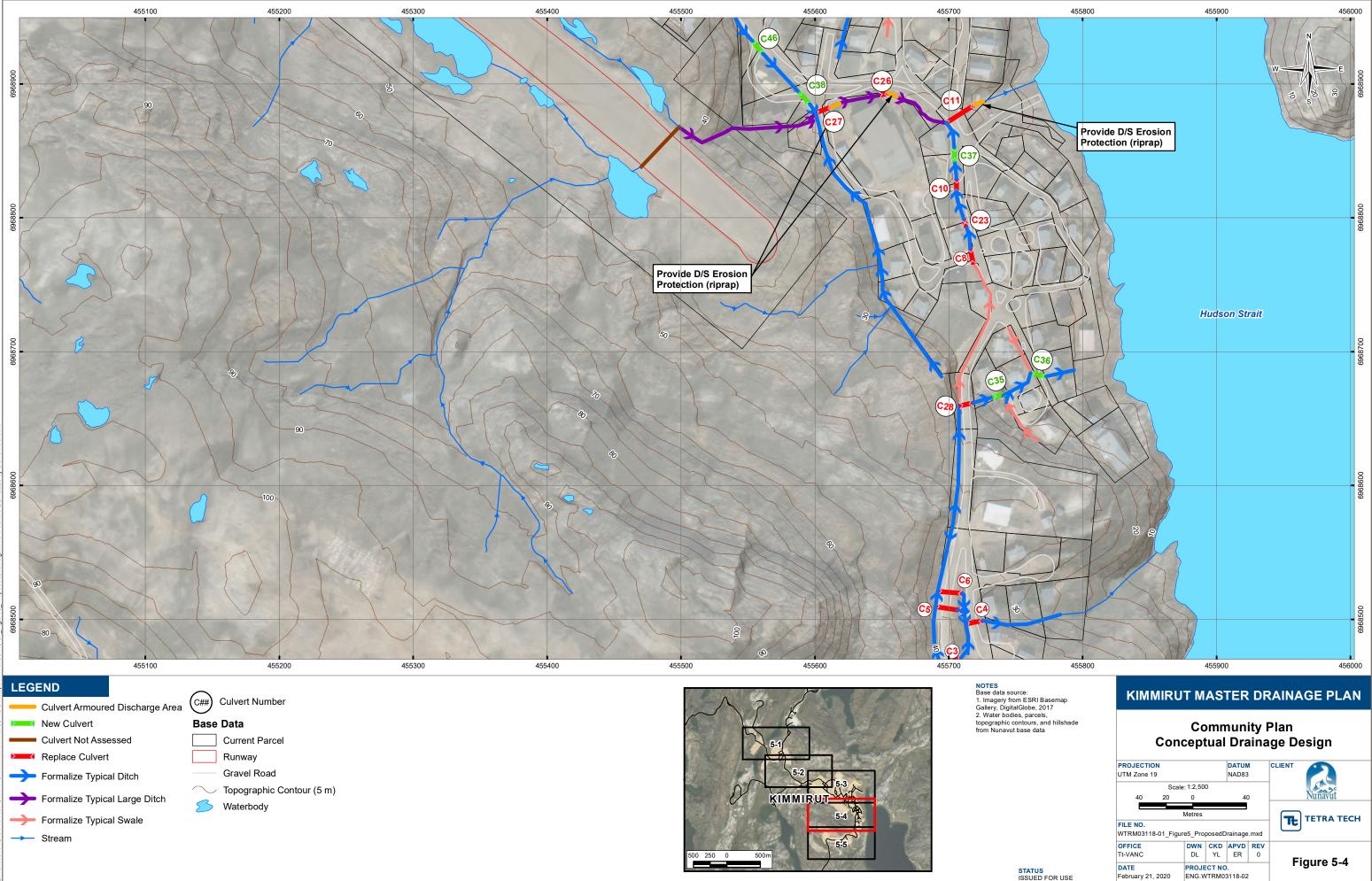
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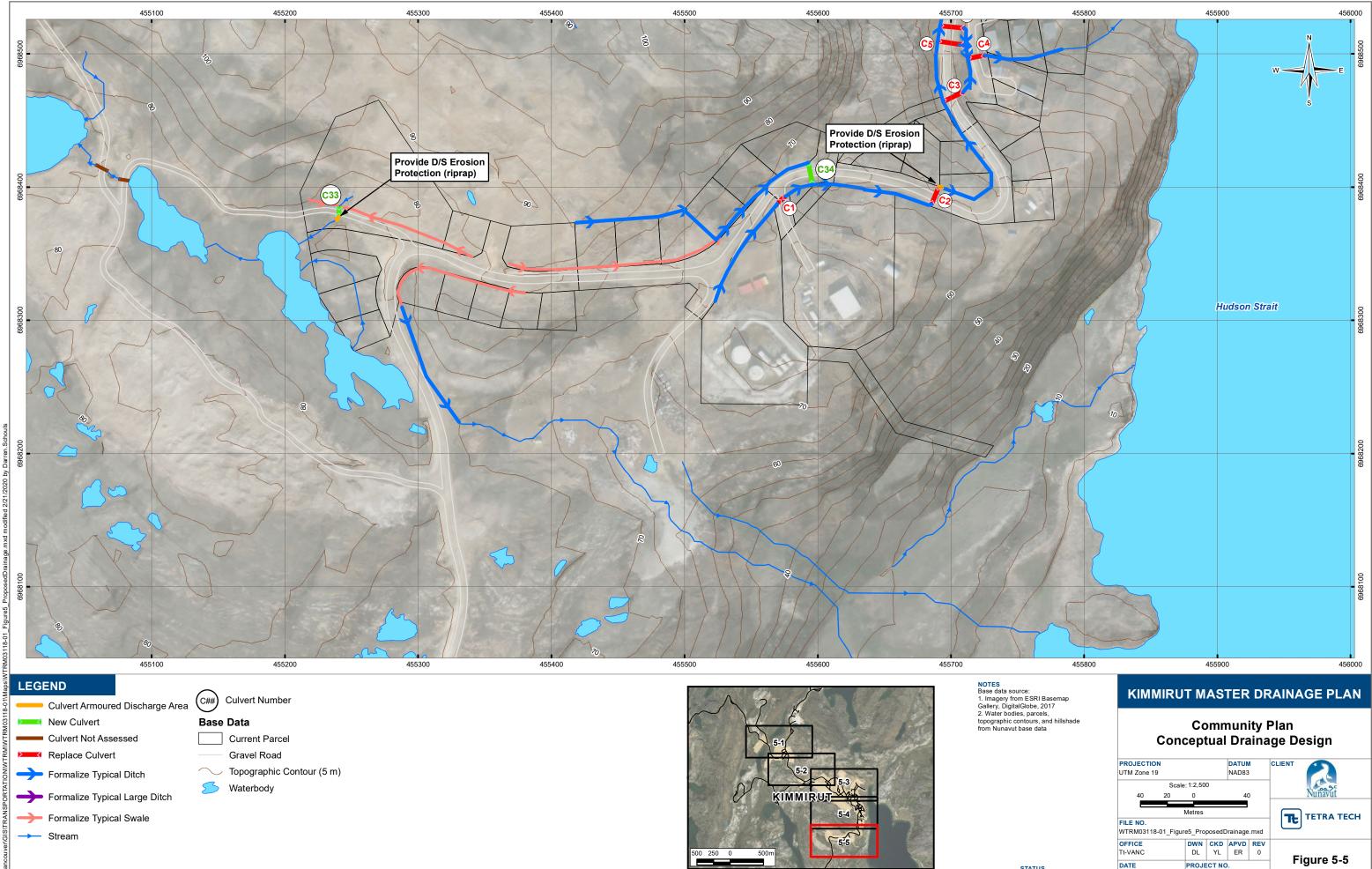
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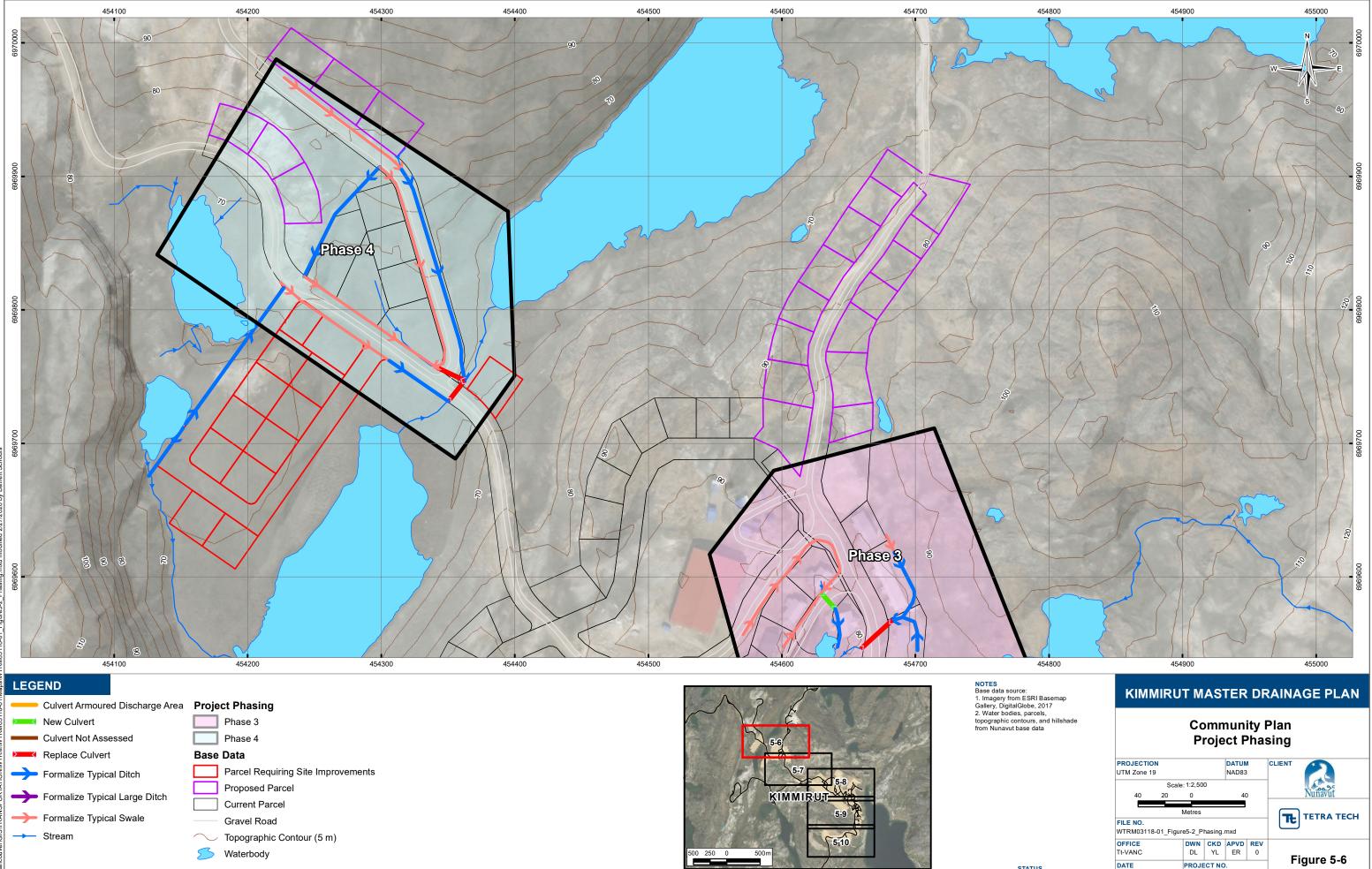
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## 5.2 Project Phasing

Tetra Tech has developed a staging plan allowing CGS and the Hamlet to first focus on the most important elements of our drainage plan and consider postponing some of the less critical aspects to future construction seasons. For each stage shown below in Figures 5-6 to 5-10, we have developed a Class "D" cost estimate to assist in future budgeting (see Section 5.3 below).

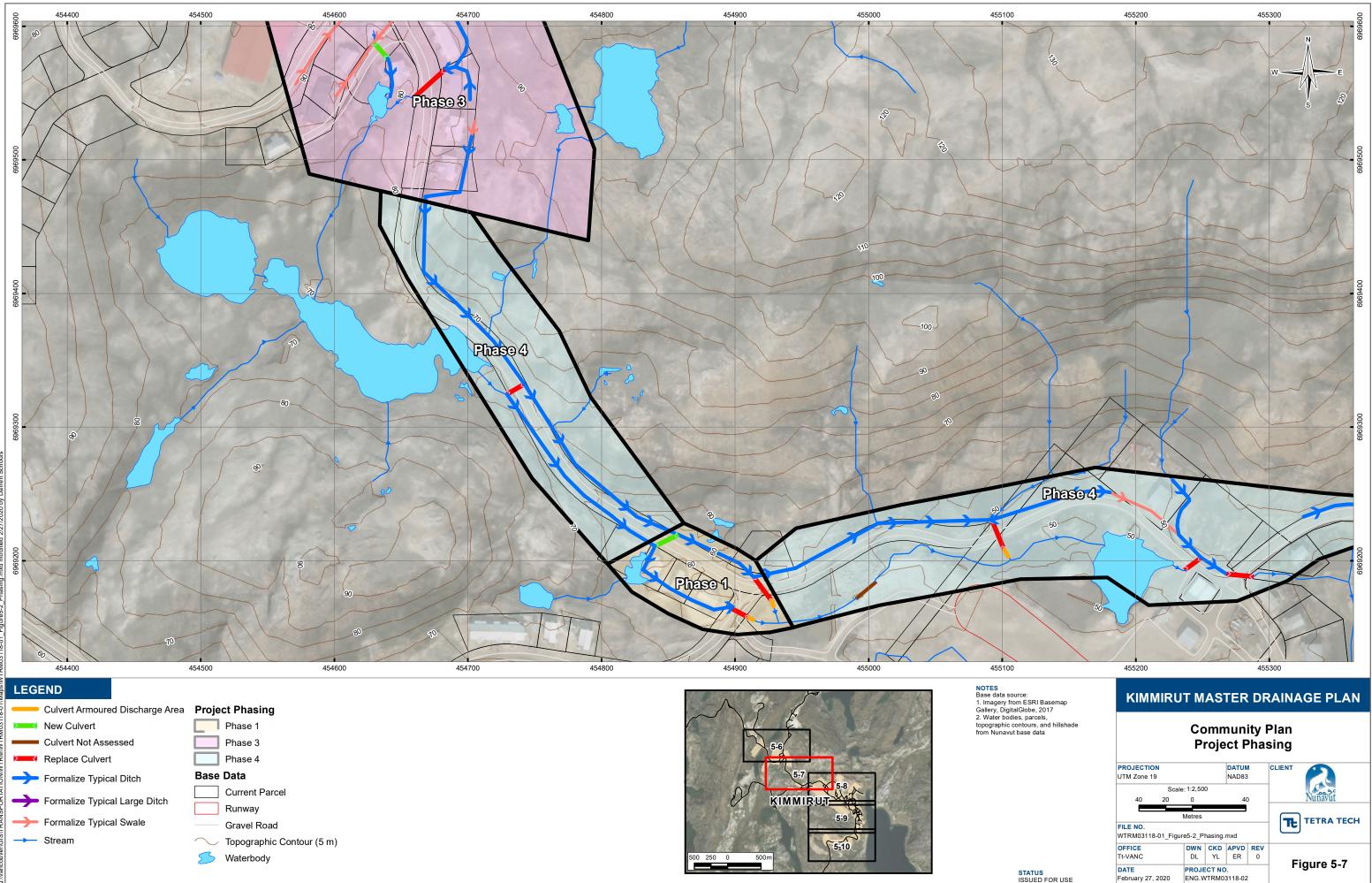




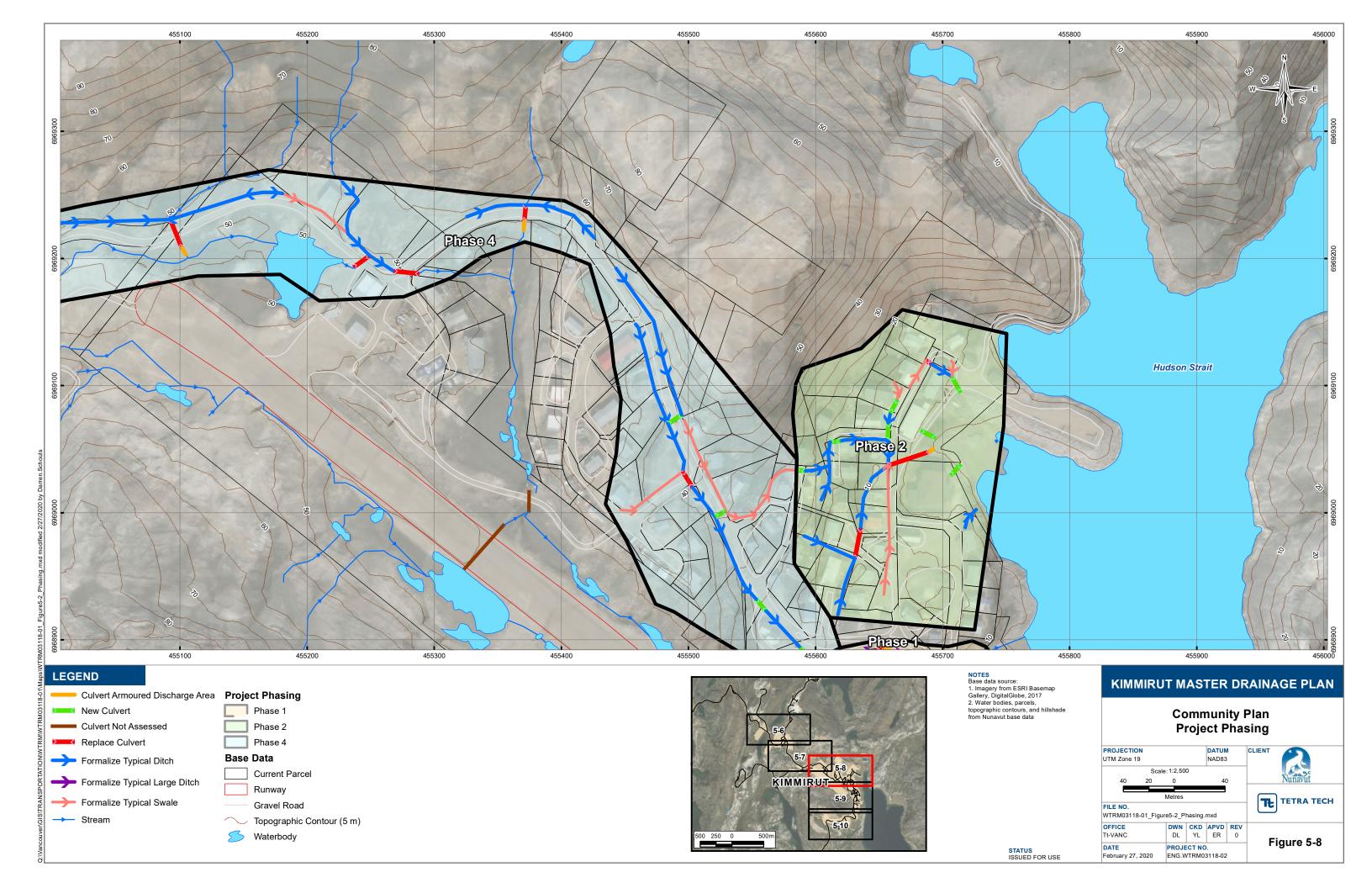
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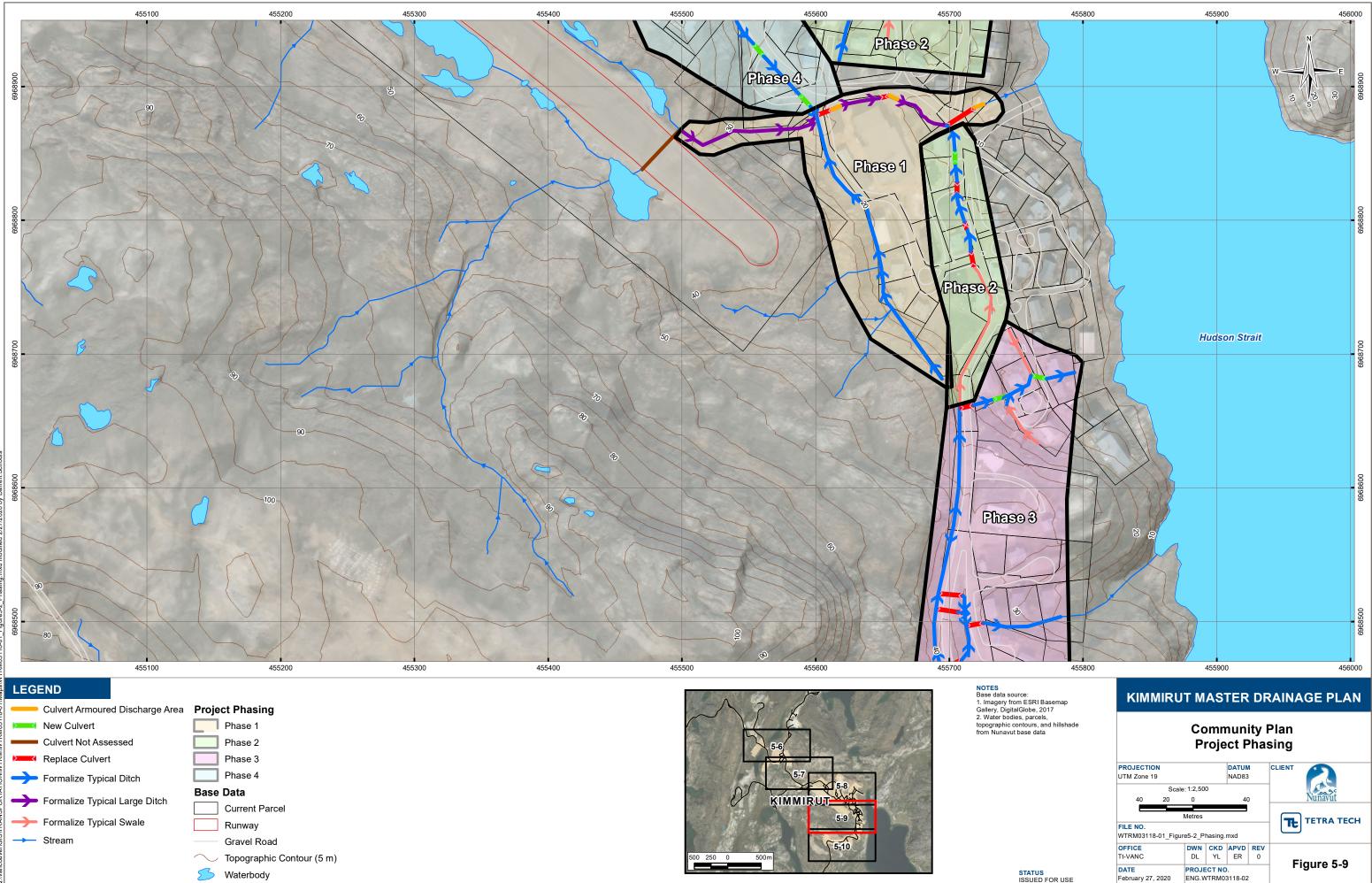
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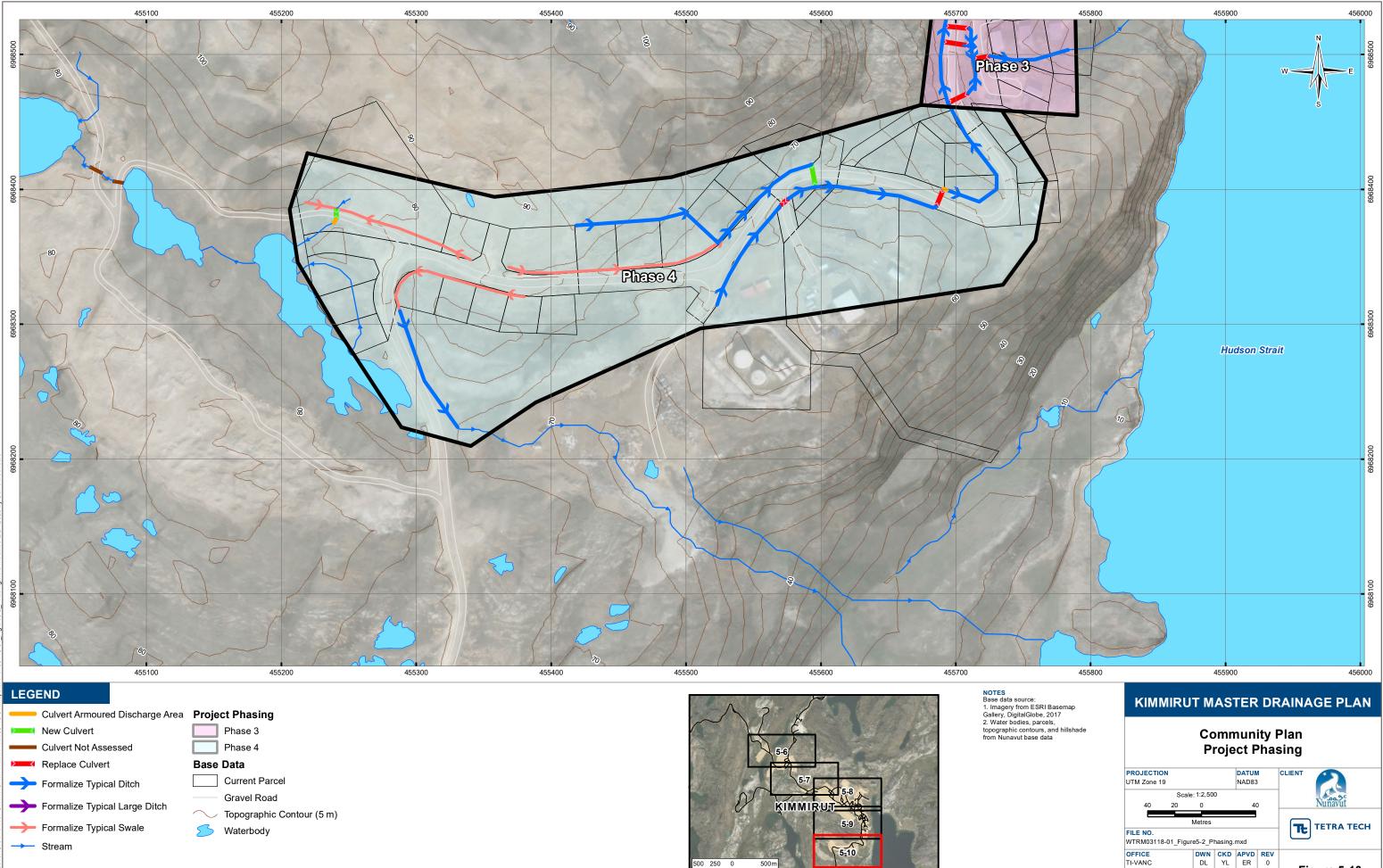


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Figure 5-10



### 5.3 Construction Cost Estimate

Construction of the Kimmirut Master Drainage Plan has been broken into four phases, with Phase 1 having the highest priority, and Phase 4 having the lowest priority.

A Class "D" cost estimate has been made for each phase. The cost estimates are included in Appendix D. A summary of the cost estimates is shown in Table 5-1 below. Additionally, a summary of the drainage materials required for each phase is presented in Table 5-2 below.

Phasing has been broken down to distribute the cost over a longer period of time to accommodate the availability of annual budgets. Combining phases will translate into greater savings as it will allow the GN to take advantage of the economy of scale.

|                                   |       | 1         | Phase     |           |             |             |  |  |  |  |  |
|-----------------------------------|-------|-----------|-----------|-----------|-------------|-------------|--|--|--|--|--|
|                                   |       | 1         | 2         | 3         | 4           | Total       |  |  |  |  |  |
| Preliminaries                     |       | \$58,252  | \$47,274  | \$48,110  | \$89,335    | \$242,972   |  |  |  |  |  |
| Civil Works                       |       | \$303,524 | \$193,736 | \$202,104 | \$614,351   | \$1,313,715 |  |  |  |  |  |
| Miscellaneous                     |       | \$15,000  | \$15,000  | \$15,000  | \$15,000    | \$60,000    |  |  |  |  |  |
| Sub-total                         |       | \$376,776 | \$256,010 | \$265,214 | \$718,686   | \$1,616,687 |  |  |  |  |  |
| Project Contingencies             | 40.0% | \$150,711 | \$106,086 | \$287,474 | \$646,675   | \$712,059   |  |  |  |  |  |
| Total Estimated Construction Cost |       | \$527,487 | \$358,413 | \$371,300 | \$1,006,161 | \$2,263,361 |  |  |  |  |  |

### Table 5-1: Summary of Cost Estimate



| Table 5-2. Summary of Required Dramage Materials |              |                 |       |              |         |       |              |         |       |              |       |       |              |       |       |
|--|--------------|-----------------|-------|--------------|---------|-------|--------------|---------|-------|--------------|-------|-------|--------------|-------|-------|
|  | F            | Phase 1 Phase 2 |       |              | Phase 3 |       |              | Phase 4 |       |              | Total |       |              |       |       |
| ltem   | Est Quantity | Unit            | Count | Est Quantity | Unit    | Count | Est Quantity | Unit    | Count | Est Quantity | Unit  | Count | Est Quantity | Unit  | Count |
| 450 mm<br>Culvert                                | 20           | m               | 1     | 152          | m       | 13    | 69           | m       | 5     | 131          | m     | 9     | 372          | m     | 28    |
| 600 mm<br>Culvert                                | 24           | m               | 1     | 36           | m       | 1     | 71           | m       | 3     | 66           | m     | 5     | 197          | m     | 10    |
| 750 mm<br>Culvert                                | 17           | m               | 1     |              | m       |       | 14           | m       | 1     | 20           | m     | 1     | 51           | m     | 3     |
| 900 mm<br>Culvert                                |              | m               |       |              | m       |       |              | m       |       | 25           | m     | 1     | 24           | m     | 1     |
| 1400 mm<br>Culvert                               | 46           | m               | 3     |              | m       |       |              | m       |       |              | m     |       | 46           | m     | 3     |
| Total New<br>Culverts                            | 107          | m               | 6     | 188          | m       | 14    | 154          | m       | 9     | 242          | m     | 16    | 690          | m     | 45    |
| 50 kg Class<br>Riprap                            | 238          | cu. m           |       | 20           | cu. m   |       | 0            | cu. m   |       | 52           | cu. m |       | 310          | cu. m |       |
| 10 kg Class<br>Riprap                            | 728          | cu. m           |       | 403          | cu. m   |       | 511          | cu. m   |       | 2,321        | cu. m |       | 3963         | cu. m |       |
| 50 – 75 mm<br>Clear Crush                        | 0            | cu. m           |       | 31           | cu. m   |       | 33           | cu. m   |       | 167          | cu. m |       | 231          | cu. m |       |
| Non-Woven<br>Geotextile                          | 2733         | sq. m           |       | 1,364        | sq. m   |       | 1,730        | sq. m   |       | 8,368        | sq. m |       | 14,195       | sq. m |       |
| Culvert<br>Removal                               | 86           | m               | 5     | 94           | m       | 6     | 111          | m       | 6     | 161          | m     | 10    | 460          | m     | 27    |

### Table 5-2: Summary of Required Drainage Materials

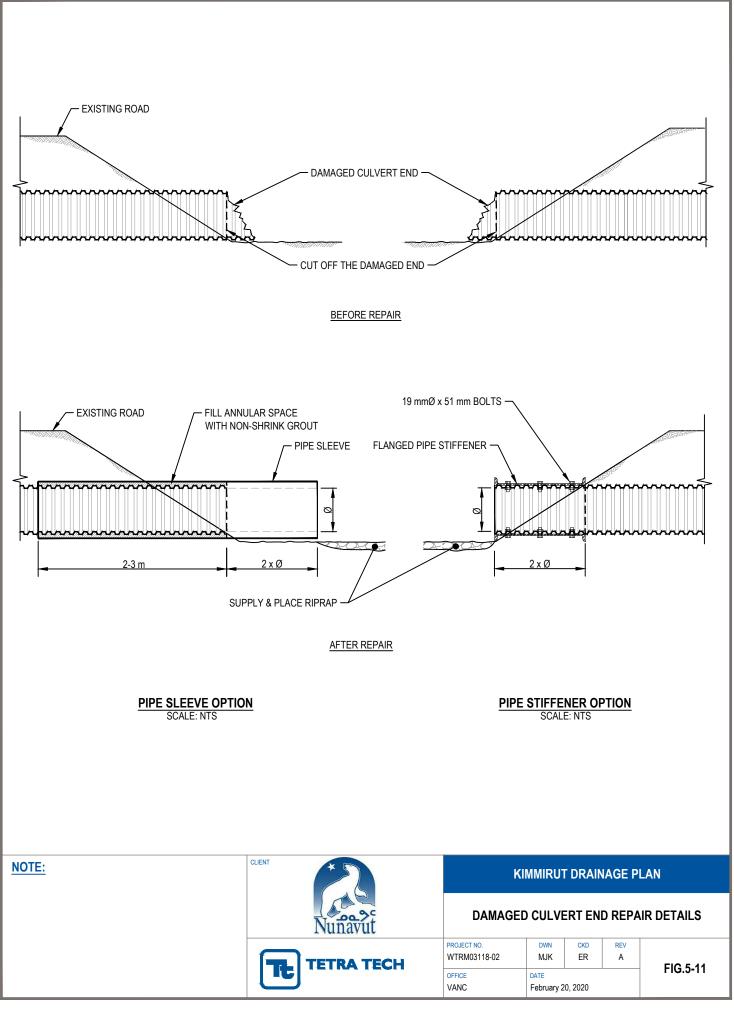
## 5.4 Ongoing System Maintenance

A properly maintained and monitored community drainage system is an important part of maintaining the safety and well-being of the community. To ensure proper functioning of the drainage system, a program to maintain and monitor the drainage system should be implemented.

### 5.4.1 Culvert Maintenance and Repair

As per the guidelines for community drainage system planning, design, and maintenance in northern communities (CSA Group, 2015), culvert maintenance and repair guidelines are as follows:

- Culverts should be marked with a post painted in a bright colour and installed at the precise location of the culvert end. Culvert marking posts, when lost or damaged, shall be replaced.
- Spare culverts of each size shall be kept on hand to facilitate the repair and replacement of all sizes of culverts.
- Where the culverts are in good shape and only the ends are damaged, a SWSP sleeve should be added to
  reinstate the original length of the culvert. The annular space between the existing pipe and the SWSP sleeve
  should be grouted and sealed. Figure 5-11 provides a sketch covering the proposed repairs.



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### 5.4.2 Snow Removal Management Plan

As per the guidelines for community drainage system planning, design, and maintenance in northern communities (CSA Group, 2015), snowmelt from removed snow should be prevented from re-entering the drainage system. Runoff from stockpiled snow can re-enter and overwhelm the drainage system and causing flooding damage.

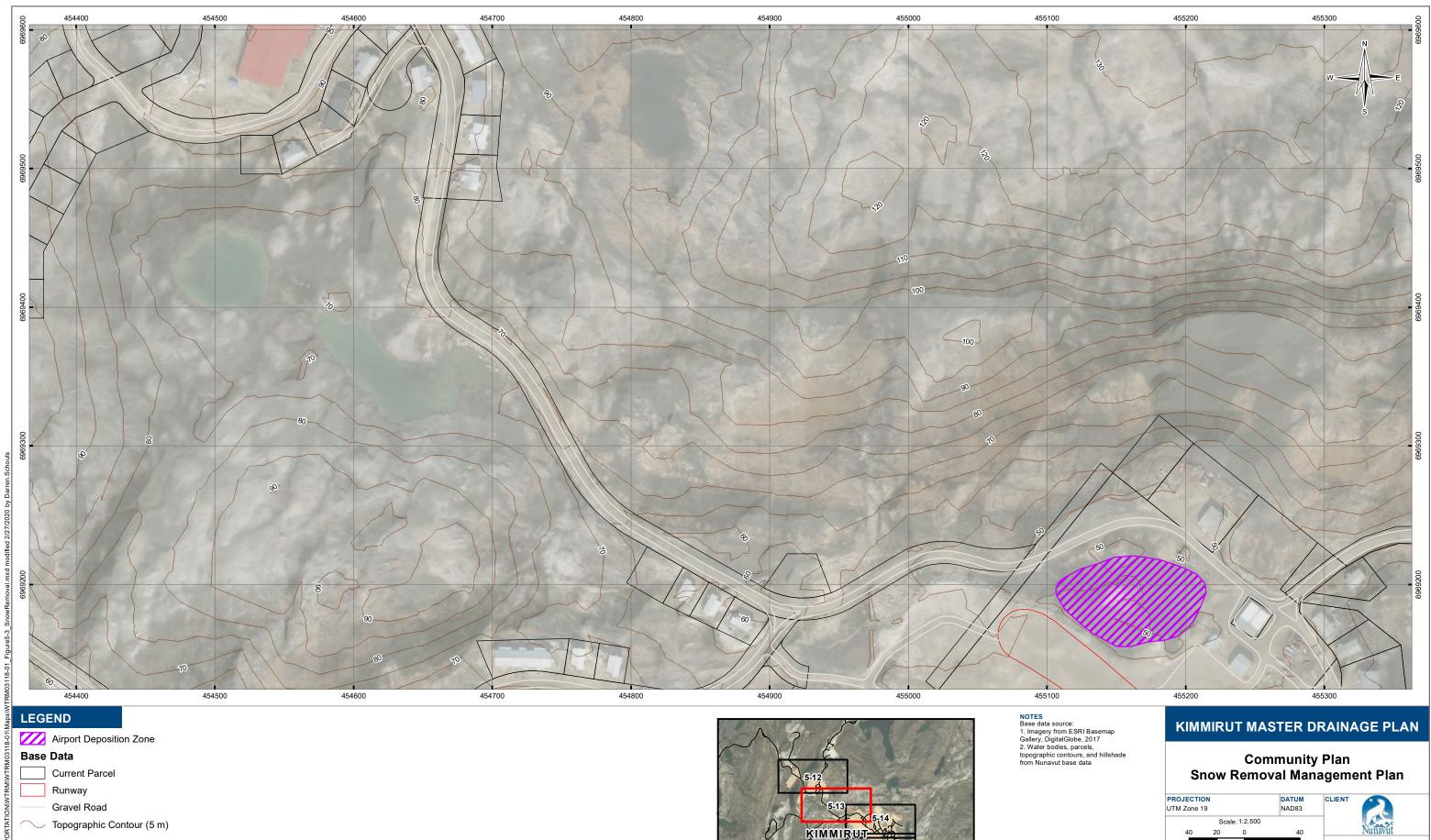
To that end, Tetra Tech has identified the following snow removal strategy:

- Removed snow from roadways and driveways can be safely deposited in one of the designated Deposition Zones as shown in Figures 5-12 to 5-16.
- Removed snow from the airport runway can be stored in one of the designated Airport Deposition Zones as shown in Figures 5-12 and 5-16.
- Removed snow from the airport runway shall not be stored along the east side of the runway as shown in Figure 5-14 and Figure 5-15.
- Airport maintenance staff shall continually monitor the snow accumulation to the northeast of the runway where snow damming can occur. Staff are advised to break the snow down with an excavator if damming occurs.



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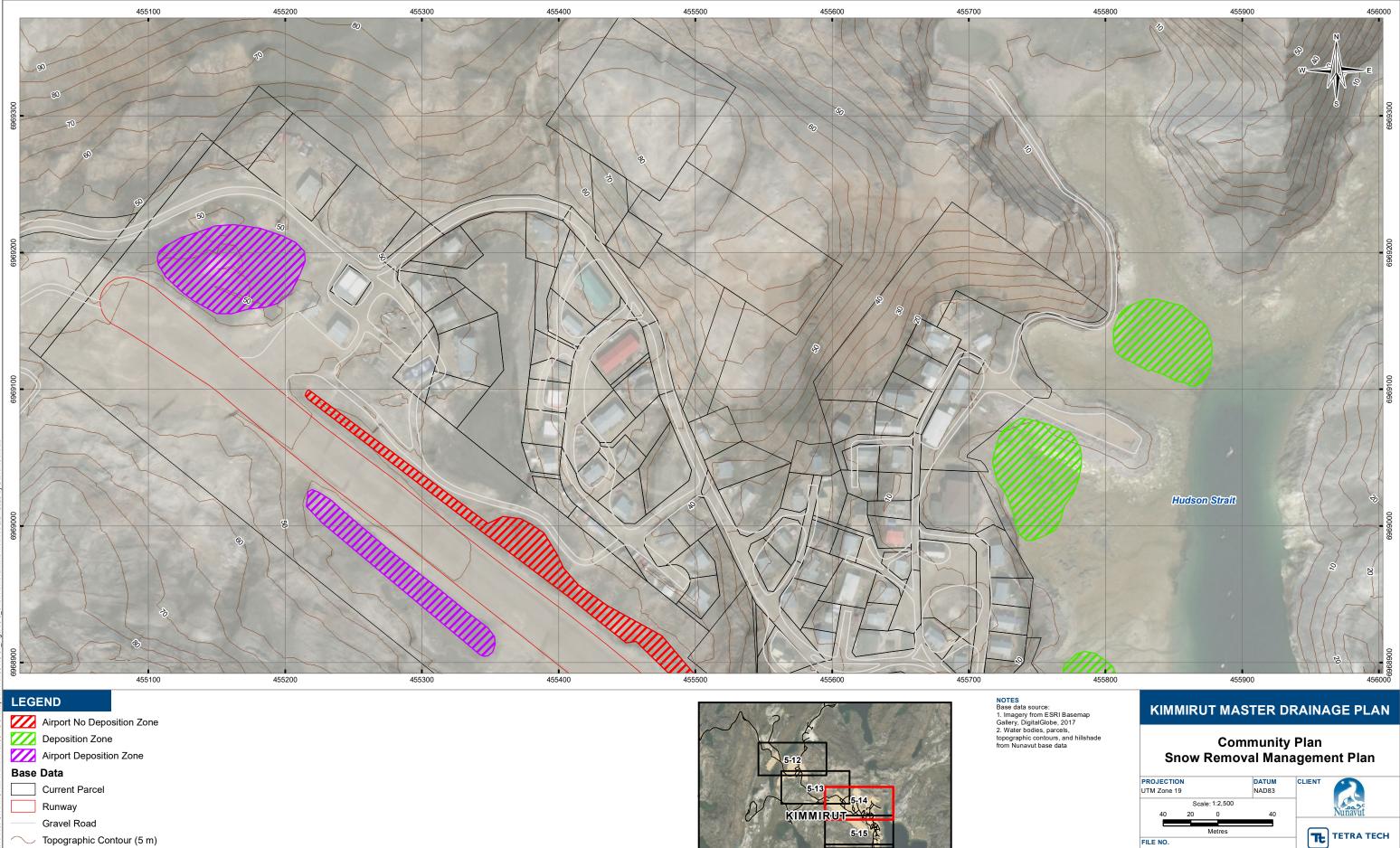


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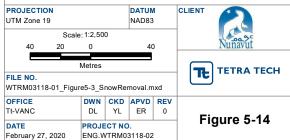
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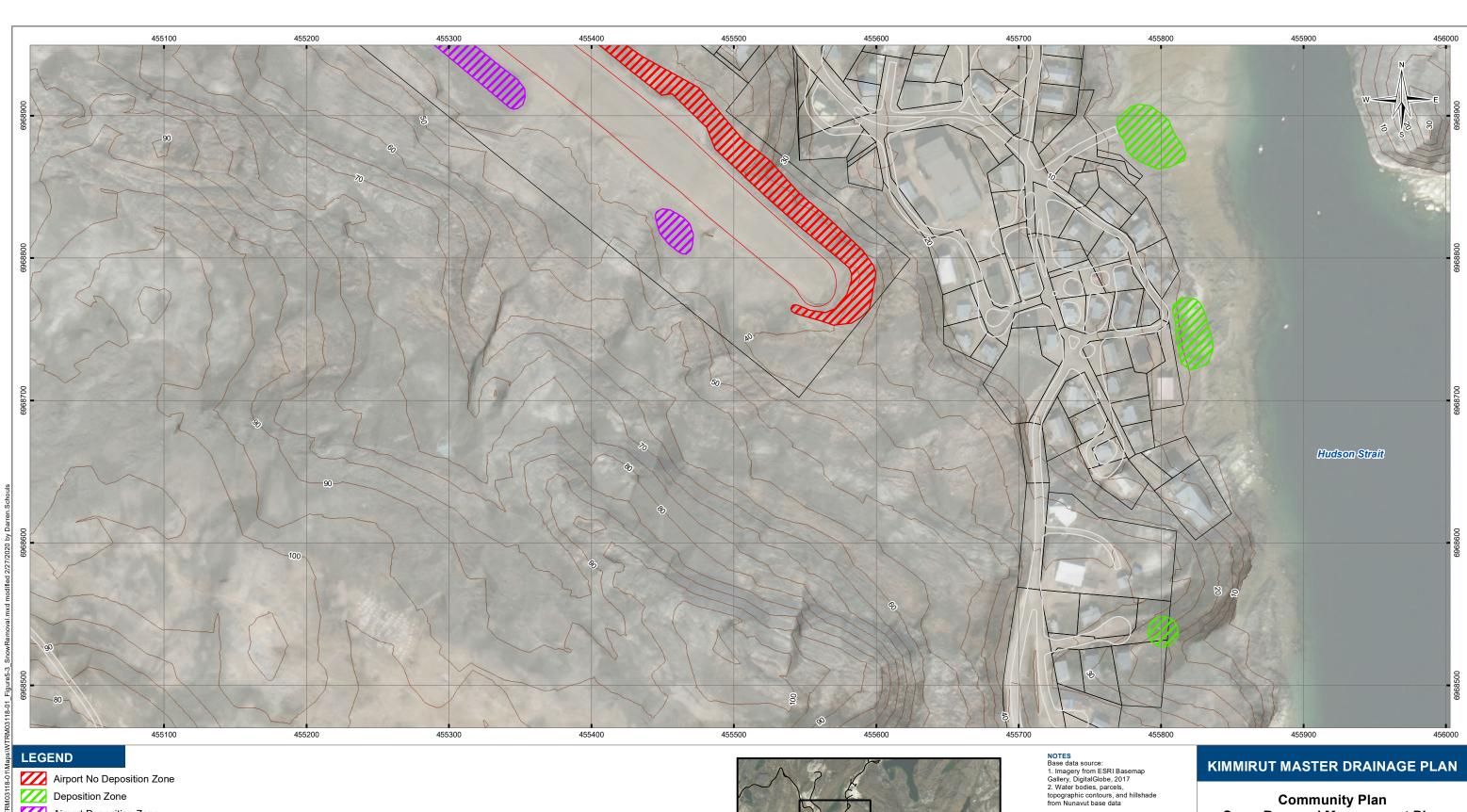
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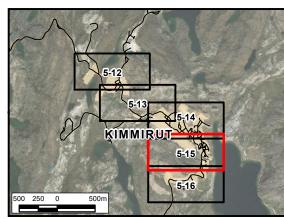
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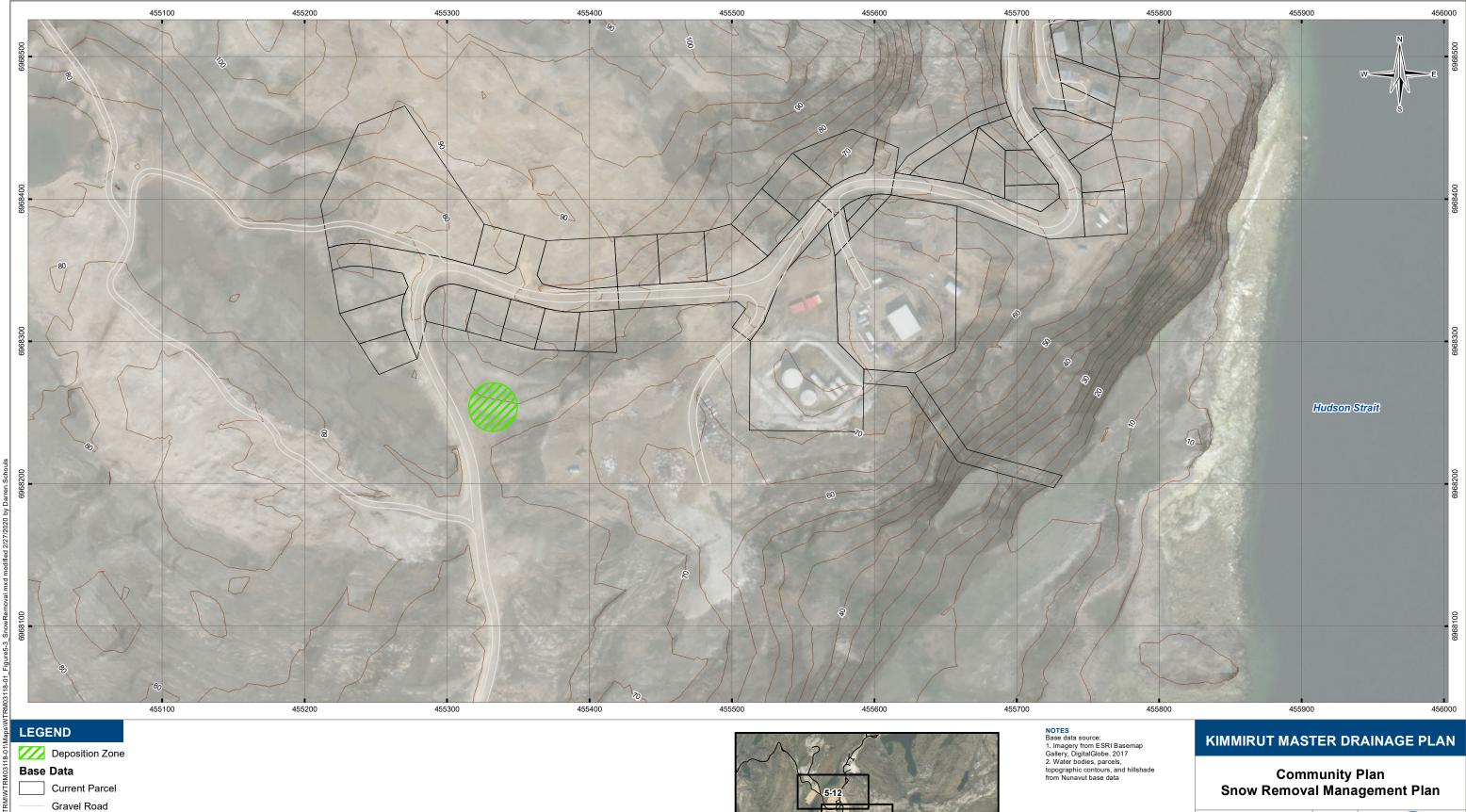
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  - Current Parcel
- Runway Gravel Road
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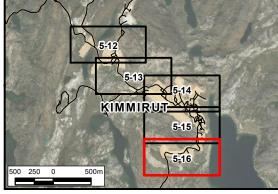
# Community Plan Snow Removal Management Plan

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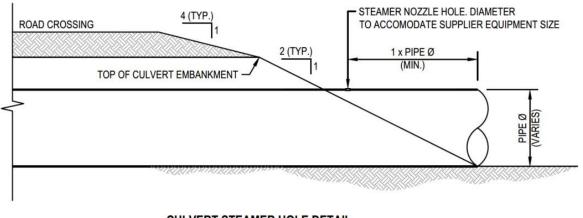
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### 5.4.3 Culvert Thawing

An annual maintenance program should incorporate a culvert thawing strategy. Some options for thawing culverts are presented in Appendix C for consideration. Figure 5-17 below shows the proposed method for thawing ice inside culverts.

As per the project phasing diagrams shown in Figures 5-6 to 5-10, higher priority culverts should be thawed first. For example, culverts in Phase 1 zones should be thawed before culverts in Phase 2 zones.



CULVERT STEAMER HOLE DETAIL SCALE: NTS Figure 5-17: Culvert Thawing Detail

### 5.4.4 Maintenance Schedule

A recommended seasonal maintenance schedule as per the guidelines for community drainage system planning, design, and maintenance in northern communities (CSA Group, 2015), is presented as follows:

### Spring:

- Visually inspect and thaw frozen culverts in order of their priority level, as discussed in Section 5.4.3. Note any damages to culverts.
- Remove debris from blocked or partially blocked culverts.
- Collect and dispose of litter if present.
- Following the spring Freshet, inspect the drainage system to identify deficiencies for repair.

### Summer:

- Repair washed out ditches, swales and riprap aprons as necessary. Ponding in ditches and swales should be identified and fixed by re-sloping the ditch.
- A water pump can be used to flush blocked culverts free of sediment, rocks, and debris. Discharge of sediments into natural streams should be avoided and appropriate sediment and erosion control measures should be incorporated to protect the receiving water bodies.





• Repair damaged culvert ends. Replace or re-install culverts that have shifted or moved. Repair culverts in order of their priority level and the level of damage observed.

### Fall:

- Complete repairs to the drainage system.
- Replace missing or damaged culvert marking posts.
- Create an inventory of materials required for the next year's maintenance program.

### Winter:

- Monitor culverts and culvert marking posts.
- Implement the snow removal management plan as detailed in Section 5.4.2.
- Monitor snow buildup beside the airport runway and remove snow as necessary to prevent snow damming.



## 6.0 CLOSURE

We trust this document meets your present requirements. If you have any questions or comments, please contact the undersigned.

### Respectfully submitted, Tetra Tech Canada Inc.



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> file: 704-TRN.WTRM03118-02 file: 704-TRN.WTRM03118-02

Reviewed by: David Moschini, P.Eng. Manager – Water Resources & Infrastructure Direct Line: 778.945.5798 David.Moschini@tetratech.com





### 7.0 REFERENCES

- Beckstead, G. & L.B. Smith (1985, September). Geotechnical and hydrological evaluation Proposed residential subdivisions Coppermine, N.W.T.. Thurber Consultants Itd. & Hydrocon Engineering (Continental) Ltd.
- CSA Group. (2015, January). Community drainage system planning, design, and maintenance in northern communities. CAN/CSA-S503-15. National Standard of Canada
- 3v Geomatics Inc. (2016, March 24). Nunavut Terrain Analysis Final Report 2015/16. Vancouver, BC, Canada.
- CBC News. (2012, May 7). *Flash flood hits Kimmirut, Nunavut.* Retrieved from CBC Radio Canada: https://www.cbc.ca/news/canada/north/flash-flood-hits-kimmirut-nunavut-1.1159428
- Kikkert, P. (2019, July 11). *Nunavut*. Retrieved from The Canadian Encyclopedia: https://www.thecanadianencyclopedia.ca/en/article/nunavut
- Lewis, J., & Miller, K. (2010). *Climate Change Adaptation Action Plan for Iqaluit.* Retrieved from Canadian Institute of Planners: https://www.cip-icu.ca/Files/Resources/IQALUIT\_REPORT\_E
- Simonovic, S., Schardong, A., Gaur, A., & Sandink, D. (2018). *IDF curves for ungauged locations Canada*. Retrieved from Computerized IDF CC Tool for the Development of Intensity-Duration-Frequency Curves under a Changing Climate: www.idf-cc-uwo.ca/idfgrid
- The Prairie Climate Centre. (2019, July 10). *Find & Display Local Data*. Retrieved from The Climate Atlas of Canada: https://climateatlas.ca/



# APPENDIX A

## TETRA TECH'S LIMITATIONS ON THE USE OF THIS DOCUMENT



### HYDROTECHNICAL

### 1.1 USE OF DOCUMENT AND OWNERSHIP

This document pertains to a specific site, a specific development, and a specific scope of work. The document may include plans, drawings, profiles and other supporting documents that collectively constitute the document (the "Professional Document").

The Professional Document is intended for the sole use of TETRA TECH's Client (the "Client") as specifically identified in the TETRA TECH Services Agreement or other Contractual Agreement entered into with the Client (either of which is termed the "Contract" herein). TETRA TECH does not accept any responsibility for the accuracy of any of the data, analyses, recommendations or other contents of the Professional Document when it is used or relied upon by any party other than the Client, unless authorized in writing by TETRA TECH.

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Both electronic file and/or hard copy versions of TETRA TECH's Instruments of Professional Service shall not, under any circumstances, be altered by any party except TETRA TECH. TETRA TECH's Instruments of Professional Service will be used only and exactly as submitted by TETRA TECH.

Electronic files submitted by TETRA TECH have been prepared and submitted using specific software and hardware systems. TETRA TECH makes no representation about the compatibility of these files with the Client's current or future software and hardware systems.

### **1.3 STANDARD OF CARE**

Services performed by TETRA TECH for the Professional Document have been conducted in accordance with the Contract, in a manner consistent with the level of skill ordinarily exercised by members of the profession currently practicing under similar conditions in the jurisdiction in which the services are provided. Professional judgment has been applied in developing the conclusions and/or recommendations provided in this Professional Document. No warranty or guarantee, express or implied, is made concerning the test results, comments, recommendations, or any other portion of the Professional Document.

If any error or omission is detected by the Client or an Authorized Party, the error or omission must be immediately brought to the attention of TETRA TECH.

### **1.4 DISCLOSURE OF INFORMATION BY CLIENT**

The Client acknowledges that it has fully cooperated with TETRA TECH with respect to the provision of all available information on the past, present, and proposed conditions on the site, including historical information respecting the use of the site. The Client further acknowledges that in order for TETRA TECH to properly provide the services contracted for in the Contract, TETRA TECH has relied upon the Client with respect to both the full disclosure and accuracy of any such information.

### **1.5 INFORMATION PROVIDED TO TETRA TECH BY OTHERS**

During the performance of the work and the preparation of this Professional Document, TETRA TECH may have relied on information provided by third parties other than the Client.

While TETRA TECH endeavours to verify the accuracy of such information, TETRA TECH accepts no responsibility for the accuracy or the reliability of such information even where inaccurate or unreliable information impacts any recommendations, design or other deliverables and causes the Client or an Authorized Party loss or damage.

### **1.6 GENERAL LIMITATIONS OF DOCUMENT**

This Professional Document is based solely on the conditions presented and the data available to TETRA TECH at the time the data were collected in the field or gathered from available databases.

The Client, and any Authorized Party, acknowledges that the Professional Document is based on limited data and that the conclusions, opinions, and recommendations contained in the Professional Document are the result of the application of professional judgment to such limited data.

The Professional Document is not applicable to any other sites, nor should it be relied upon for types of development other than those to which it refers. Any variation from the site conditions present, or variation in assumed conditions which might form the basis of design or recommendations as outlined in this report, at or on the development proposed as of the date of the Professional Document requires a supplementary exploration, investigation, and assessment.

TETRA TECH is neither qualified to, nor is it making, any recommendations with respect to the purchase, sale, investment or development of the property, the decisions on which are the sole responsibility of the Client.



### **1.7 ENVIRONMENTAL AND REGULATORY ISSUES**

Unless expressly agreed to in the Services Agreement, TETRA TECH was not retained to investigate, address or consider, and has not investigated, addressed or considered any environmental or regulatory issues associated with the project.

### **1.8 LEVEL OF RISK**

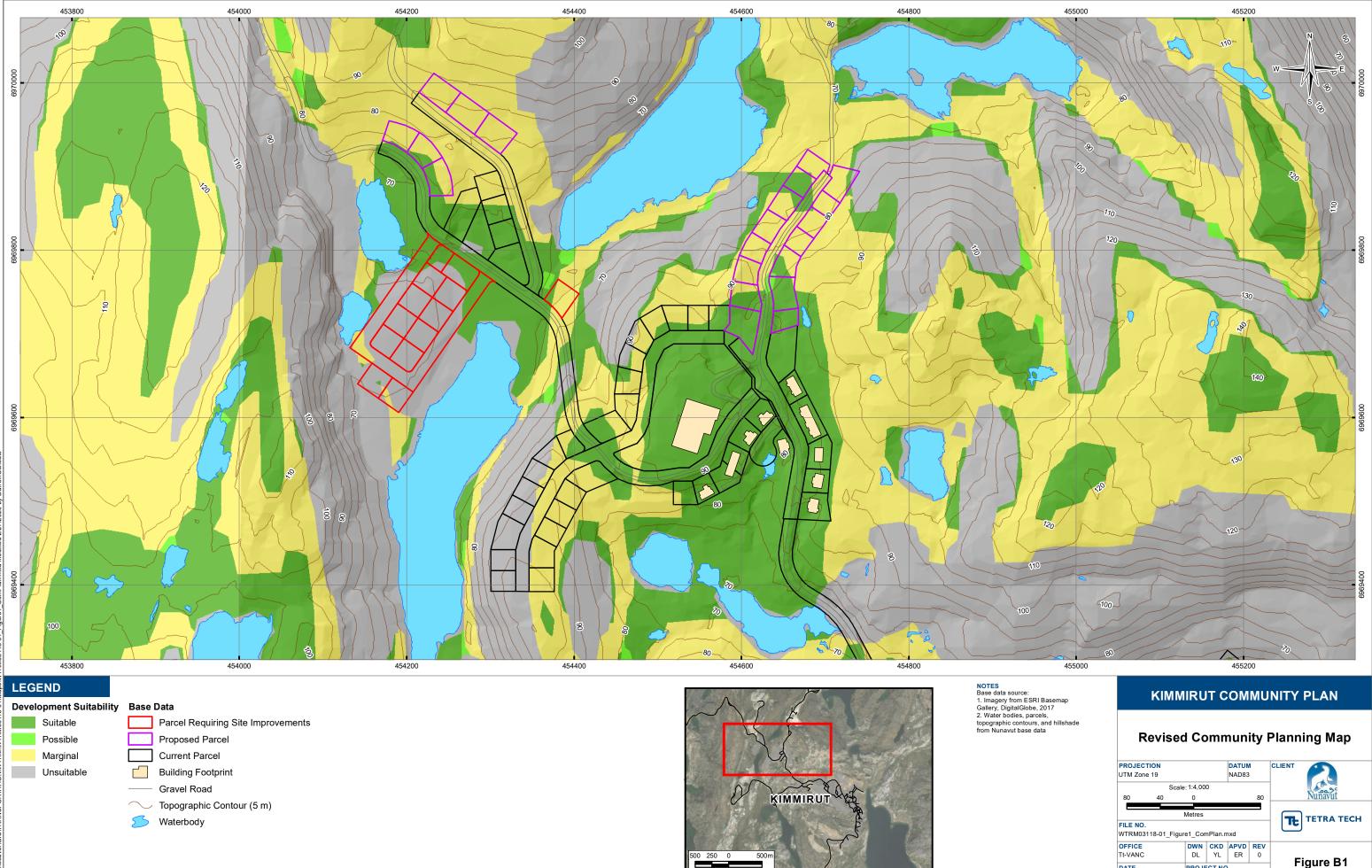
It is incumbent upon the Client and any Authorized Party, to be knowledgeable of the level of risk that has been incorporated into the project design, in consideration of the level of the hydrotechnical information that was reasonably acquired to facilitate completion of the design.



## APPENDIX B

## **COMMUNITY PLANS AND BYLAW NO. 127**





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# **SCHEDULE 1 - COMMUNITY PLAN**

### SECTION 1 INTRODUCTION

### 1.1 Purpose of the Plan

The purpose of the Kimmirut Community Plan is to outline Council's policies for managing the physical development of the Hamlet for the next 20 years - to 2034. The Community Plan was created through a community consultation process and reflects the needs and desires of the Community. The Community Plan builds on previous plans, while incorporating new challenges, issues and needs identified by the Community.

### 1.2 Goals of the Community Plan

Community Plan policies emerge from the values of a community and its vision of how it would like to grow. The goals established for this Community Plan are:

1. To develop in an orderly fashion creating a safe, healthy, functional, and attractive community that reflects community values and culture.

- To promote the Plan as a tool for making effective and consistent decisions regarding land use and development in the community.
   To ensure an adequate supply of land for all types of uses to support the growth and change of the community.
- 4. To build upon community values of participation and unity to support community projects and local economic development.
- 5. To protect the natural beauty of "Nuna", protect viewpoints to the water, and retain waterfront and lakeshore areas for public uses and traditional activities.

### 1.3 Administration of the Plan

The Community Plan is enacted by By-law. Changes to the Plan can be made by amending the By-laws in accordance with the *Nunavut Planning Act*. The Community Plan should be reviewed and updated every five years as required by the *Nunavut Planning Act*. A Zoning By-law is also being enacted for the purpose of implementing detailed policies based on the Community Plan. All development must follow the intent of the Community Plan and Zoning By-law. The Community Plan includes Schedule 1 (Plan Policy Text), Schedule 2 (Community Plan and Zoning Map) and Schedule 3 (General Land Use Map).

### SECTION 2. COMMUNITY GROWTH AND PHASING POLICIES

At the time of preparation of this Plan, the population of Kimmirut was approximately 455 people. This Plan is based on a future population of 591 people by 2034. It is estimated that an additional 67 dwelling units will be required to meet the projected population growth, representing the need for approximately 3 hectares of land for residential development. In addition, an appropriate mix and range of industrial, commercial, and community uses has been proposed to meet long-term needs. The policies of Council are:

### a) Plan for a 2034 population of 591.

b) Identify sufficient land on the Community Plan to meet the needs of the projected 2034 population.
c) Review the Community Plan in 5 years, in 2019, to re-assess actual rates of growth and community needs.
d) Council will generally phase new land development as follows:

i.) <u>2014 - 2019:</u>

- Develop existing vacant lots within the Arena Subdivision (Phase 1 area).
- Develop lots in the industrial subdivision near the power plant.
- ii.) <u>2019 2024</u>
- Develop Phase 2 area within the Arena Subdivision.
- Develop lots in the industrial subdivision near the power plant.
- iii.) <u>2024 2034</u>
- Develop Phase 3 area within the Arena Subdivision.

### e) Council may change the phasing of development without amendment to this Plan.

### SECTION 3. GENERAL POLICIES

- The following policies of Council apply to all development in the Hamlet regardless of land use designation:
- a) The development of lots shall be subject to the following lot development policies:
   i.) All service connections to buildings shall be easily accessed from the front yard on all lots and grouped together, where possible.
- ii.) Access to new buildings will avoid, where possible, main entrances on the south-southeast side to reduce problems associated with snow drifting.
- iii.) Buildings shall be sited to respect setbacks identified on the Zoning Chart.
- iv.) Any building over 500 m2 in gross floor area shall consider potential wind impacts on surrounding development. A wind study may be required by the Development Officer.
- v.) Culverts are required and shall be installed at the access points to lots.
- vi.) On any portion of a lot where fill is introduced, drainage shall be directed towards the public road. Exceptions may be made by the Development Officer. Where possible, drainage troughs shall not be located in Utility Rights-of-Way or Easements.
- vii.) Road widenings may be obtained as required at the time of development or redevelopment of a lot in situations where the road right of way is less than 16 metres wide.
- b) Utilities or communication facilities shall be permitted in any land use designation. Other than designated Rights-of-Way or Easements for Utility or Communication lines, Easements alongside roadways, marked between the edge of the roadway and lot lines, will be used for distribution lines, with a minimum clearance, as specified in the Utility Corporation's Joint Use Agreement.
  c) The Hamlet will pile snow in locations to minimize downwind snow drifting and where spring melt run-off can be properly channeled to drainage ditches or waterbodies.
- d) The Hamlet will avoid piling snow within at least 30.5 metres (100 feet) of any watercourse.
- e) No development is generally permitted within 30 metres from the normal high water mark of a waterbody or watercourse.
   f) The Hamlet shall protect any cemeteries and sites of archaeological, ethnicographical, palaeontological or historical significance from disturbance. Any development in or near such sites shall follow the Nunavut Archaeological and Palaeontological Regulations, 2001 of the Nunavut Act (Canada).
- g) The Hamlet shall encourage development that minimizes emissions from fossil fuels, that are energy efficient and that consider alternative energy supply technology.
- h) The Hamlet shall work with the Nunavut Planning Commission to ensure that the Kimmirut Community Plan and the future Baffin Regional Land Use Plan are compatible.

### SECTION 4. LAND USE DESIGNATION

### 4.1 Residential

The Residential designation provides land for primarily residential uses, but also permits other small-scale conditional uses subject to the approval of Council. The policies of Council are intended to maintain an adequate supply of land for residential development, to build safe and livable neighbourhoods and to protect residential areas from incompatible development. The policies of Council are:

- a) The Residential designation will be used primarily for housing with all types of dwelling types permitted. Other related residential uses such as a group home, a home occupation, or bed and breakfast will also be permitted.
- b) Residential development will be phased so that a minimum of 4 vacant surveyed lots are available at any given time. Residential areas will be developed with an average residential density of 22 units per hectare and will include a mix of unit types including those for elders.

### 4.2 Community Use

- The Community Use designation is intended to maintain an adequate supply of land for community uses, preferably in significant and important locations so that residents may enjoy easy access to public facilities and services. The policies of Council are:
   a) The Community Use designation will be used primarily for public uses (i.e. social, cultural, religious, or educational) and government services.
- b) Community facilities will be centrally located to ensure safe and convenient access by residents.

### 4.3 Commercial

The Commercial designation is intended to support local economic development by maintaining an adequate supply of land for commercial uses in a key locations across the Hamlet offering good access for residents and visitors. The policies of Council are: a) The Commercial designation will be used for commercial uses such as hotels, restaurants, retail, personal and business services, and offices.

- b) Residential uses shall be permitted when located above a ground floor commercial use.
- c) Commercial facilities will be located along main roads, where possible, to provide safe and convenient access by residents.d) Council will encourage the re-use or redevelopment of existing commercial sites within the existing townsite.

### 4.4 Open Space

The Open Space designation is intended to protect shoreline environments, maintain access to the sea and to reserve open spaces within the built up area for recreational uses and cultural events. The policies of Council are:

- a) The Open Space designation will be used primarily for parks, walking trails, traditional and recreational uses such as beach shacks, harbour uses, boat storage, dog teams, community docks, temporary storage of sealift materials and equipment during sealift operations, and municipal infrastructure such as a water pump house. All uses are conditional and at the discretion of Council.
- b) A playground should be located within 300 metre walking distance from any residence in the community.
   c) Unless otherwise noted, all Commissioner's Land forming part of the 100-foot strip (30.5 m) along the seashore measured from the ordinary high water mark will be designated Open Space.
- d) No development is generally permitted within 30 metres from the normal high water mark of any river or major creek. Council may consider the filling of a waterbody where it is needed for future development provided that the appropriate approvals are obtained.
  e) Open Space corridors will be protected for trail connections and drainage channels.

### 4.5 Industrial

The Industrial designation is intended to reduce the negative effects and dangers associated with industrial uses such as noise, dust, odours, truck travel and the storage of potentially hazardous substances by concentrating these uses on the periphery of the townsite. The policies of Council are:

a) Permitted uses in the Industrial designation will include all forms of manufacturing, processing, warehousing and storage uses as well as uses associated with marine transportation. Permitted uses will also include garages, power generation plants, and fuel storage.
b) Council will develop new industrial subdivisions near the current landfill site to minimize land use conflicts and to reserve land closer to the townsite for residential and community uses. Council will work with local businesses and government operations to identify opportunities to relocate over time non-conforming industrial uses (eg. garages, warehouses, power plant) to industrial areas.

### 4.6 Transportation

The Transportation designation is intended to protect and ensure the safe operation of airport and related activities such as the NavCanada communications site. The policies of Council are:

- a) Permitted uses in the Transportation designation includes all activities related to air traffic and uses accessory to these activities such as related commercial activities and communications sites.
- b) All development within the 4km boundary of the airport, as shown on Schedule 3, shall comply with the Kimmirut Airport Zoning Regulations. Development applications shall be referred to Nunavut Airports for review and approval where development is proposed adjacent to the airport and/or where development has the potential to interfere with airport operations.
- c) All development within the Transportation Influence Zone of the communications facility is subject to the approval of NavCanada.d) Council will discourage the use of travelled pathways that are not identified as public right-of-ways.

### 4.7 Hinterland

- The Hinterland designation applies to all unsurveyed land within the Municipal Boundary not designated by another land use and is intended to protect the natural beauty and cultural resources of the land - 'Nuna' - while providing access for traditional, recreational and tourism activities, as well as quarrying. The policies of Council are:
- a) The Hinterland designation generally permits traditional, tourism and passive recreational uses. Permitted uses also include dog teams, quarrying, and infrastructure projects for local economic development.
- b) Council shall ensure that development does not negatively impact wildlife, wildlife habitat and harvesting and is consistent with the guiding principles of Inuit Qaujimajatuqangit (IQ).

### 4.8 Waste Disposal

The Waste Disposal designation is intended to identify existing or former waste disposal sites and ensure required development setbacks are followed. The policies of Council are:

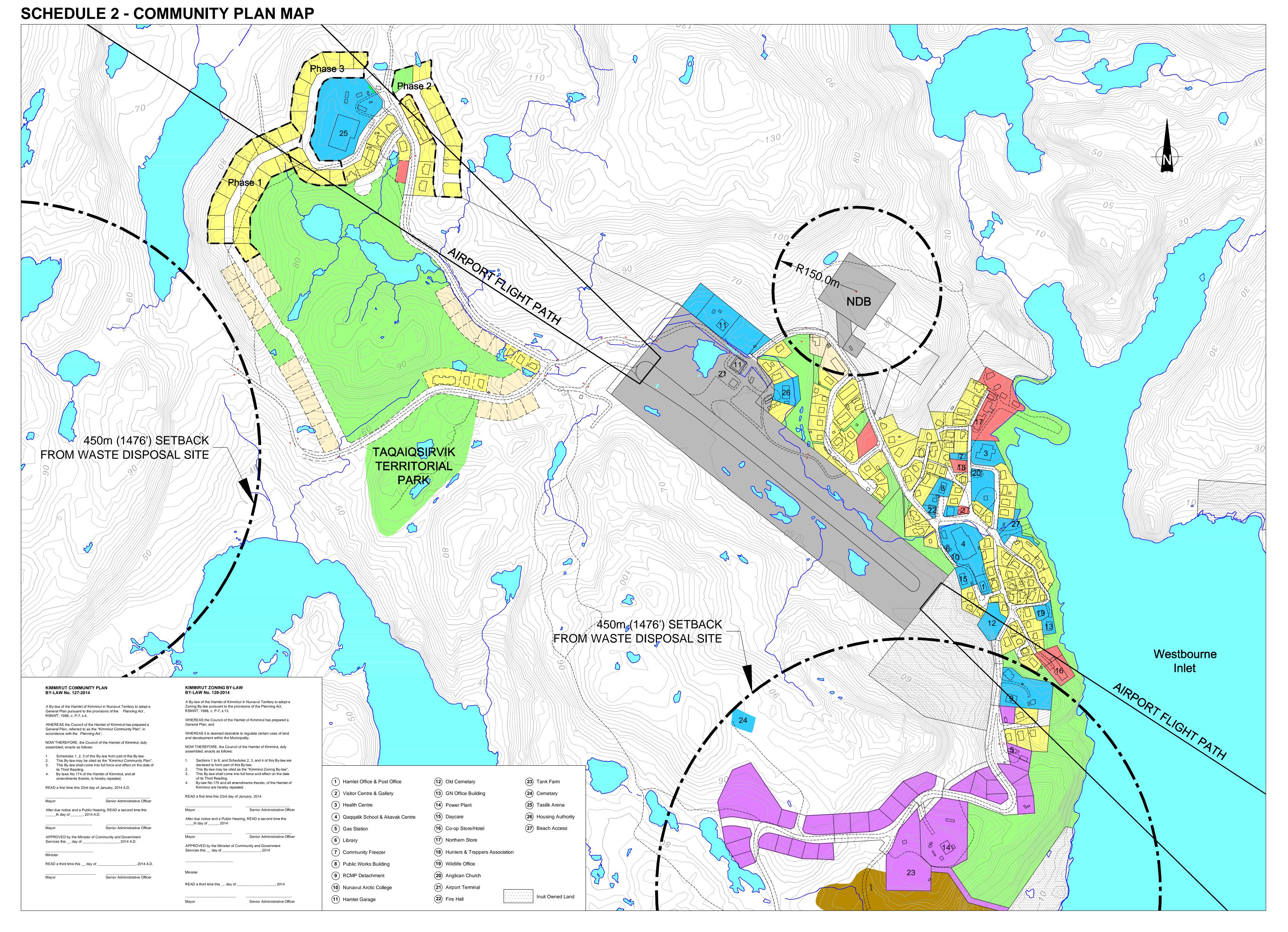
- a) The Waste Disposal designation permits no development except those uses accessory to the operation or remediation of a waste disposal site.
- b) The Hamlet shall prohibit the development of residential uses and uses involving food storage or food preparation within the 450 metre setback from any existing or former waste disposal site, pursuant to the General Sanitation Regulations of the Public Health Act.
- c) The Hamlet shall prohibit the development of any public road allowance or cemetery within a 90 metre setback from a waste disposal ground, pursuant to the General Sanitation Regulation of the Public Health Act.
- d) The Hamlet will evaluate all possible options for an integrated waste management system, including:
  - a. the suitability of the existing landfill site for long-term use;
  - b. the use of an incinerator;
  - c. metal recovery projects; and
- d. complementary strategies, such as source reduction, reuse, and recycling of waste materials.

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The Granular Resources designation is intended to protect aggregate deposits for future extraction. The policies of Council are: a) The Granular Resources designation does not permit any development except uses accessory to the operation or remediation of a quarry or gravel pit.

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b) Municipal Reserve lands shall be redesignated by amendment to this Plan prior to being used for community expansion.
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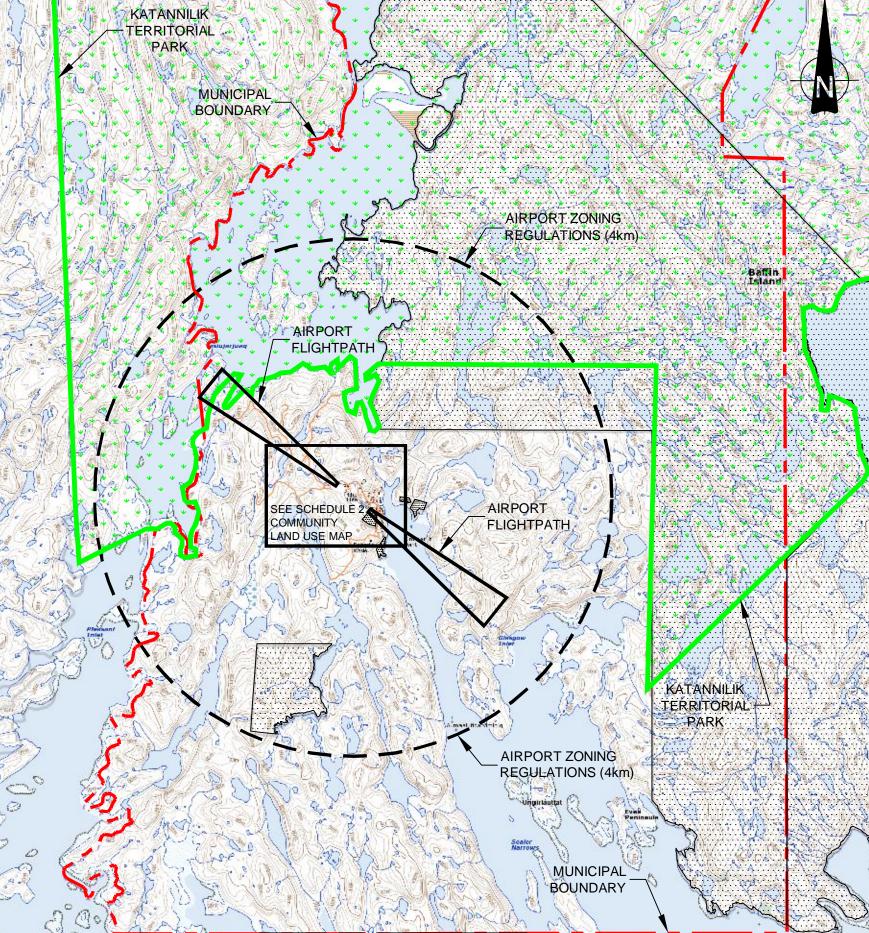


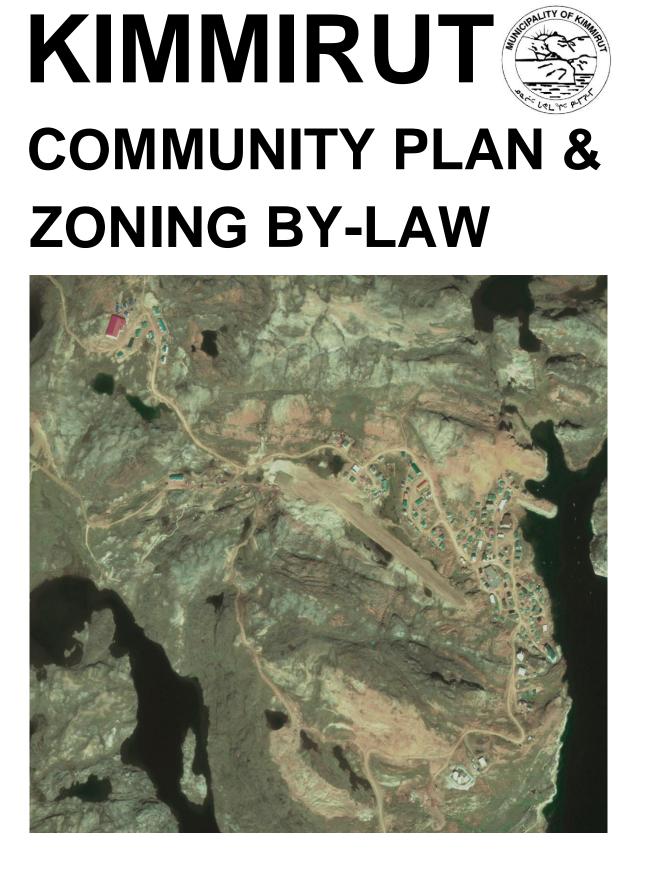
# SCHEDULE 3 - GENERAL LAND USE MAP

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# **SCHEDULE 4 - ZONE REGULATIONS**

|                           | Permitted Uses  | 6   | Conditional Uses   | Zone Requirements  |  |  |
|---------------------------|---|---|--|--|--|--|
| Residential               | Dwelling, single-unit<br>Dwelling, semi-detached or duplex<br>Park or playground  |   | Dwelling, semi-detached or duplex  |  | Bed and breakfast<br>Craft studio<br>Day care centre<br>Dwelling, row house<br>Dwelling, multi-unit<br>Dwelling, apartment<br>Dwelling, mini home<br>Elders facility<br>Group home<br>Home occupation<br>Secondary suite | <ul> <li>(a) <u>Setbacks (minimum)</u><br/>Front = 6 metres<br/>Rear = 6 metres<br/>Rear, backing onto an OS Zone = 2.5 metres<br/>Side (Exterior) = 4 metres<br/>Side (Interior) = 6 metres, or as required by the Fire Marshal<br/><u>Building Height (maximum)</u><br/>8.5 metres (28 feet)</li> <li>(b) Despite the provisions of Section 6.3(a), for semi-detached<br/>dwellings or rowhouse dwellings located on separate, adjacent lots,<br/>the side yard where units are attached may be reduced to zero.</li> <li>(c) Parking or storage of a commercial vehicle having a gross vehicle<br/>weight of 4,500 kg or more such as construction equipment<br/>including bulldozers, backhoes, high hoes, and pay loaders is not<br/>permitted.</li> <li>(d) The following provisions will apply to Secondary Suites:<br/>The suite forms part of a single unit or semi-detached dwelling;</li> <li>(ii) The suite is structurally attached or located within the principal<br/>dwelling, or 60m<sup>2</sup> of gross floor area, whichever is less.</li> </ul> |
| Commercial                | Bank<br>Broadcasting studio<br>Commercial recreation<br>Communications facility<br>Convenience store<br>Craft studio<br>Day care centre   | Hotel<br>Office<br>Parking lot<br>Personal service<br>Restaurant<br>Retail store<br>Service and repair shop                     | Automotive gas bar<br>Automotive repair, sales, or rental shop<br>Dwelling unit(s) in a non-residential building<br>provided that the dwelling unit(s) are above the<br>ground floor.<br>Contractor's shop<br>Home occupation<br>Staff Housing<br>Uses similar in character and purpose to those<br>listed for this zone | (a) <u>Setbacks (minimum)</u><br>Front = 6 metres<br>Rear = 6 metres<br>Side (Exterior) = 4 metres<br>Side (Interior) = 6 metres, or as required by the Fire Marshal<br><u>Building Height (maximum)</u><br>3 storeys, not to exceed 13 metres (42.65 feet)  |  |  |
| Community Use             | Broadcasting studio<br>Community freezer<br>Community hall or centre<br>Correctional facility<br>Day care centre<br>Educational facility<br>Elders facility<br>Emergency and protective services                                  | Place of Worship<br>Government office<br>Group home<br>Health care facility<br>Park or Playground<br>Parking lot<br>Post office | Cemetery<br>Staff housing<br>Uses similar in character and purpose<br>to those listed for this zone  | (a) <u>Setbacks (minimum)</u><br>Front = 6 metres<br>Rear = 6 metres<br>Side (Exterior) = 6 metres, or as required by the Fire Marshal<br><u>Building Height (maximum)</u><br>13 metres (42.65 feet)   |  |  |
| Open Space                | Archaeological site<br>Beach shacks<br>Boat storage<br>Dock<br>Monument, cairn, or statue<br>Park or playground<br>Shed to store equipment for traditional,<br>cultural, and recreational activities taking<br>place in the Zone. | Snow fence<br>Sports field<br>Washroom facility   | Communications facility<br>Dog teams<br>Temporary outdoor storage of sealift<br>equipment during sealift<br>Temporary tenting or camping<br>Uses similar in character and purpose to<br>those listed for this zone   | <ul> <li>(a) The following provisions applies to all development in the Open Space Zone:<br/><u>Gross Floor Area (maximum)</u><br/>25 sq.m.<br/><u>Building Height (maximum)</u><br/>3.1 metres (10 feet)</li> <li>(b) No building or structure shall be located closer than 10m to any side or rear lot line.</li> <li>(c) Dog teams may not be located closer than 30.5 m to a water body.</li> </ul>  |  |  |
| Industrial                | Automotive gas bar<br>Automotive repair, sales or facility<br>Building supply or contractors shop<br>Caretaker unit<br>Communications facility<br>Heavy equipment and vehicle yard<br>Outdoor storage<br>Rental shop<br>Warehouse |   | Community freezer<br>Barge staging and landing site with associated<br>warehousing<br>Food processing facility<br>Fuel storage facility<br>Hazardous goods storage<br>Manufacturing plant<br>Power generation facility<br>Uses similar in character and purpose to those<br>listed for this zone                         | <ul> <li>(a) Setbacks (minimum)<br/>Front = 6 metres<br/>Rear = 8 metres<br/>Side (Exterior) = 6 metres<br/>Side (Interior) = 8 metres, or as required by the Fire Marshal<br/>Building Height (maximum)<br/>10.7 metres (35 feet)</li> <li>(b) Only 1 caretaker unit is permitted on a lot.</li> <li>(c) Hazardous goods storage or tank farm uses<br/>shall not be permitted within 30.5 metres of<br/>any water course.</li> <li>(d) No commercial development involving food<br/>storage, handling or preparation shall be<br/>permitted within 450m of a waste handling<br/>facility.</li> </ul>  |  |  |
| <b>Granular Resources</b> |   |   | Quarry   |  |  |  |
| Waste Disposal            |   |   | Waste disposal site<br>Sewage treatment system (lagoon, etc.)  | (a) No residential development or commercial development involving food storage, handling<br>or preparation shall be permitted within 450 metres of a waste disposal site.   |  |  |
| Hinterland                | Archaeological site<br>Dog team<br>Temporary tenting or camping   |   | Beach shack<br>Cabin<br>Quarry<br>Cemetery<br>Commercial harvesting<br>Communications facility<br>Permanent hunting and fishing cabins or camps<br>Resource exploration and development<br>Snow fence<br>Tourist facilities<br>Wind turbine<br>Uses similar in character and purpose to those<br>listed for this zone    | <ul> <li>(a) Any development within the Transportation Influence Zone as indicated on the Land<br/>Use Map shall be subject to the approval of NAV Canada.</li> <li>(b) No development is permitted within 150 metres downwind of any snow fence without<br/>the approval of council.</li> <li>(c) No development is permitted within 200 metres of a wind turbine.</li> <li>(d) No development is permitted within 100 metres of an Archaeological or Paleontological<br/>Site, unless approved by the Territorial Archaeologist or Director of Culture and<br/>Heritage from the Department of Culture and Heritage.</li> <li>(e) Cabins may not be located closer than 30.5m to a waterbody and/or road (whether it be<br/>surveyed or not).</li> </ul> |  |  |
| Transportation            | Airport and related uses<br>Communications facility<br>Service shop<br>Sea lift facility  |   |  | <ul> <li>(a) Any development within a 4,000 m radius of the airport reference point, as indicated on the Land Use Map, is subject to the Kimmirut Airport Zoning Regulations and shall be subject to the approval of NAV Canada and Nunavut Airports.</li> <li>(b) No development shall occur within 150 metres of the Non-Directional Beacon (NDB) Site.</li> </ul>   |  |  |
| Municipal Reserve         |   |   |  | (a) The Municipal Reserve Zone identifies lands that may be interesting for future redevelopment. No<br>development is permitted in the MR Zone unless of temporary nature, subject to Council approval.   |  |  |













# KIMMIRUT COMMUNITY PLAN BY-LAW N 0. 127

# March 2014



## KIMMIRUT COMMUNITY PLAN BY-LAW No. 127-2014

A By-law of the Hamlet of Kimmirut in Nunavut Territory to adopt a General Plan pursuant to the provisions of the *Planning Act*, RSNWT, 1988, c. P-7, s.4.

WHEREAS the Council of the Hamlet of Kimmirut has prepared a General Plan, referred to as the "Kimmirut Community Plan", in accordance with the *Planning Act*,

NOW THEREFORE, the Council of the Hamlet of Kimmirut, duly assembled, enacts as follows:

- 1. Schedules 1, 2, 3 of this By-law form part of this By-law.
- 2. This By-law may be cited as the "Kimmirut Community Plan".
- 3. This By-law shall come into full force and effect on the date of its Third Reading.
- 4. By-laws No.92-2006 of the Hamlet of Kimmirut, and all amendments thereto, are hereby repealed.

READ a first time this 23<sup>rd</sup> day of January, 2014 A.D.

Mayor

Senior Administrative Officer

After due notice and a Public Hearing, READ a second time this \_\_\_\_\_<sup>th</sup> day of \_\_\_\_\_, 201\_ A.D.

Mayor

Senior Administrative Officer

APPROVED by the Minister of Community and Government Services this \_\_ day of \_\_\_\_\_, 201\_ A.D.

Minister

READ a third time this \_\_\_ day of \_\_\_\_\_, 201\_ A.D.

| Mayor |
|-------|
|-------|

Senior Administrative Officer

## SCHEDULE 1

## **SECTION 1. INTRODUCTION**

## 1.1 Purpose of the Plan

The purpose of the Kimmirut Community Plan is to outline Council's policies for managing the physical development of the Hamlet for the next 20 years – to 2034. The Community Plan was created through a community consultation process and reflects the needs and desires of the Community. The Community Plan builds on previous plans, while incorporating new challenges, issues and needs identified by the Community.

## 1.2 Goals of the Community Plan

Community Plan policies emerge from the values of a community and its vision of how it would like to grow. The goals established for this Community Plan are:

- 1. To develop in an orderly fashion creating a safe, healthy, functional, and attractive community that reflects community values and culture.
- 2. To promote the Plan as a tool for making effective and consistent decisions regarding land use and development in the community.
- 3. To ensure an adequate supply of land for all types of uses to support the growth and change of the community.
- 4. To build upon community values of participation and unity to support community projects and local economic development.
- 5. To protect the natural beauty of "Nuna", protect viewpoints to the water, and retain waterfront and lakeshore areas for public uses and traditional activities.

## 1.3 Administration of the Plan

The Community Plan is enacted by By-law. Changes to the Plan can be made by amending the By-laws in accordance with the *Nunavut Planning Act*. The Community Plan should be reviewed and updated every five years as required by the *Nunavut Planning Act*. A Zoning By-law is also being enacted for the purpose of implementing detailed policies based on the Community Plan. All development must follow the intent of the Community Plan and Zoning By-law. The Community Plan includes Schedule 1 (Plan Policy Text), Schedule 2 (Community Plan and Zoning Map) and Schedule 3 (General Land Use Map).

### SECTION 2. COMMUNITY GROWTH AND PHASING POLICIES

At the time of preparation of this Plan, the population of Kimmirut was approximately 455 people. This Plan is based on a future population of 591 people by 2034. It is estimated that an additional 67 dwelling units will be required to meet the projected population growth, representing the need for approximately 3 hectares of land for residential development. In addition, an appropriate mix and range of industrial, commercial, and community uses has been proposed to meet long-term needs. The policies of Council are:

- a) Plan for a 2034 population of 591.
- b) Identify sufficient land on the Community Plan to meet the needs of the projected 2034 population.
- c) Review the Community Plan in 5 years, in 2019, to re-assess actual rates of growth and community needs.
- d) Council will generally phase new land development as follows:
  - i.) <u>2014 2019:</u>
    - Develop existing vacant lots within the Arena Subdivision (Phase 1 area).
    - Develop lots in the industrial subdivision near the power plant.
  - ii.) <u>2019 2024</u>
    - Develop Phase 2 area within the Arena Subdivision.
    - Develop lots in the industrial subdivision near the power plant.
  - iii.) <u>2024 2034</u>
    - Develop Phase 3 area within the Arena Subdivision.
- e) Council may change the phasing of development without amendment to this Plan.

## **SECTION 3. GENERAL POLICIES**

The following policies of Council apply to all development in the Hamlet regardless of land use designation:

- a) The development of lots shall be subject to the following lot development policies:
  - i.) All service connections to buildings shall be easily accessed from the front yard on all lots and grouped together, where possible.
  - ii.) Access to new buildings will avoid, where possible, main entrances on the south-southeast side to reduce problems associated with snow drifting.
  - iii.) Buildings shall be sited to respect setbacks identified on the Zoning Chart.
  - iv.) Any building over 500 m<sup>2</sup> in gross floor area shall consider potential wind impacts on surrounding development. A wind study may be required by the Development Officer.
  - v.) Culverts are required and shall be installed at the access points to lots.
  - vi.) On any portion of a lot where fill is introduced, drainage shall be directed towards the public road. Exceptions may be made by the Development Officer. Where possible, drainage troughs shall not be located in Utility Rights-of-Way or Easements.
  - vii.) Road widenings may be obtained as required at the time of development or redevelopment of a lot in situations where the road right of way is less than 16 metres wide.
- b) Utilities or communication facilities shall be permitted in any land use designation. Other than designated Rights-of-Way or Easements for Utility or Communication lines, Easements alongside roadways, marked between the edge of the roadway and lot lines, will be used for distribution lines, with a minimum clearance, as specified in the Utility Corporation's Joint Use Agreement.
- c) The Hamlet will pile snow in locations to minimize downwind snow drifting and where spring melt run-off can be properly channeled to drainage ditches or waterbodies.
- d) The Hamlet will avoid piling snow within at least 30.5 metres (100 feet) of any watercourse.
- e) No development is generally permitted within 30 metres from the normal high water mark of a waterbody or watercourse.
- f) The Hamlet shall protect any cemeteries and sites of archaeological, ethnicographical, palaeontological or historical significance from disturbance. Any development in or near such sites shall follow the *Nunavut Archaeological and Palaeontological Regulations, 2001* of the <u>Nunavut Act</u> (Canada).

- g) The Hamlet shall encourage development that minimizes emissions from fossil fuels, that are energy efficient and that consider alternative energy supply technology.
- h) The Hamlet shall work with the Nunavut Planning Commission to ensure that the Kimmirut Community Plan and the future Baffin Regional Land Use Plan are compatible.

## SECTION 4. LAND USE DESIGNATION

### 4.1 Residential

The Residential designation provides land for primarily residential uses, but also permits other small-scale conditional uses subject to the approval of Council. The policies of Council are intended to maintain an adequate supply of land for residential development, to build safe and livable neighbourhoods and to protect residential areas from incompatible development. The policies of Council are:

- a) The Residential designation will be used primarily for housing with all types of dwelling types permitted. Other related residential uses such as a group home, a home occupation, or bed and breakfast will also be permitted.
- b) Residential development will be phased so that a minimum of 4 vacant surveyed lots are available at any given time. Residential areas will be developed with an average residential density of 22 units per hectare and will include a mix of unit types including those for elders.

### 4.2 Community Use

The Community Use designation is intended to maintain an adequate supply of land for community uses, preferably in significant and important locations so that residents may enjoy easy access to public facilities and services. The policies of Council are:

- a) The Community Use designation will be used primarily for public uses (i.e. social, cultural, religious, or educational) and government services.
- b) Community facilities will be centrally located to ensure safe and convenient access by residents.

### 4.3 Commercial

The Commercial designation is intended to support local economic development by maintaining an adequate supply of land for commercial uses in a key locations across the Hamlet offering good access for residents and visitors. The policies of Council are:

- a) The Commercial designation will be used for commercial uses such as hotels, restaurants, retail, personal and business services, and offices.
- b) Residential uses shall be permitted when located above a ground floor commercial use.
- c) Commercial facilities will be located along main roads, where possible, to provide safe and convenient access by residents.
- d) Council will encourage the re-use or redevelopment of existing commercial sites within the existing townsite.

## 4.4 Open Space

The Open Space designation is intended to protect shoreline environments, maintain access to the sea and to reserve open spaces within the built up area for recreational uses and cultural events. The policies of Council are:

- a) The Open Space designation will be used primarily for parks, walking trails, traditional and recreational uses such as beach shacks, harbour uses, boat storage, dog teams, community docks, temporary storage of sealift materials and equipment during sealift operations, and municipal infrastructure such as a water pump house. All uses are conditional and at the discretion of Council.
- b) A playground should be located within 300 metre walking distance from any residence in the community.
- c) Unless otherwise noted, all Commissioner's Land forming part of the 100foot strip (30.5 m) along the seashore measured from the ordinary high water mark will be designated Open Space.
- d) No development is generally permitted within 30 metres from the normal high water mark of any river or major creek. Council may consider the filling of a waterbody where it is needed for future development provided that the appropriate approvals are obtained.
- e) Open Space corridors will be protected for trail connections and drainage channels.

## 4.5 Industrial

The Industrial designation is intended to reduce the negative effects and dangers associated with industrial uses such as noise, dust, odours, truck travel and the storage of potentially hazardous substances by concentrating these uses on the periphery of the townsite. The policies of Council are:

- a) Permitted uses in the Industrial designation will include all forms of manufacturing, processing, warehousing and storage uses as well as uses associated with marine transportation. Permitted uses will also include garages, power generation plants, and fuel storage.
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- a) The Waste Disposal designation permits no development except those uses accessory to the operation or remediation of a waste disposal site.
- b) The Hamlet shall prohibit the development of residential uses and uses involving food storage or food preparation within the 450 metre setback from any existing or former waste disposal site, pursuant to the *General Sanitation Regulations* of the Public Health Act.
- c) The Hamlet shall prohibit the development of any public road allowance or cemetery within a 90 metre setback from a waste disposal ground, pursuant to the General Sanitation Regulation of the *Public Health Act*.

- d) The Hamlet will evaluate all possible options for an integrated waste management system, including:
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### 4.10 Municipal Reserve

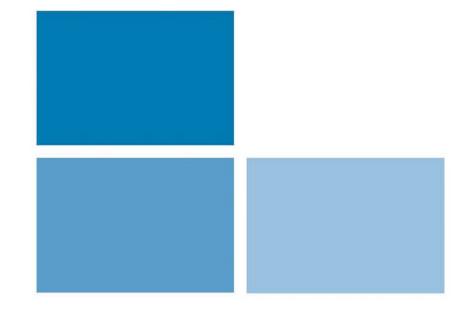
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Municipality of Kimmirut P.O Box 120 Kimmirut NU, X0A 0N0 Tel: 867.939.82247 Fax: 867.939.20450







# APPENDIX C

## **CULVERT THAWING METHODS**





# **Culvert Thawing**



Culverts are subject to freezing during winter and spring. During winter, ground water can continuously feed streams which either flow through culverts or over roadways causing icing. During spring breakup, daytime melting must be carried through culverts.

When a culvert freezes it can no longer do the job it was designed to do and trapped water will begin to cause problems and ultimately, money.

## What's the Solution?

To thaw culverts, a combination of hot water/steam and high pressure water in a mobile environment is the effective method.

## **Mobile Pressure Washers**

To thaw culverts quickly, a skid style hot water pressure washer/steamer, also known as a truck mounted pressure washer is the equipment of choice.

Self-contained and designed to hold up under the toughest of conditions, skid mounted pressure washers/steamers can be bolted onto the back of a truck, on an open deck trailer or in an enclosed trailer.



Enclosed Trailer Mounted Pressure Washer



**Open Deck Mounted Pressure Washer** 



Skid Mounted Presure Washer

## **Culvert Nozzles**

Culvert nozzles are required to dig effectively through ice. The reverse jets on the fixed and rotary nozzles pull the hose through the tube or sewer line and blast debris from the line or tube wall.

Backward ports drive the nozzle forward and flush debris Forward ports blast into pipe and break up clogs & debris Physically small for cornering ability up to 4200 PSI Corrosion resistant stainless steel construction A wide range of orifice sizes are available for various pressure and flow applications

Rotating style adds extra agitation and surface cleaning



## United States Patent [19]

#### Olsson

#### [54] METHOD FOR THAWING OUT ROAD CULVERTS CHOKED WITH ICE

- [76] Inventor: Lars-Uno Olsson, Heden 4084, S-780 53 Nås, Sweden
- [21] Appl. No.: 931,722
- [22] PCT Filed: Feb. 24, 1986
- [86] PCT No.: PCT/SE86/00080
  - § 371 Date: Oct. 24, 1986
- § 102(e) Date: Oct. 24, 1986
- [87] PCT Pub. No.: WO86/04939
   PCT Pub. Date: Aug. 28, 1986

#### [30] Foreign Application Priority Data

- Feb. 25, 1985 [SE] Sweden ...... 8500914
- [51] Int. Cl.<sup>4</sup> ..... E03B 7/10; F16L 53/00
- [52] U.S. Cl. ..... 138/32; 138/28; 138/35
- [58] Field of Search ...... 138/26, 28, 32, 35; 254/262, 263, DIG. 14; 405/124, 130, 131; 137/301

#### [56] References Cited

#### U.S. PATENT DOCUMENTS

596,062 12/1897 Firey ..... 138/28

### [11] Patent Number: 4,770,211

#### [45] Date of Patent: Sep. 13, 1988

| 678,118   | 7/1901 | Kruschke .          |
|-----------|--------|---------------------|
| 926,092   | 6/1909 | Bright 138/28       |
| 2,029,630 | 2/1936 | McMichael 138/28    |
| 2,676,607 | 4/1954 | Carr et al 138/32 X |

#### FOREIGN PATENT DOCUMENTS

| 1122877  | 5/1982  | Canada           | 138/32 |
|----------|---------|------------------|--------|
| 1219487  | 5/1960  | France           | 138/28 |
| 2478161  | 9/1981  | France .         |        |
| 80034861 | 11/1981 | Sweden .         |        |
| 1345     | 1/1891  | United Kingdom   | 138/28 |
| 15138    | 7/1892  | United Kingdom   | 138/28 |
| 1288677  | 9/1972  | United Kingdom . |        |
|          |         | U.S.S.R          |        |
| 901427   | 1/1982  | U.S.S.R          |        |

Primary Examiner-James E. Bryant, III

Attorney, Agent, or Firm-Witherspoon & Hargest

#### [57] ABSTRACT

Method for clearing a road culvert or the like which is choked with ice, wherein a substantially homogeneous rope of a material having at least a certain reversible extensibility is extended through the culvert from its inlet side to its outlet side and wherein the rope in its unloaded condition is clamped in connection with the outlet side and the inlet side respectively of the culvert so that the rope extends through the culvert.

#### 4 Claims, 3 Drawing Sheets

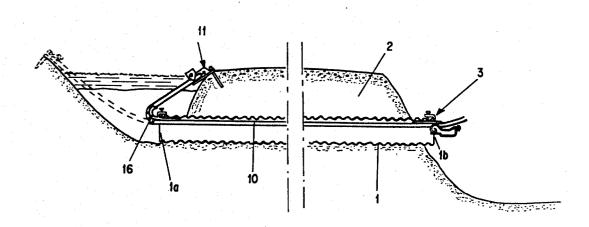
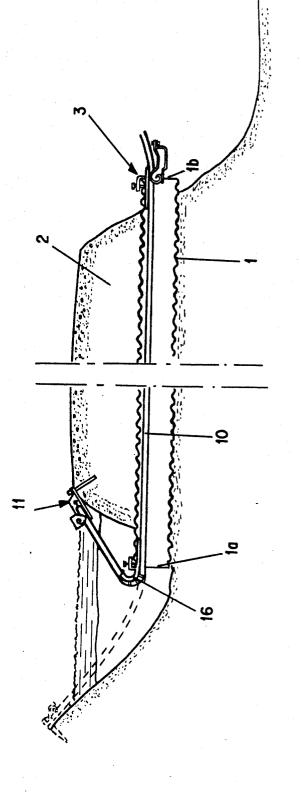
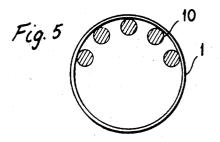
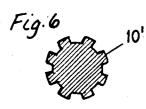
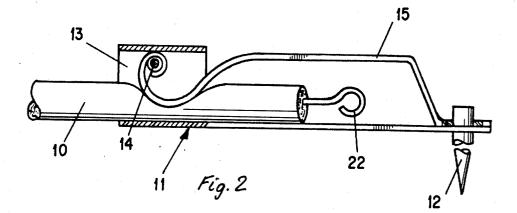


Fig. 1









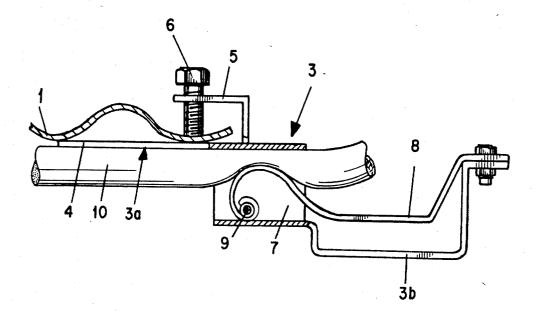
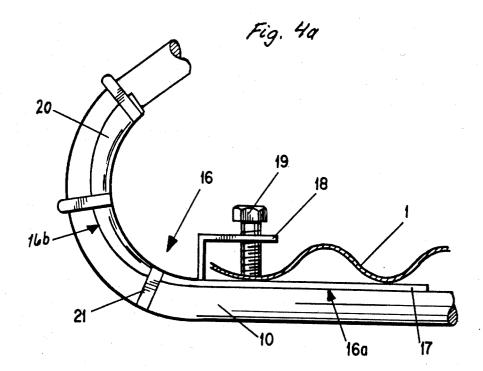


Fig. 3



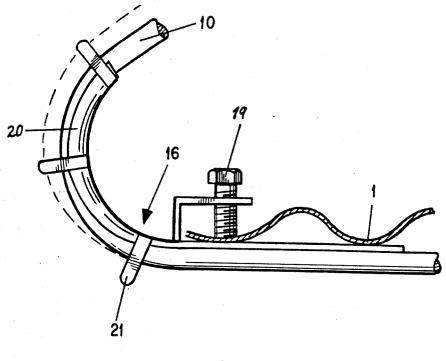


Fig. 46

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#### METHOD FOR THAWING OUT ROAD CULVERTS **CHOKED WITH ICE**

#### BACKGROUND OF THE INVENTION

The present invention relates to a method for thawing out road culverts choked with ice and also relates to an apparatus for carrying out said method.

A common problem in connection with winter main-10 tenance is that road culverts become completely choked with ice, which makes it impossible to drain melted ice through the road culverts in warm weather, and especially by the spring flood. If such a road culvert that is completely choked with ice is not thawed out before the spring flood this may cause serious flooding and also a danger of parts of the road way being washed away.

In order to prevent the above mentioned, serious consequences of a road culvert choked with ice it is presently common practice to continously inspect road 20 culverts which by experience are known to cause problems. When a road culvert choked with ice is found during such a periodical inspection, the procedure is presently to send out a clearing partrol, usually two question. Today steam generators are mostly used for thawing out road culverts in this manner, although attempts have also been made to use conventional building dryers. Already from the above it is clear that the thawing out of a road culvert in the conventional man- 30 culvert diameters and lengths. ner brings about relatively high costs which apart from transport costs also include wage costs for two persons and the cost for the steam generator.

Apart from the fact that the conventional clearing method discussed above is relatively expensive it also 35 suffers from a number of more or less serious disadvantages that are clear from the following general description of the presently employed method using steam thawing. As indicated above a steam generator is transported out to the working place on a lorry or the like, 40 tures of the invention are also clear. and when the ends of the road culvert have been exposed the steam generator is started and is connected through hoses to steam pipes used for the thawing. In certain cases it is only necessary to thaw out a smaller passage through the culvert, whereupon the flow of 45 closed drawings, on which: water through this smaller passage continues to widen the passage in the ice until the culvert is completely cleared. In such a case it is, for obtaining the best result, absolutely necessary that the first thawing out of the smaller passage is carried out relatively close to the 50 tus according to the invention. upper portion of the road culvert since the water will eat its way down through the ice towards the bottom of the culvert. Since road culverts may have a length of up to 15-20 meters, depending upon the width of the road, such a thawing out of a first small passage through the 55 entire length of the road culvert is very difficult to achieve with a satisfactory result by means of a steam pipe. The reason for this is that if the steam pipe has such a length that it may reach through the entire length of the road culvert it will not be possible to keep it close 60 to the upper portion of the road culvert throughout the entire length thereof and accordingly the steam pipe will deflect such that in the worst case it will leave the culvert close to its bottom. Accordingly it may also happen that the steam pipe will be stopped and cannot 65 be brought through the entire length of the road culvert in case stones have fallen into the road culvert and remained therein on the bottom of the culvert.

In other cases it is not sufficient to thaw out only a smaller passage in the road culvert in order to avoid flooding, and therefore it will be necessary to clear the whole culvert in order to avoid the risk that a smaller passage is frozen again. It will also be realized that in the above discussed case where it proves impossible even to thaw out a first small passage in the road culvert by means of a steam pipe, it may become necessary to clear the whole culvert. In such a case when the whole culvert is to be cleared the procedure is such that a number of unperforated steam pipes, being upon in the outer end and having a length of approximately 3 meters are successively introduced from the outlet side of the culvert. When these unperforated pipes have been 15 inserted to their full length they are withdrawn and are exchanged for perforated steam pipes which are fixed in position. Then steam is turned on to perform its thawing action until this length of the culvert may be cleared. This procedure is repeated until the culvert has been cleared throughout its length. The last portion of the length of the culvert is usually cleared from its inlet side, but it will be realized that if the culvert has a length of 10-15 meters and possibly even 20 meters it will be necessary for the persons performing the clearpersons, by car for thawing out the road culvert in 25 ing to crawl into the culvert in order to be able to carry out a great deal of the work. Even if this work is not extremely risky it is cold and damp and generally unpleasant. Naturally such a clearing of a complete culvert is very time consuming, and especially so by larger

#### SUMMARY OF THE INVENTION

The object of the present invention is to provide a method and an apparatus by means of which the above discussed disadvantages in connection with conventional methods may be eliminated as far as possible.

This object is achieved by means of a method and an apparatus of the kind indicated in the enclosed patent claims. From the patent claims the characteristic fea-

#### BRIEF DESCRIPTION OF THE DRAWINGS

Exemplifying embodiments of the invention are described more closely below in connection with the en-

FIG. 1 is a schematic illustration of the principles of the present invention in connection with a road embankment with a road culvert, both in cross section.

FIG. 2 illustrates a ground attachment of the appara-

FIG. 3 illustrates a culvert attachment of the apparatus according to the invention.

FIG. 4a illustrates an edge cover in combination with the rope in its unloaded condition.

FIG. 4b illustrates the edge cover according to FIG. 4a, but with the rope in its loaded condition.

FIG. 5 illustrates a modified embodiment with several apparatuses according to the invention positioned in a road culvert, and

FIG. 6 illustrates another embodiment of the rope having an alternative cross-sectional shape.

Although the invention is described herein with reference only to the clearing of a road culvert, it should be obvious that the invention with the same advantage may be used for thawing out other types of culverts for draining off melted ice and/or rain-water. An example of this may be culverts used in fields by farmers in order to prevent flooding of the fields.

#### DETAILED DESCRIPTION OF PREFERRED **EMBODIMENTS**

FIG. 1 schematically illustrates the use of the invention by a road culvert 1 extended through a road en- 5 bankment 2 in order to conduct melted ice and/or rainwater from an inlet side 1a to an outlet side 1b. Mostly the outlet side 1b of the culvert is relatively freely accessible from the outside even if the road culvert 1 is completely choked with ice, and thus, for reasons 10 which will be explained below, a culvert attachment 3 is positioned in connection with the outlet and 1b of the culvert. An embodiment of the culvert attachment 3 is illustrated in greater detail in FIG. 3 from which it is clear that the culvert attachment has a first portion 3a 15 is also provided with a number of guide loops 21 evenly intended to be clamped to the culvert. In the illustrated embodiment the first portion 3a comprises an inner leg 4 and an outer leg 5 between which the culvert 1 is introduced and clamped by means of a bolt 6 engaging a threaded bore in the outer leg 5. The other portion 3b 20 invention is intended to be extended through a road of the culvert attachment is formed integral with the first portion 3a and is at its outer end releasably connected to a clamping means 8, for instance by means of a screw-nut connection 8a. In the illustrated embodiment the clamping means 8 consists of a flat bar being 25 bent into a helical shape in its free end for a pivotal mounting on a pin 9 being firmly connected to a plate secured to the culvert attachment substantially midway between its ends. Through the pivotal mounting of the clamping means 8 on the pin 9 a rope 10 that will be 30 at the culvert attachment 3 as well as at the ground more closely described below may be released and clamped between the helical end of the clamping means 8 and a portion of the culvert attachment close to the middle thereof by swinging the clamping means 8 upwardly and downwardly respectively about the pin 9. 35

In connection with the inlet side 1a of the road culvert 1 and at a distance therefrom a ground attachment 11 is anchored in the road embarkment 2 or at some other suitable place in accordance with what will be discussed below. In FIG. 2 a suitable embodiment of the 40 ground attachment 11 is illustrated which in one of its ends is provided with a peg 12 which is pointed in one of its ends and which is intended to be forced down into the ground for anchoring the ground attachment. In its other end the ground attachment 11 is provided with a 45 rope out from the culvert, it is sufficient if the rope has plate 13 which essentially corresponds to the plate 7 on the culvert attachment of FIG. 3 and which accordingly is provided with a pin 14 for pivotal mounting of one end of a clamping means 15 which in turn corresponds to the clamping means 8 of FIG. 3. Thus, the 50 clamping means 15 has a helically shaped end for mounting on the pin 14, and in its opposite end it is releasably attached to the ground attachment 11, preferably by means of a nut 15a screwed into a threaded upper portion of the anchoring peg 12. It will now be 55 area is substantially reduced to half without any danger realized that in accordance with what has been described in connection with FIG. 3 the clamping means 15 is intended for releasably clamping the rope 10 between its helical end a portion of the ground attachment 11. 60

In the case illustrated in FIG. 1 where the ground attachment is anchored in connection with the road embankment 2 it also becomes necessary to provide an edge cover 16 at the inlet end 1a of the culvert, and this partly for guiding the rope 10 around the relatively 65 damage through for instance gravel and rocks. sharp bend and at the same time also for protecting the rope. As is clear from FIGS. 4a and 4b the edge cover 16 in a suitable embodiment consists of a first portion

16a which to a great extent corresponds to the first portion 3a of the culvert attachment 3 and thus comprises an inner leg 17 and an outer leg 18 between which the culvert 1 is clamped by means of a bolt 19 screwed into a threaded bore in the outer leg 18. The other portion 16b of the edge cover provides the guiding proper for the rope 10 and for this purpose includes an upwardly bent guide rail 20 having a smooth curvature for deflecting the rope 10 between 90° and 180°, in the illustrated embodiment approximately 135°. For providing the best guiding the guide rail 20 has an inner, longitudinal groove having a shape essentially corresponding to that of the rope 10. For additionally securing and guiding the rope 10 in the guide rail 20 the latter distributed along the length of the guide rail, and through these loops the rope is threaded.

For reasons of clarity it should be mentioned that although the elongated means, which according to the culvert, herein is referred to as a rope this term is not intended to delimit the invention regarding the crosssectional shape or surface of the elongated means. Although the rope in the illustrated embodiments has a substantially circular cross-sectional shape it is obvious that the term rope should also cover rectangular, triangular or other suitable cross-section shapes.

As mentioned above the rope 10 is intended to be extended through the road culvert 1 and to be clamped attachment 11. The rope is substantially solid or homogeneous (possibly with air bubbles contained in the material) and in the illustrated embodiments it has a basically circular sectional area. The rope is cut into a suitable length corresponding to the length of the road culvert to which it is to be attached. Characteristic of the rope is that it is manufactured from a material which at least to a certain degree may be reversibly extended, i.e. a material which when it is subject to a tension load undergoes a certain, not permanent, reduction in cross section. Thus, when the tension load is removed the rope shall resume its original shape. By an embodiment of the invention where a free passage is established through ice in the road culvert by simply pulling the a relatively low reversible extensibility sufficient for reducing the cross-sectional area of the rope to such a degree that it without problem is released from the surrounding ice. By another embodiment where the passage through the ice is established with the rope remaining in the culvert by extending the rope to such an extent that its cross-sectional area is greatly reduced, it must on the other hand be possible to subject the material to such a tension load that its cross-sectional of the material rupturing or breaking. A material that has been found suitable for the later embodiment and that complies with the requirements thereof is a synthetic rubber EPDM (SIS 1626-70).

In either or both of its ends the rope is provided with a hook 22 the function of which will be described below. In certain cases it may also be preferable to provide the free ends of the rope with a not shown web or stocking intended to protect the rope from external

According to an emboidment of the invention the clearing or thawing out of a road culvert is carried out in the following manner:

In good time before the winter, when the culvert is open, the above described equipment is installed, and when installed it can remain there year after year and it will not be necessary to dismount it unless some portion thereof is damaged. The assembly is carried out such 5 that a culvert attachment 3 of the kind described above is clamped to the outlet side 1b of the culvert 1. The ground attachment 11 may be secured by forcing the anchoring peg 12 into the ground by means of any suitable tool so that it is firmly anchored, and the anchoring 10 may be carried out in alternative places depending upon the surrounding terrain. Hereby it is determining that the ground attachment shall be anchored at a spot where there is little danger that it will become covered by ice during winter. The reason for this is naturally 15 that it must be easy to get hold of the end of the rope 10 being positioned in connecton therewith without having to expose said end by chopping off ice. Of importance for the positioning is also that the anchoring position must be as close as possible to the inlet end 1a of the 20 culvert so that the length of the rope may be reduced. In view of this the positioning illustrated with full lines in FIG. 1 seems to be preferable in most cases, but it is also possible to position the ground attachment as illustrated with broken lines in FIG. 1, in which case the rope will 25 be extended obliquely upwardly in FIG. 1.

As mentioned above the positioning of the ground attachment 11 illustrated with full lines in FIG. 1 also necessitates the mounting of an edge cover 16 at the inlet end 1a of the culvert for deflecting and guiding the 30 trated with broken lines in FIG. 1 there is a danger that rope 10. By the alternative positioning illustrated with broken lines it would be possible to manage without any edge cover or with an edge cover of a simpler design. When the culvert attachment, the ground attachment and possibly an edge cover have been installed the rope 35 10 is extended through the culvert and, where appropriate, the rope is then threaded through the edge cover, and its ends are clamped to the culvert attachment and to the ground attachment respectively. The clamping is carried out in such a way that the clamping means 8 and 40 15 respectively is disengaged and is swung about the pin 9 and 14 respectively, whereupon the rope is installed in the respective attachment and is clamped in position by means of the clamping means which are secured by the nut 8a and 15a respectively. The rope 10 is clamped to 45 the attachments in its substantially unloaded condition, i.e. without being subject to any essential tension load. However, especially in connection with longer road culverts it may be necessary to clamp the rope 10 when the same is subject to a certain, low tension load in 50 order to make sure that the rope does not hang down towards the middle but runs close to the upper edge of the culvert 1 throughout its extension, and as discussed in the introduction this is essentially in order to make it possible for the water flowing through an opened pas- 55 sage to eat its way down in the ice so that the ice may be efficiently cleared away. The rope remains in the above described position and when it is discovered, during a routine inspection discussed above, that the culvert is completely choked with ice so that melted ice 60 cannot be drained therethrough it will, by employing the invention, no longer be necessary to send out any special patrol for clearing the culvert, but in most cases the person carrying out the inspection may carry out the clearing by himself. By one embodiment the proce- 65 having a large diameter it may suitable to provide sevdure is such that the rope is released at the culvert attachment 3 by the outlet side 1b of the culvert, possibly subsequent to exposing this side by removing snow,

through disengaging the clamping means 8 and swinging the same about the pin 9. The rope which in this embodiment should have a high reversible extensibility is then stretched or tensioned by hand from the outlet side 1b while remaining clamped at the ground attachment 11, and through this tension load and due to the tensibility of the material the rope 10 is immediately released from the ice as its cross-sectional area is greatly reduced. Hereby a free passage for the melted ice is established around the circumference of rope and when this has been achieved the rope is clamped to the culvert attachment 3 again in its loaded condition so that the water may continue to flow in the passage in such a way that it wears its way through the ice and finally clears the whole culvert. When the culvert has been cleared the rope is released from the culvert attachment 3 again and is unloaded so that it resumes its original shape and finally it is clamped again so that the procedure may be repeated if the culvert should become choked with ice once more. As has been mentioned above it is obvious that the rope 10 by this embodiment should have as high a reversible extensibility as possible in order to establish the largest possible passage for the melted ice when it is stretched or tensioned. In this embodiment it may also be suitable if the rope has a rectangular cross-sectional shape in order to leave as wide a passage as possible for the melted ice to thereby ensure a positive clearing of the complete culvert.

When the ground attachment is positioned as illusthe reduction of the cross section of the rope at the end closest to the ground attachment, due to the great distance from the place where the tension load is applied, goes on so slowly that the water beginning to flow in freezes before sufficient flow has been established in order to keep the passage open. For that reason it may be preferable in all cases to use the variant illustrated with full lines in FIG. 1, having an edge cover 16. The reason for this is that when the rope is stretched about the edge cover the passage may be opened up more quickly by performing the tensioning or stretching in two different steps. In FIG. 4a the rope is illustrated guided about the edge cover in its unloaded condition, but in FIG. 4b the broken lines illustrate how the extension of the rope is blocked by the guide rail 20 of the edge cover so that the reduction of the cross-sectional area of the rope, when the rope is normally tensioned, has been fully established up to the guide rail and possibly a distance around the same, while the remaining portion of the rope still maintains its full cross-sectional dimension so that no melted ice or snow enters from above. At this state the rope is clamped at the culvert attachment 3 when in its loaded condition and the person moves to the ground attachment 11 and exposes the same when necessary. Then the rope is released at the ground attachment and since only a relatively short portion of the rope from the edge cover 16 and up to the ground attachment is unloaded this portion of the rope may quickly be stretched or tensioned so that a full flow through the established passage is immediately obtained and so that the above mentioned danger of freezing is elminated.

By certain road culverts which by experience are known to cause serious problems, or by road culverts eral ropes 10 at a distance from each other in connection with the upper portion of the culvert, and for instance in the way schematicaly illustrated in FIG. 5. Another 5

alternative that may be considered in connection with larger road culverts is to employ thicker ropes therein, but in such a case it may be necessary to provide some kind of not shown auxiliary device having a gear mechanism for tensioning or stretching the rope.

In FIG. 6 a rope 10' is illustrated having an alternative cross-sectional shape with longitudinal grooves or channels. This rope is intended to be twisted in connection with the streching or tensioning thereof so that the grooves assume a screw line shape around the rope. 10 Apart from the fact that this configuration establishes a somewhat larger passage for the melted ice it also gives the ice a non-uniform surface so that the melted ice more efficiently wears off the ice. This is even further emphasized if the grooves or channels initially are heli-15 cally shaped in the rope.

In extremely difficult situations where the above described method is not sufficient or in cases where it is desirable to open up a culvert in spite of the fact that there is no water such as melted ice or snow present that 20 can wear down through the ice during its flow through the culvert, it is in accordance with another embodiment also possible to use the invention together with a conventional steam unit or possibly together with a hot-air unit, such as a building dryer. For this purpose a 25 hook 22 is provided in one or possibly both ends of the rope. By connecting a particular steam pipe (possibly a flexible steam hose), which is closed in one end and in said end is provided with a loop for engaging the hook 22 and which is perforated along a portion of its length, 30 to the steam unit the complete culvert may be cleared from one side without the necessity for crawling into the culvert. This is achieved by hooking-up the loop of the steam pipe to the hook 22 of the rope, whereupon the steam pipe, through withdrawal of the rope, is 35 pulled stepwise through the culvert as this is thawed out. Due to the fact that the steam pipe is pulled in through the passage established by the rope it will not be necessary to take up separate holes for the perforated steam pipe and moreover the complete culvert may be 40 thawed out in one operation independent of the length of the culvert. This work is naturally speeded up even further if several ropes are installed in the culvert in accordance with FIG. 5, whereby a corresponding number of steam pipes may be used. It should be real- 45 ized that by this embodiment it is, as mentioned, sufficient if the rope only has a certain reversible extensibility, since it is intended to establish a passage through the ice by being completely withdrawn from the culvert. Thus, the reduction of the cross-sectional area need 50 rope; connecting the steam pipe to a steam unit; applyonly be sufficient to ensure that the rope is released from the ice.

Although preferred embodiments of the invention have been described and illustrated herein it should be obvious to those skilled in the art that a great number of 55 a free passage through the culvert and successively changes and modifications may be carried out without departing from the scope of the invention. For instance it is possible to employ alternative designs for the culvert attachment, the ground attachment and the edge cover, both regarding their preferred clamping to the 60

culvert, anchoring in the ground and clamping of the rope respectively. Thus, the scope of the invention should only be restricted by the enclosed patent claims. I claim:

1. A method for clearing road culverts or the like having become choked with ice, comprising the steps of: extending a substantially homogenous rope of a material having at least a certain reversible extensibility through the culvert from its inlet side to its outlet side before it becomes choked with ice; clamping the rope in its unloaded condition in connection to the outlet side and inlet side of the culvert so that the rope extends through the culvert; and, once the culvert has become choked with ice, releasing the rope from its clamping in connection with the outlet side of the culvert; applying a tension load to the rope from the released end for reducing the cross-sectional area of the rope and thereby forming a free passage through the culvert around the circumference of the rope; clamping the rope again in connection with the outlet side of the culvert, in the loaded extended condition of the rope; and allowing a continuous flow of melted ice or snow in the passage formed around the circumference of the rope, thereby clearing the road culvert.

2. A method as described in claim 1, wherein a rope having a high reversible extensibility is used and wherein the rope is clamped close to the upper portion of the culvert.

3. A method as described in claim 2, wherein the rope in connection with the inlet side of the culvert is deflected from its extension within the culvert through an edge cover; the corresponding end of the rope is clamped at a distance from the inlet side of the culvert and both ends of the rope, one after the other, are released from the clamping, are tensioned or extended and clamped again.

4. A method for clearing road culverts or the like having become choked with ice, comprising the steps of: extending a substantially homogeneous rope of a material having at least a certain reversible extensibility through the culvert from its inlet side to its outlet side before it becomes choked with ice; clamping the rope in its unloaded condition in connection to the outlet side and the inlet side of the culvert so that the rope extends through the culvert; and, once the culvert has become choked with ice, releasing both ends of the rope at their respective clamping positions; connecting a steam pipe perforated along a portion of its length to one end of the ing a tension load to the end of the rope not connected to the steam pipe, for reducing the cross-sectional area of the rope so that it is released from the ice; successively pulling the rope out from the culvert for forming pulling the steam pipe into the passage in the ice established by withdrawing the rope; thereby successively clearing the culvert by means of steam supplied from the steam unit.



## United States Patent [19]

### Sterling et al.

#### [54] METHOD FOR THAWING FROZEN ROAD CULVERTS

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- [73] Assignee: Iceworm International Inc., Alberta, Canada
- [21] Appl. No.: 08/936,825
- [22] Filed: Sep. 25, 1997
- [51] Int. Cl.<sup>6</sup> ..... H05B 1/00; H01C 3/06
- [52] U.S. Cl. ..... 219/213; 219/549; 338/214

128; 338/214

#### [56] References Cited

#### U.S. PATENT DOCUMENTS

1,349,136 8/1920 Lillard.

#### US005986237A

### [11] Patent Number: 5,986,237

### [45] **Date of Patent:** Nov. 16, 1999

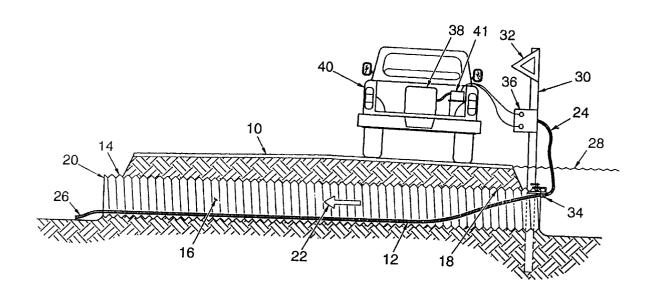
3,823,304 7/1974 Siemianowski ..... 219/213

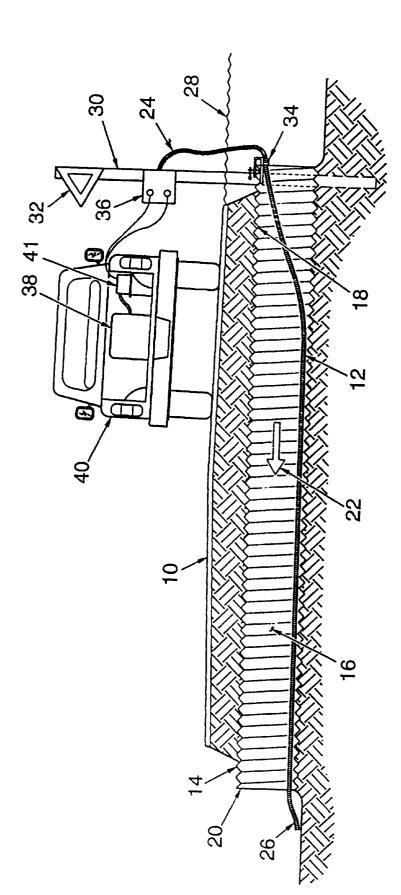
Primary Examiner—Teresa Walberg Assistant Examiner—Thor S. Campbell Attorney, Agent, or Firm—Davis and Bujold

#### [57] ABSTRACT

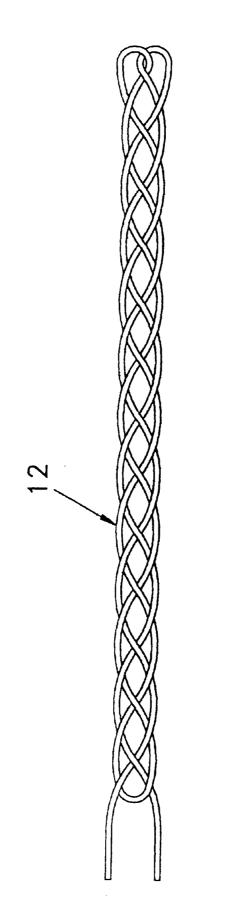
A method for thawing frozen road culverts. The first step involves positioning an electrically conductive cable in a road culvert prior to an ice blockage occurring. A connection end of the electrically conductive cable is anchored in an accessible location. The second step involves connecting a power source to the connection end of the electrically conductive cable after an ice blockage of the road culvert has occurred and supplying power to the electrically conductive cable, such that energy generated by power flowing through the electrically conductive cable causes a flow path to be created through the ice blockage in the road culvert.

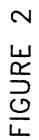
#### 7 Claims, 2 Drawing Sheets











#### METHOD FOR THAWING FROZEN ROAD **CULVERTS**

#### FIELD OF THE INVENTION

The present invention relates to a method for thawing 5 conductive cable illustrated in FIG. 1. frozen road culverts.

#### BACKGROUND OF THE INVENTION

With the coming of spring every year there is a daily cycle of melting and freezing. The heat of the sun during the day 10causes snow to melt. As the sun goes down the temperature falls and water resulting from melting of the snow freezes.

Culverts are strategically placed under roads which are in a path followed by a flow of water from the melting snow. The culverts divert the flow of water so the road does not 15 wash out. Unfortunately, the daily cycle of melting and freezing sometimes results in a culvert becoming blocked by an ice plug. If the ice plug is not removed in a timely fashion, the flow of water seeks an alternative path which often results in a washing out of portions of the road.

At the present time, steam truck crews are dispatched whenever it is noted that a culvert is plugged by ice. Removal of an ice plug from a culvert is generally a slow process. High pressure steam is injected into the ice plug, usually from a downstream side of the culvert, until a flow of water is restored. An ice plug that extends part way into a culvert generally can be removed by high pressure steam within three hours. Ice plugs that extend completely through a culvert can take considerably longer to remove.

The problem of road culverts plugging with ice has 30 become so prevalent, that oversize culverts are frequently used for the express purpose of reducing the frequency of the problem.

#### SUMMARY OF THE INVENTION

What is required is a more time efficient method of thawing frozen road culverts.

According to one aspect of the present invention there is provided a method for thawing frozen road culverts. The first step involves positioning an electrically conductive 40 cable in a road culvert prior to an ice blockage occurring. A connection end of the electrically conductive cable is anchored in an accessible location. The second step involves connecting a power source to the connection end of the road culvert has occurred and supplying power to the electrically conductive cable, such that energy generated by power flowing through the electrically conductive cable causes a flow path to be created through the ice blockage in the road culvert.

According to another aspect of the present invention, there provided, a combination including a road culvert and an electrically conductive cable. The road culvert has an interior bore with an upstream end and a downstream end relative to normal water flow. The electrically conductive 55 cable is positioned in the interior bore and extends substantially the length of the road culvert from the upstream end toward the downstream end. A connection end of the electrically conductive cable is anchored in an accessible location, such that a power source connectable to the connection end of the electrically conductive cable to supply power to energize the electrically conductive cable.

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#### BRIEF DESCRIPTION OF THE DRAWINGS

These and other features of the invention will become 65 tection with a breaker trip mechanism. more apparent from the following description in which reference is made to the appended drawings, wherein:

FIG. 1 is a front elevation view, in section, of a culvert that has been equipped with an electrically conductive cable in accordance with the teachings of the present method.

FIG. 2 is a detailed top plan view of a electrically

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The preferred method for thawing frozen road culverts will now be described with reference to FIG. 1.

The teachings of the preferred method, as will hereafter be further described, require that an electrically conductive cable 12 be positioned in a road culvert 14. Road is generally indicated by reference numeral 10. Road culvert 14 has an interior bore 16 with an upstream end 18 and a downstream end 20 relative to a direction of normal water flow as indicated by arrow 22. Electrically conductive cable 12 has a connection end 24 and a remote end 26. Beneficial results have been obtained using electrically conductive cable 12 made from #10 insulated copper wire, although in applica-20 tions requiring higher temperatures wire made from alloys that can withstand higher temperatures may be used. Electrically conductive cable 12 is positioned in interior bore 16 of road culvert 14 and, preferably, extends substantially the length of road culvert 14 from upstream end 18 toward downstream end 20. It is essential that electrically conductive cable 12 is positioned at upstream end 18, for it is at upstream end 18 that a lockage by ice is most likely to occur. It is not always ssential that electrically conductive cable 12 reach all the ay to downstream end 20. Each installation must be made having regard to surface topography and other conditions prevailing. Some road culverts become blocked at both ends, others are prone only to upstream blockage. Connection end 24 of electrically conductive cable 12 is 35 anchored in an accessible location. When choosing an accessible location must bear in mind the conditions that will prevail when an ice blockage condition is encountered. There is likely to be an accumulation of water upstream of road culvert 14, so the accessible location ispeferably above a high water mark generally indicated by reference numeral 28. There is also likely to be an accumulation of snow on the ground, so connection end 24 is preferably a sufficient height to be above any accumulation of snow. In order to achieve this objective, it is preferred that connection end 24 be electrically conductive cable after an ice blockage of the 45 mounted onto a post 30. Post 30 can be marked with a sign 32 or otherwise marked so as to be readily identified by work crews. In order to ensure that electrically conductive cable 12 does not shift after installation, it is preferred that electrically conductive cable 12 be clamped by means of clamp 34 to upstream end 18 of road culvert 14. Connection 50 end 24 of electrically conductive cable 12 is preferably is connected to a junction box 36. A power source 38 is used to supply power to electrically conductive cable 12. For safety reasons, a low voltage direct current power source which generates six to forty volts is preferred. It will be appreciated that the power required will vary with the gauge and length of electrically conductive cable 12 used. It is not viewed as being cost effective to have a power source at every installation. It is viewed as being more practical to take power source 38 to the particular road culvert that is blocked, it is, therefore, preferred that power source 38 be mounted on a truck 40. For reasons of safety, it is preferred that power source 38 have a control box 41 which include features that control current and provide overcurrent pro-

> The use and operation of the above described combination in accordance with the teachings of the preferred method

will now be described. The first step involves positioning electrically conductive cable 12 in road culvert 14 prior to an ice blockage occurring. Of course, after an ice blockage has occurred it is too late to insert electrically conductive cable 12. Historical data can be used to select those of road 5 culverts 14 that are most prone to ice blockage. Connection end 24 of electrically conductive cable 24 is anchored in an accessible location, such as post 30. It is preferred that cable be secured to road culvert 14 at upstream end 18 by means of clamp 34. Cable 24 is then laid through road culvert 14. 10

The second step involves connecting power source 38 to connection end 24 of electrically conductive cable 12 after an ice blockage (not shown) of road culvert 14 has occurred. As low voltage power source 38 is truck mounted, truck 40 can be dispatched. The connection of power source  $\mathbf{38}$  to  $^{15}$ connection end 24 of electrically conductive cable 12 is made through junction box 36. Power source 38 provides power to electrically conductive cable 12. Tests have shown that energy generated by electrically conductive cable 12 causes a flow path to be created through the ice blockage in  $\ ^{20}$ the immediate vicinity of electrically conductive cable 12. The resulting flow of water then tends to accelerate the process of removing the blockage by rapidly washing away the ice. A trickle of water through road culvert 14 generally occurs in as little as two minutes and normal flow through  $\ ^{25}$ road culvert 14 is generally restored within ten minutes. The rapid clearing of the blockage is believed to be due to more than just the heat generated by power passing through electrically conductive cable 12.

Referring to FIG. 2, in addition to thermal energy, there is <sup>30</sup> believed to be an eddy current induced. In order to enhance this effect cable 12 is looped lengthwise back and forth in boustrophedonic fashion. The loops are then twisted together in order to make cable 12 more compact and easier to handle. Regardless of what forces are at work, the energy <sup>35</sup> generated can be objectively shown to clear an ice blockage in a remarkably short time.

It will be apparent to one skilled in the art that modifications may be made to the illustrated embodiment without departing from the spirit and scope of the invention as hereinafter defined in the Claims.

The embodiments of the invention in which an exclusine property or privilege is claimed are defined as follows:

1. A method for thawing frozen road culverts, comprising  $_{45}$  the steps of:

- positioning an electrically conductive cable in a road culvert prior to an ice blockage occurring, with a connection end of the electrically conductive cable anchored in an accessible location;
- dispatching a mobile low voltage power source to the road culvert when a blockage occurs; and

- connecting the power source to the connection end of the electrically conductive cable and supplying power to the electrically conductive cable, such that energy generated by power flowing through the electrically conductive cable causes a flow path to be created through an ice blockage in the road culvert.
- 2. In combination:
- a road culvert having an interior bore;
- an electrically conductive cable positioned in the interior bore and extending substantially the length of the road culvert;
- a connection end of the electrically conductive cable being anchored in an accessible location, such that a power source is connectable to the connection end of the electrically conductive cable to supply power to energize the electrically conductive cable; and
- a mobile low voltage power source for supplying power to the electrically conductive cable.

3. The combination as defined in claim 2, wherein the road culvert has with an upstream end and a downstream end relative to normal water flow, the cable extending from the upstream end toward the downstream end.

4. The combination as defined in claim 2, wherein the cable is looped lengthwise back and forth in boustrophedonic fashion.

5. The combination as defined in claim 4, wherein the cable is twisted.

**6**. A method for thawing frozen road culverts, comprising the steps of:

- positioning an electrically conductive cable in a road culvert prior to an ice blockage occurring, with a connection end of the electrically conductive cable anchored in an accessible location outside the road culvert and an opposite end of the cable being unattended and extending completely through the road culvert and projecting out through the opposite end thereof;
  - dispatching a mobile low voltage power source to the road culvert when a blockage occurs in the road culvert; and
- connecting the power source to the connection end of the electrically conductive cable and supplying electrical power to the electrically conductive cable, such that energy generated by the electrical power flowing through the electrically conductive cable causes a flow path to be created through the ice blockage in the road culvert thereby assisting with thawing of the road culvert.

7. The combination of claim 2 wherein the accessible location of the connection end of the cable is located outside 50 the road culvert so as to be accessible.

\* \* \* \* \*



# APPENDIX D

## **PHASED COST ESTIMATES**





#### **Community and Government Services - Government of Nunavut Class 'D' Cost Estimate** It **TETRA TECH** Tetra Tech Project WTRM03118-01 - Kimmirut Drainage Project **Preliminary Estimate of Probable Costs** Total Preliminaries \$242,972 Civil Works \$1,313,715 Miscellaneous \$60,000 Sub-total \$1,616,687 Project Contingencies 40.0% \$646.675 **Total Estimated Construction Cost** \$2,263,361 NMS Specs Preliminaries Unit **Est Quantity** Est. Unit Price Est. Total Mob / Demob, Temporary Facilities, Security, 01 25 01 0-1 Quality Control, etc. lump sum 1 \$146,971.50 \$146,972 01 35 14 0-2 Traffic Control, Barricades, and Temporary Signage lump sum 1 \$16,000.00 \$16,000 01 71 00 0-3 Construction Surveys 1 \$80,000.00 \$80,000 lump sum Sub-total Preliminaries \$242,972 **Civil Works** Unit Est Ouantity **Est. Unit Price** Est. Total 31 14 11 1-1 Excavation and Off-Site Disposal 500 \$30.00 \$15,000 cu.m Supply and Install 450 mm Steel Casing Culvert 1-2 \$527.00 \$196,044 33 42 13 m 372 33 42 13 1-3 Supply and Install 600 mm Steel Casing Culvert \$707.00 \$139,279 197 m 33 42 13 1-4 Supply and Install 750 mm Steel Casing Culvert 50 \$888.00 \$44,400 m 33 42 13 1-5 Supply and Install 900 mm Steel Casing Culvert 24 \$1.068.00 \$25,632 m 33 42 13 1-6 Supply and Install 1400 mm Steel Casing Culvert \$1,610.00 \$74,060 m 46 31 37 10 1-7 Supply and Place 50 kg Class Riprap 310 \$200.00 \$62,000 cu. m 1-8 Supply and Place 10 kg Class Riprap \$100.00 \$396,300 31 37 10 cu. m 3,963 1-9 Supply and Place 50 - 75 mm Clear Crush \$100.00 \$23,100 31 37 10 231 cu. m 31 32 21 1-10 Supply and Place Non-Woven Geotextile 14,195 \$20.00 \$283,900 sq. m 02 41 13 1-11 \$2,000.00 \$54,000 Culvert Removal and Off-Site Disposal 27 each Sub-total Site Services \$1,313,715 Miscellaneous Est Ouantity **Est. Unit Price** Est. Total Unit 01 35 43 1 \$20,000.00 2-1 Dewatering lump sum \$20,000 01 35 43 2-2 Sediments and Erosion Control Measures \$40,000.00 \$40,000 lump sum 1 Sub-total Miscellaneous \$60.000 Notes: 1 Quantities shown on this table are estimates and provided for reference only.



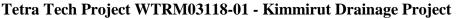
## **Community and Government Services - Government of Nunavut** Class 'D' Cost Estimate - Phase 1 Tetra Tech Project WTRM03118-01 - Kimmirut Drainage Project

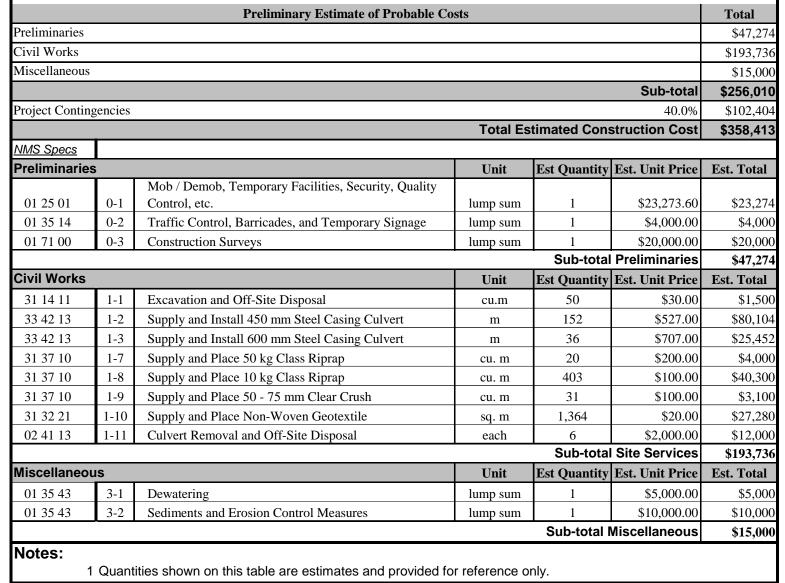
TETRA TECH

|                         |                  | Tetra Tech Project WTRW05118-01 - R                  |                  | <u> </u>      |                                   |  |
|-------------------------|------------------|--|------------------|---------------|-----------------------------------|--|
|                         |                  | Preliminary Estimate of Probable C                   | osts             |               |                                   | Total                                  |
| Preliminaries           |                  |  |                  |               |                                   | \$58,25                                |
| Civil Works             |                  |  |                  |               |                                   | \$303,52                               |
| Miscellaneous           |                  |  |                  |               |                                   | \$15,00                                |
|                         |                  |  |                  |               | Sub-total                         | \$376,77                               |
| Project Contin          | igencies         |  |                  |               | 40.0%                             | \$150,71                               |
|                         | -                |  | Total I          | Estimated Cor | nstruction Cost                   | \$527,48                               |
| <u>NMS Specs</u>        |                  |  |                  |               |                                   |  |
| Preliminarie            | S                |  | Unit             | Est Quantity  | Est. Unit Price                   | Est. Total                             |
|                         |                  | Mob / Demob, Temporary Facilities, Security, Quality |                  |               |                                   |  |
| 01 25 01                | 0-1              | Control, etc.  | lump sum         | 1             | \$34,252.40                       | \$34,25                                |
| 01 35 14                | 0-2              | Traffic Control, Barricades, and Temporary Signage   | lump sum         | 1             | \$4,000.00                        | \$4,00                                 |
| 01 71 00                | 0-3              | Construction Surveys                                 | lump sum         | 1             | \$20,000.00                       | \$20,00                                |
|                         |                  |  |                  |               | al Preliminaries                  | \$58,25                                |
| Civil Works             |                  |  | Unit             | Est Quantity  | Est. Unit Price                   | Est. Total                             |
| 31 14 11                | 1-1              | Excavation and Off-Site Disposal                     | cu.m             | 60            | \$30.00                           | \$1,80                                 |
| 33 42 13                | 1-2              | Supply and Install 450 mm Steel Casing Culvert       | m                | 20            | \$527.00                          | \$10,54                                |
| 33 42 13                | 1-3              | Supply and Install 600 mm Steel Casing Culvert       | m                | 24            | \$707.00                          | \$16,96                                |
| 33 42 13                | 1-4              | Supply and Install 750 mm Steel Casing Culvert       | m                | 17            | \$888.00                          | \$15,09                                |
| 33 42 13                | 1-6              | Supply and Install 1400 mm Steel Casing Culvert      | m                | 46            | \$1,610.00                        | \$74,06                                |
| 31 37 10                | 1-7              | Supply and Place 50 kg Class Riprap                  | cu. m            | 238           | \$200.00                          | \$47,60                                |
| 31 37 10                | 1-8              | Supply and Place 10 kg Class Riprap                  | cu. m            | 728           | \$100.00                          | \$72,80                                |
| 31 32 21                | 1-10             | Supply and Place Non-Woven Geotextile                | sq. m            | 2,733         | \$20.00                           | \$54,66                                |
|                         | 1-11             | Culvert Removal and Off-Site Disposal                | each             | 5             | \$2,000.00                        | \$10,00                                |
| 02 41 13                |                  |  | -                | Sub-tota      | al Site Services                  | \$303,52                               |
| 02 41 13                |                  |  |                  |               |                                   |  |
| 02 41 13<br>Miscellaneo | us               |  | Unit             | Est Quantity  | Est. Unit Price                   | Est. Total                             |
|                         | <b>us</b><br>2-1 | Dewatering   | Unit<br>lump sum | Est Quantity  | <b>Est. Unit Price</b> \$5,000.00 |  |
| Miscellaneo             |                  | Dewatering<br>Sediments and Erosion Control Measures |                  | e 1           |                                   | <b>Est. Total</b><br>\$5,00<br>\$10,00 |



## Community and Government Services - Government of Nunavut Class 'D' Cost Estimate - Phase 2





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**TETRA TECI** 



# **Community and Government Services - Government of Nunavut** Class 'D' Cost Estimate - Phase 3



Tetra Tech Project WTRM03118-01 - Kimmirut Drainage Project

|                      | Preliminary Estimate of Probable Costs |  |          |              |                  |            |  |
|----------------------|--|--|----------|--------------|------------------|------------|--|
| Preliminaries        |  |  |          |              |                  | \$48,110   |  |
| Civil Works          |  |  |          |              |                  | \$202,104  |  |
| Miscellaneous        |  |  |          |              |                  | \$15,000   |  |
|                      |  |  |          |              | Sub-total        | \$265,214  |  |
| Project Contin       | gencies                                |  |          |              | 40.0%            | \$106,086  |  |
|                      | -                                      |  | Total E  | stimated Cor | struction Cost   | \$371,300  |  |
| <u>NMS Specs</u>     |  |  | -        |              |                  |            |  |
| Preliminaries        | s                                      |  | Unit     | Est Quantity | Est. Unit Price  | Est. Total |  |
|                      |  | Mob / Demob, Temporary Facilities, Security, Quality |          |              |                  |            |  |
| 01 25 01             | 0-1                                    | Control, etc.  | lump sum | 1            | \$24,110.40      | \$24,110   |  |
| 01 35 14             | 0-2                                    | Traffic Control, Barricades, and Temporary Signage   | lump sum | 1            | \$4,000.00       | \$4,000    |  |
| 01 71 00             | 0-3                                    | Construction Surveys                                 | lump sum | 1            | \$20,000.00      | \$20,000   |  |
|                      |  |  |          |              | al Preliminaries | \$48,110   |  |
| Civil Works          |  |  | Unit     | Est Quantity |                  | Est. Total |  |
| 31 14 11             | 1-1                                    | Excavation and Off-Site Disposal                     | cu.m     | 100          | \$30.00          | \$3,000    |  |
| 33 42 13             | 1-2                                    | Supply and Install 450 mm Steel Casing Culvert       | m        | 69           | \$527.00         | \$36,363   |  |
| 33 42 13             | 1-3                                    | Supply and Install 600 mm Steel Casing Culvert       | m        | 71           | \$707.00         | \$50,197   |  |
| 33 42 13             | 1-4                                    | Supply and Install 750 mm Steel Casing Culvert       | m        | 13           | \$888.00         | \$11,544   |  |
| 31 37 10             | 1-8                                    | Supply and Place 10 kg Class Riprap                  | cu. m    | 511          | \$100.00         | \$51,100   |  |
| 31 37 10             | 1-9                                    | Supply and Place 50 - 75 mm Clear Crush              | cu. m    | 33           | \$100.00         | \$3,300    |  |
| 31 32 21             | 1-10                                   | Supply and Place Non-Woven Geotextile                | sq. m    | 1,730        | \$20.00          | \$34,600   |  |
| 02 41 13             | 1-11                                   | Culvert Removal and Off-Site Disposal                | each     | 6            | \$2,000.00       | \$12,000   |  |
|                      |  |  |          | Sub-tota     | al Site Services | \$202,104  |  |
| Miscellaneous        |  |  |          | Est Quantity | Est. Unit Price  | Est. Total |  |
|                      | 2-1                                    | Dewatering   | lump sum | 1            | \$5,000.00       | \$5,000    |  |
| 01 35 43             |  |  | 1        | 1 .          |                  |            |  |
| 01 35 43<br>01 35 43 | 2-2                                    | Sediments and Erosion Control Measures               | lump sum | 1            | \$10,000.00      | \$10,000   |  |



## Community and Government Services - Government of Nunavut Class 'D' Cost Estimate - Phase 4



Tetra Tech Project WTRM03118-01 - Kimmirut Drainage Project

|                  |         | Preliminary Estimate of Probable Co                    | osts         |                     |                  | Total       |
|------------------|---------|--|--------------|---------------------|------------------|-------------|
| Preliminaries    |         |  |              |                     |                  | \$89,335    |
| Civil Works      |         |  |              |                     |                  | \$614,351   |
| Miscellaneous    |         |  |              |                     |                  | \$15,000    |
|                  |         |  |              |                     | Sub-total        | \$718,686   |
| Project Conting  | gencies |  |              |                     | 40.0%            | \$287,474   |
|                  | _       |  | Total E      | stimated Cor        | struction Cost   | \$1,006,161 |
| <u>NMS Specs</u> |         |  |              |                     |                  |             |
| Preliminaries    |         |  | Unit         | <b>Est Quantity</b> | Est. Unit Price  | Est. Total  |
|                  |         | Mob / Demob, Temporary Facilities, Security, Quality   |              |                     |                  |             |
| 01 25 01         | 0-1     | Control, etc.  | lump sum     | 1                   | \$65,335.10      | \$65,335    |
| 01 35 14         | 0-2     | Traffic Control, Barricades, and Temporary Signage     | lump sum     | 1                   | \$4,000.00       | \$4,000     |
| 01 71 00         | 0-3     | Construction Surveys                                   | lump sum     | 1                   | \$20,000.00      | \$20,000    |
|                  |         |  |              |                     | al Preliminaries | \$89,335    |
| Civil Works      |         |  | Unit         | Est Quantity        | Est. Unit Price  | Est. Total  |
| 31 14 11         | 1-1     | Excavation and Off-Site Disposal                       | cu.m         | 290                 | \$30.00          | \$8,700     |
| 33 42 13         | 1-2     | Supply and Install 450 mm Steel Casing Culvert         | m            | 131                 | \$527.00         | \$69,037    |
| 33 42 13         | 1-3     | Supply and Install 600 mm Steel Casing Culvert         | m            | 66                  | \$707.00         | \$46,662    |
| 33 42 13         | 1-4     | Supply and Install 750 mm Steel Casing Culvert         | m            | 20                  | \$888.00         | \$17,760    |
| 33 42 13         | 1-5     | Supply and Install 900 mm Steel Casing Culvert         | m            | 24                  | \$1,068.00       | \$25,632    |
| 31 37 10         | 1-7     | Supply and Place 50 kg Class Riprap                    | cu. m        | 52                  | \$200.00         | \$10,400    |
| 31 37 10         | 1-8     | Supply and Place 10 kg Class Riprap                    | cu. m        | 2,321               | \$100.00         | \$232,100   |
| 31 37 10         | 1-9     | Supply and Place 50 - 75 mm Clear Crush                | cu. m        | 167                 | \$100.00         | \$16,700    |
| 31 32 21         | 1-10    | Supply and Place Non-Woven Geotextile                  | sq. m        | 8,368               | \$20.00          | \$167,360   |
| 02 41 13         | 1-11    | Culvert Removal and Off-Site Disposal                  | each         | 10                  | \$2,000.00       | \$20,000    |
|                  |         |  |              | Sub-tota            | al Site Services | \$614,351   |
| Miscellaneous    |         |  |              | <b>Est Quantity</b> | Est. Unit Price  | Est. Total  |
| 01 35 43         | 2-1     | Dewatering   | lump sum     | 1                   | \$5,000.00       | \$5,000     |
| 01 35 43         | 2-2     | Sediments and Erosion Control Measures                 | lump sum     | 1                   | \$10,000.00      | \$10,000    |
|                  |         |  |              | Sub-total           | Miscellaneous    | \$15,000    |
| Notes:<br>1      | Quanti  | ties shown on this table are estimates and provided fo | or reference | only.               |                  |             |



## APPENDIX E

## INVENTORY OF EXISTING CULVERTS AND EROSION





## Table 1: Existing Culverts Inventory

| Label     | Diameter<br>(mm) | Material | Condition         | Picture | Notes |
|-----------|------------------|----------|-------------------|---------|-------|
| Culvert 1 | 600              | csp      | blocked           |         |       |
| Culvert 2 | 500              | csp      | damaged           |         |       |
| Culvert 3 | 500              | csp      | partially blocked |         |       |
| Culvert 4 | 1000             | csp      | damaged           |         |       |
| Culvert 5 | 500              | csp      | damaged           |         |       |



### HAMLET OF KIMMIRUT - MASTER DRAINAGE PLAN FILE: 704-TRN.WTRM03118-02 | FEBRUARY 2020 | ISSUED FOR USE



| Label     | Diameter<br>(mm) | Material | Condition         | Picture | Notes             |
|-----------|------------------|----------|-------------------|---------|-------------------|
| Culvert 6 | 500              | csp      | blocked           |         | Reverse<br>graded |
| Culvert 7 | 500              | csp      | blocked           |         |                   |
| Culvert 8 | 150              | рус      |                   |         |                   |
| Culvert 9 | 500              | csp      | partially blocked |         | buried            |





| Label      | Diameter<br>(mm) | Material | Condition | Picture | Notes  |
|------------|------------------|----------|-----------|---------|--------|
| Culvert 10 | 500              | csp      | damaged   |         |        |
| Culvert 11 | 1200             | csp      | damaged   |         |        |
| Culvert 12 | 100              |          | blocked   |         |        |
| Culvert 13 | 500              |          | blocked   |         | buried |
| Culvert 14 | 300              |          |           |         |        |
| Culvert 15 | 1000             | csp      | damaged   |         |        |
| Culvert 16 | 1200             | csp      | damaged   |         |        |





| Culvert 17 | 750 |     | blocked |        |
|------------|-----|-----|---------|--------|
|            |     |     |         | buried |
| Culvert 18 | 600 | csp | blocked |        |
| Culvert 19 | 600 | csp | damaged |        |
|            | 600 | csp | damaged |        |





| Label      | Diameter<br>(mm) | Material     | Condition         | Picture | Notes                |
|------------|------------------|--------------|-------------------|---------|----------------------|
| Culvert 22 | 600              |              | damaged           |         |                      |
| Culvert 23 | 2 x 150          | steel casing | partially blocked |         | undersized           |
| Culvert 24 |                  | csp          |                   |         | buried,<br>anecdotal |
| Culvert 25 |                  |              | blocked           |         |                      |
| Culvert 26 | 1200             | csp          | damaged           |         |                      |



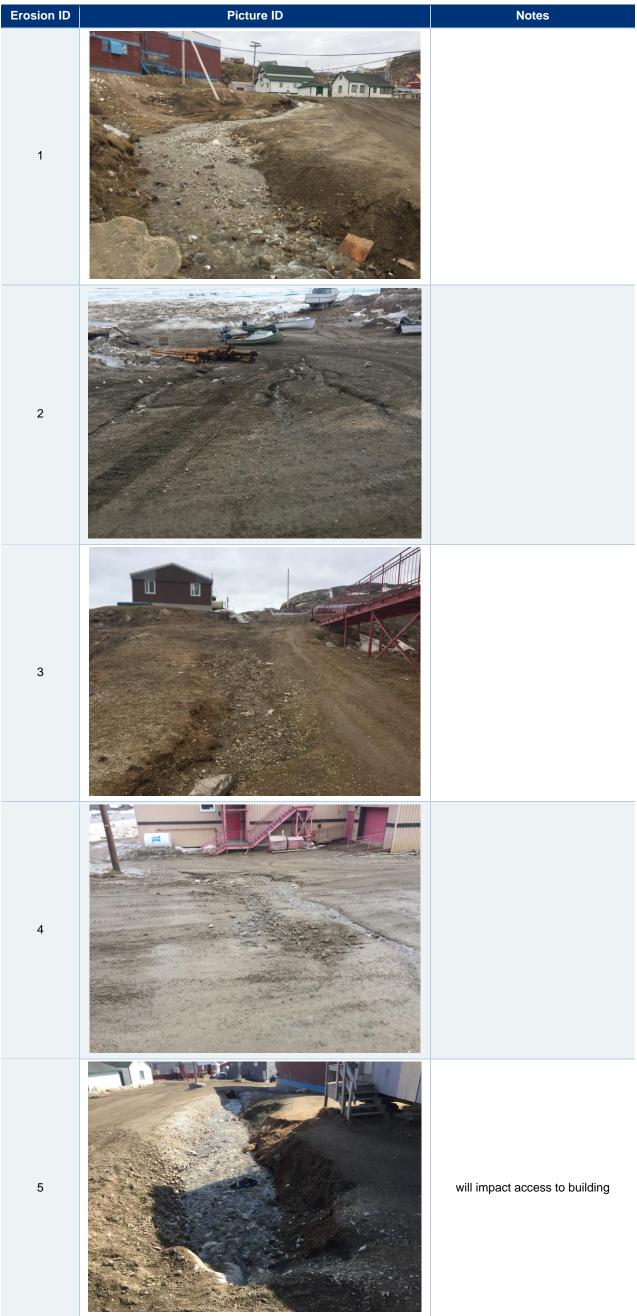


| Label      | Diameter<br>(mm) | Material | Condition         | Picture | Notes                |
|------------|------------------|----------|-------------------|---------|----------------------|
| Culvert 27 |                  | csp      | damaged           |         |                      |
| Culvert 28 |                  |          | buried, anecdotal |         | buried,<br>anecdotal |
| Culvert 29 |                  |          | blocked           |         | not<br>assessed      |
| Culvert 30 |                  | csp      | partially blocked |         | not<br>assessed      |
| Culvert 31 |                  |          | blocked           |         | buried               |
| Culvert 32 | 500              |          | damaged           |         |                      |





### Table 2: Erosion Inventory





| Erosion ID | Picture ID | Notes |
|------------|------------|-------|
| 6          |            |       |
| 7          |            |       |



# APPENDIX F

## LIST OF PROPOSED CULVERTS





| Name      | Upgrade<br>Type    | Proposed<br>Phase | Material | Wall<br>Thickness<br>(mm) | Length<br>(m) | Diameter<br>(mm) | Max.<br>Flow<br>(m³/s) | Max.<br>Velocity<br>(m/s) | Max/Full<br>Depth<br>(%) |
|-----------|--------------------|-------------------|----------|---------------------------|---------------|------------------|------------------------|---------------------------|--------------------------|
| Culvert1  | replace<br>culvert | 4                 | SWSP     | 10-12                     | 7.5           | 450              | 0.05                   | 2.57                      | 31                       |
| Culvert2  | replace<br>culvert | 4                 | SWSP     | 10-12                     | 14.4          | 600              | 0.24                   | 4.13                      | 26                       |
| Culvert3  | replace<br>culvert | 3                 | SWSP     | 10-12                     | 17.0          | 450              | 0.09                   | 3.39                      | 27                       |
| Culvert4  | replace<br>culvert | 3                 | SWSP     | 10-12                     | 13.1          | 750              | 0.40                   | 2.49                      | 43                       |
| Culvert5  | replace<br>culvert | 3                 | SWSP     | 10-12                     | 19.9          | 600              | 0.11                   | 2.08                      | 32                       |
| Culvert6  | replace<br>culvert | 3                 | SWSP     | 10-12                     | 18.6          | 600              | 0.18                   | 1.76                      | 51                       |
| Culvert8  | replace<br>culvert | 2                 | SWSP     | 10-12                     | 12.2          | 450              | 0.04                   | 1.92                      | 35                       |
| Culvert10 | replace<br>culvert | 2                 | SWSP     | 10-12                     | 10.9          | 450              | 0.08                   | 1.48                      | 37                       |
| Culvert11 | replace<br>culvert | 1                 | SWSP     | 10-12                     | 24.9          | 1400             | 1.43                   | 5.70                      | 22                       |
| Culvert12 | replace<br>culvert | 2                 | SWSP     | 10-12                     | 5.7           | 450              | 0.00                   | 0.54                      | 3                        |
| Culvert13 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 14.7          | 450              | 0.12                   | 3.28                      | 27                       |
| Culvert14 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 12.9          | 450              | 0.13                   | 4.49                      | 24                       |
| Culvert15 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 20.3          | 600              | 0.20                   | 3.72                      | 24                       |
| Culvert16 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 15.6          | 450              | 0.13                   | 2.20                      | 41                       |
| Culvert17 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 24.1          | 900              | 0.73                   | 5.31                      | 27                       |
| Culvert19 | replace<br>culvert | 1                 | SWSP     | 10-12                     | 23.3          | 600              | 0.19                   | 3.87                      | 29                       |
| Culvert20 | replace<br>culvert | 1                 | SWSP     | 10-12                     | 16.8          | 750              | 0.31                   | 4.99                      | 22                       |
| Culvert21 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 15.3          | 450              | 0.10                   | 1.20                      | 54                       |
| Culvert22 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 19.8          | 750              | 0.38                   | 3.33                      | 34                       |
| Culvert23 | replace<br>culvert | 2                 | SWSP     | 10-12                     | 5.8           | 450              | 0.06                   | 1.78                      | 46                       |

### Table 1: Proposed Culverts





| Name      | Upgrade<br>Type    | Proposed<br>Phase | Material | Wall<br>Thickness<br>(mm) | Length<br>(m) | Diameter<br>(mm) | Max.<br>Flow<br>(m³/s) | Max.<br>Velocity<br>(m/s) | Max/Full<br>Depth<br>(%) |
|-----------|--------------------|-------------------|----------|---------------------------|---------------|------------------|------------------------|---------------------------|--------------------------|
| Culvert24 | replace<br>culvert | 2                 | SWSP     | 10-12                     | 35.2          | 600              | 0.25                   | 5.03                      | 23                       |
| Culvert25 | replace<br>culvert | 2                 | SWSP     | 10-12                     | 24.0          | 450              | 0.05                   | 1.60                      | 31                       |
| Culvert26 | replace<br>culvert | 1                 | SWSP     | 10-12                     | 7.8           | 1400             | 1.35                   | 4.64                      | 24                       |
| Culvert27 | replace<br>culvert | 1                 | SWSP     | 10-12                     | 12.8          | 1400             | 1.35                   | 3.69                      | 29                       |
| Culvert28 | replace<br>culvert | 3                 | SWSP     | 10-12                     | 10.9          | 450              | 0.08                   | 3.79                      | 23                       |
| Culvert31 | replace<br>culvert | 3                 | SWSP     | 10-12                     | 31.8          | 600              | 0.12                   | 1.12                      | 42                       |
| Culvert32 | replace<br>culvert | 4                 | SWSP     | 10-12                     | 24.5          | 450              | 0.06                   | 1.45                      | 32                       |
| Culvert33 | new<br>culvert     | 4                 | SWSP     | 10-12                     | 8.1           | 600              | 0.17                   | 4.72                      | 24                       |
| Culvert34 | new<br>culvert     | 4                 | SWSP     | 10-12                     | 17.0          | 450              | 0.14                   | 2.75                      | 35                       |
| Culvert35 | new<br>culvert     | 3                 | SWSP     | 10-12                     | 12.2          | 450              | 0.08                   | 2.03                      | 36                       |
| Culvert36 | new<br>culvert     | 3                 | SWSP     | 10-12                     | 12.0          | 450              | 0.15                   | 3.10                      | 33                       |
| Culvert37 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 10.8          | 450              | 0.08                   | 2.54                      | 29                       |
| Culvert38 | new<br>culvert     | 4                 | SWSP     | 10-12                     | 12.6          | 600              | 0.21                   | 2.59                      | 33                       |
| Culvert39 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 11.9          | 450              | 0.00                   | 0.91                      | 2                        |
| Culvert40 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 13.3          | 450              | 0.00                   | 2.35                      | 4                        |
| Culvert41 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 14.6          | 450              | 0.01                   | 1.86                      | 9                        |
| Culvert42 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 11.7          | 450              | 0.04                   | 1.24                      | 42                       |
| Culvert43 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 14.8          | 450              | 0.08                   | 1.64                      | 42                       |
| Culvert44 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 8.1           | 450              | 0.07                   | 3.42                      | 22                       |
| Culvert45 | new<br>culvert     | 2                 | SWSP     | 10-12                     | 7.8           | 450              | 0.05                   | 3.41                      | 25                       |
| Culvert46 | new<br>culvert     | 4                 | SWSP     | 10-12                     | 10.6          | 600              | 0.19                   | 2.99                      | 36                       |



| Name      | Upgrade<br>Type | Proposed<br>Phase | Material | Wall<br>Thickness<br>(mm) | Length<br>(m) | Diameter<br>(mm) | Max.<br>Flow<br>(m³/s) | Max.<br>Velocity<br>(m/s) | Max/Full<br>Depth<br>(%) |
|-----------|-----------------|-------------------|----------|---------------------------|---------------|------------------|------------------------|---------------------------|--------------------------|
| Culvert47 | new<br>culvert  | 4                 | SWSP     | 10-12                     | 9.8           | 450              | 0.03                   | 1.53                      | 36                       |
| Culvert48 | new<br>culvert  | 4                 | SWSP     | 10-12                     | 13.0          | 450              | 0.06                   | 2.11                      | 40                       |
| Culvert49 | new<br>culvert  | 1                 | SWSP     | 10-12                     | 19.7          | 450              | 0.06                   | 0.81                      | 54                       |
| Culvert50 | new<br>culvert  | 3                 | SWSP     | 10-12                     | 16.0          | 450              | 0.06                   | 2.61                      | 24                       |





|                 |                             |                      |                             | In                      | let                      | Οι                      | utlet                    | Total                                 |
|-----------------|-----------------------------|----------------------|-----------------------------|-------------------------|--------------------------|-------------------------|--------------------------|---------------------------------------|
| Culvert<br>Name | Culvert<br>Diameter<br>(mm) | Riprap Class<br>(kg) | Riprap<br>Thickness<br>(mm) | Riprap<br>Length<br>(m) | Riprap<br>Volume<br>(m³) | Riprap<br>Length<br>(m) | Riprap<br>Volume<br>(m³) | Riprap<br>Volume<br>(m <sup>3</sup> ) |
| Culvert1        | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert2        | 600                         | 25                   | 450                         | 1.2                     | 4.1                      | 3.0                     | 6.7                      | 10.9                                  |
| Culvert3        | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert4        | 750                         | 10                   | 350                         | 1.5                     | 5.0                      | 3.8                     | 8.2                      | 13.2                                  |
| Culvert5        | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                                   |
| Culvert6        | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                                   |
| Culvert8        | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert10       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert11       | 1400                        | 50                   | 550                         | 2.8                     | 27.4                     | 7.0                     | 44.9                     | 72.3                                  |
| Culvert12       | 450                         | 25                   | 450                         | 0.9                     | 2.3                      | 2.3                     | 3.8                      | 6.1                                   |
| Culvert13       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert14       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert15       | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                                   |
| Culvert16       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert17       | 900                         | 50                   | 550                         | 1.8                     | 11.3                     | 4.5                     | 18.6                     | 29.9                                  |
| Culvert19       | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                                   |
| Culvert20       | 750                         | 50                   | 550                         | 1.5                     | 7.9                      | 3.8                     | 12.9                     | 20.8                                  |
| Culvert21       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert22       | 750                         | 10                   | 350                         | 1.5                     | 5.0                      | 3.8                     | 8.2                      | 13.2                                  |
| Culvert23       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert24       | 600                         | 50                   | 550                         | 1.2                     | 5.0                      | 3.0                     | 8.2                      | 13.3                                  |
| Culvert25       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert26       | 1400                        | 50                   | 550                         | 2.8                     | 27.4                     | 7.0                     | 44.9                     | 72.3                                  |
| Culvert27       | 1400                        | 50                   | 550                         | 2.8                     | 27.4                     | 7.0                     | 44.9                     | 72.3                                  |
| Culvert28       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                                   |
| Culvert31       | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                                   |



|                 |                             |                      |                             | In                      | let                      | Οι                      | utlet                    | Total                             |
|-----------------|-----------------------------|----------------------|-----------------------------|-------------------------|--------------------------|-------------------------|--------------------------|-----------------------------------|
| Culvert<br>Name | Culvert<br>Diameter<br>(mm) | Riprap Class<br>(kg) | Riprap<br>Thickness<br>(mm) | Riprap<br>Length<br>(m) | Riprap<br>Volume<br>(m³) | Riprap<br>Length<br>(m) | Riprap<br>Volume<br>(m³) | Total<br>Riprap<br>Volume<br>(m³) |
| Culvert32       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert33       | 600                         | 25                   | 450                         | 1.2                     | 4.1                      | 3.0                     | 6.7                      | 10.9                              |
| Culvert34       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert35       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert36       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert37       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert38       | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                               |
| Culvert39       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert40       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert41       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert42       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert43       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert44       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert45       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert46       | 600                         | 10                   | 350                         | 1.2                     | 3.2                      | 3.0                     | 5.2                      | 8.5                               |
| Culvert47       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert48       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert49       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
| Culvert50       | 450                         | 10                   | 350                         | 0.9                     | 1.8                      | 2.3                     | 3.0                      | 4.8                               |
|                 | ne Riprap for prons (m³):   |                      |                             |                         |                          |                         |                          | 523                               |



# APPENDIX G

### **PCSWMM MODEL PARAMETERS**





| Name         | Outlet        | Area<br>(ha) | Width<br>(m)   | Flow<br>Length<br>(m) | Slope<br>(%) | lmperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|--------------|---------------|--------------|----------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S2           | J49           | 1.1659       | 72.87          | 160                   | 14.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S22          | J273          | 0.6326       | 43.6           | 145                   | 15.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S25          | J104          | 0.4805       | 28.59          | 168                   | 17.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S31          | J225          | 0.3709       | 33.45          | 111                   | 18.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S37          | J141          | 0.4023       | 22.93          | 175                   | 19.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S46          | J225          | 0.2992       | 28.68          | 104                   | 18.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$53         | J254          | 0.5614       | 76.66          | 73.2                  | 18.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S77          | SU9           | 0.3725       | 122.9          | 30.3                  | 10.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S80          | SU9           | 0.3373       | 117.8<br>42.89 | 28.6<br>88.4          | 15.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S81<br>S93   | J1723<br>J347 | 0.3791       | 64.65          | 121                   | 19.5<br>15.3 | 0              | 0.01        | 0.1       | 0.05<br>0.05             | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$100        | J49           | 0.4858       | 94.94          | 51.2                  | 17.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S100         | J254          | 0.3009       | 40.13          | 75                    | 20.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S113         | J286          | 0.5272       | 70.78          | 74.5                  | 35.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S154         | J286          | 0.4402       | 58.51          | 75.2                  | 43.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S160         | J112          | 0.6921       | 128.7          | 53.8                  | 11.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S163         | J1713         | 0.9623       | 134.3          | 71.6                  | 17.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S180         | J1872         | 0.872        | 76.51          | 114                   | 10.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S182         | J373          | 0.3659       | 67.56          | 54.2                  | 28.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S184         | J511          | 0.5109       | 97.12          | 52.6                  | 2.16         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S196         | J121          | 0.4791       | 66.46          | 72.1                  | 8.81         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S208         | J389          | 0.5949       | 53.55          | 111                   | 30.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S213         | J424          | 0.264        | 82.44          | 32                    | 11.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S217         | J1692         | 0.822        | 118.2          | 69.6                  | 22.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S219         | J441          | 0.3829       | 64.71          | 59.2                  | 12.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S222         | J424          | 0.2938       | 78.88          | 37.2                  | 12.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S225         | J439          | 0.4285       | 30.09          | 142                   | 31.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S226         | J441          | 0.3016       | 50.05          | 60.3                  | 8.28         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S227         | J159          | 0.5368       | 64.41          | 83.3                  | 1.8          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S228         | J159          | 0.9926       | 72.27          | 137                   | 18.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S236         | J493          | 0.3714       | 125.3          | 29.6                  | 31.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S237         | J497          | 0.4416       | 75.39          | 58.6                  | 25.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S238         | J493          | 0.6725       | 62.52          | 108                   | 14.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S243         | J485          | 0.3522       | 51.76          | 68.1                  | 23.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S246<br>S248 | J533<br>J489  | 1.0309       | 190.2          | 54.2                  | 36.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S248         | J489<br>J515  | 0.5711       | 70.18<br>69.96 | 81.4<br>83.8          | 9.4<br>15    | 0              | 0.01        | 0.1       | 0.05<br>0.05             | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S252         | J497          | 0.3585       | 92.74          | 38.7                  | 17.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S252         | J460          | 0.5163       | 92.09          | 56.1                  | 14.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S262         | J285          | 0.5453       | 81.65          | 66.8                  | 16.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S264         | J495          | 0.5363       | 41.27          | 130                   | 17.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S265         | J485          | 0.2673       | 52.42          | 51                    | 18.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S267         | J495          | 0.2817       | 50.58          | 55.7                  | 18.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S270         | J537          | 0.8904       | 97.99          | 90.9                  | 14.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S271         | J541          | 0.4991       | 61.01          | 81.8                  | 13.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S275         | J274          | 0.0602       | 32.19          | 18.7                  | 8.12         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S276         | J283          | 0.2962       | 17.31          | 171                   | 17.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S277         | J525          | 1.3905       | 79.14          | 176                   | 17.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S280         | J506          | 0.6609       | 68.17          | 97                    | 9.76         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S284         | J1781         | 0.1634       | 47.7           | 34.3                  | 12.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S285         | J511          | 0.5392       | 69.28          | 77.8                  | 18.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S287         | J278          | 0.0015       | 4.056          | 3.7                   | 11.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S288         | J515          | 0.5745       | 73.46          | 78.2                  | 14.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S293         | J1769         | 1.0153       | 58.38          | 174                   | 18.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S296         | J285          | 0.3713       | 81.5           | 45.6                  | 13           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S299         | J523          | 0.6743       | 76.97          | 87.6                  | 17.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S300         | J1822         | 0.7559       | 114.3          | 66.1                  | 24.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S302         | J276          | 0.0165       | 20.23          | 8.16                  | 8.17         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S305         | J1740         | 0.185        | 36.91          | 50.1                  | 15.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$308        | J98           | 0.6301       | 95.24          | 66.2                  | 6.98         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S313<br>S314 | J615          | 0.4502       | 43.28          | 104                   | 13.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S314<br>S315 | J545<br>J545  | 0.3168       | 72.41<br>39.81 | 43.7<br>118           | 13.2<br>17   | 0              | 0.01        | 0.1       | 0.05<br>0.05             | 0.05<br>0.05           | 4                                 | 2                                 | 4                           |                          |
| 2272         | JJ4J          | 0.4703       | 18.55          | 118                   | 1/           | U              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |

### Table 1: Subcatchment PCSWMM Model Parameters



| Name           | Outlet       | Area<br>(ha) | Width<br>(m)   | Flow<br>Length<br>(m) | Slope<br>(%) | lmperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|----------------|--------------|--------------|----------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S319           | J594         | 0.3627       | 35.39          | 102                   | 11.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S323           | J564         | 0.7557       | 58.68          | 129                   | 24.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S324           | SU5          | 0.9136       | 100.7          | 90.7                  | 19           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S327           | J615         | 0.2492       | 75.37          | 33.1                  | 10.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S328           | SU8          | 0.4411       | 56.87          | 77.6                  | 19.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$330          | SU8          | 0.4618       | 54.22          | 85.2                  | 18.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S332<br>S334   | J283<br>J586 | 0.2237       | 6.423<br>27    | 348<br>96.6           | 15<br>22.6   | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S335           | J537         | 0.2508       | 72.42          | 34.6                  | 18.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$336          | J621         | 0.5419       | 54.95          | 98.6                  | 17.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S339           | J272         | 0.0101       | 14.05          | 7.19                  | 9.41         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S340           | J280         | 0.0009       | 2.916          | 3.09                  | 25.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S341           | J290         | 0.0013       | 4.207          | 3.09                  | 14.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S342           | J1822        | 1.4971       | 153.5          | 97.5                  | 22.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S343           | J1804        | 1.1095       | 35.39          | 314                   | 25           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S344           | J606         | 0.3517       | 50.4           | 69.8                  | 14.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$345<br>\$246 | J292         | 0.0046       | 3.126          | 14.7<br>80.7          | 9.99         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S346<br>S347   | J621<br>J588 | 0.8249       | 91.99<br>64.7  | 89.7<br>48.5          | 21.6<br>20.9 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S350           | J674         | 0.5136       | 43.17          | 48.5                  | 39           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S352           | J586         | 0.4501       | 103.6          | 43.4                  | 23.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$354          | J617         | 0.3479       | 31.01          | 112                   | 23.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S357           | J588         | 0.3903       | 54.64          | 71.4                  | 21.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S358           | J649         | 0.8084       | 71.43          | 113                   | 31.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S361           | J525         | 0.5536       | 79.48          | 69.7                  | 32.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S364           | J638         | 0.7162       | 47.19          | 152                   | 30.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S365           | J1757        | 0.3457       | 29.03          | 119                   | 31.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S367           | J634         | 0.8298       | 86.96          | 95.4                  | 17.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$370          | J678         | 0.5248       | 64.33          | 81.6                  | 25.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S373<br>S377   | J629<br>J629 | 0.2769       | 41.42<br>184.4 | 66.9<br>50.2          | 32.7<br>20.6 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S378           | J742         | 0.6565       | 58.83          | 112                   | 37           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S381           | J680         | 0.6861       | 61.64          | 111                   | 24.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S385           | J671         | 0.5798       | 56.51          | 103                   | 25.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S386           | J241         | 0.5338       | 89.33          | 59.8                  | 29.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S388           | J306         | 0.6151       | 82.32          | 74.7                  | 27.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S391           | J683         | 0.4052       | 58.04          | 69.8                  | 18.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S392           | J765         | 0.4744       | 83.37          | 56.9                  | 28.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S396           | J680         | 0.4678       | 69.11          | 67.7                  | 25.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S398           | J634         | 0.4792       | 54.78          | 87.5                  | 21.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S401<br>S406   | Su5<br>SU8   | 0.1363       | 32.32<br>56.46 | 42.2<br>90.2          | 3.52<br>9.82 | 0              | 0.01        | 0.1       | 0.05<br>0.05             | 0.05<br>0.05           | 4                                 | 2                                 | 4                           | 7                        |
| S408           | J706         | 0.2085       | 48.46          | 43                    | 21.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S409           | J792         | 0.5704       | 72.01          | 79.2                  | 22.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S410           | SU5          | 0.4736       | 89.89          | 52.7                  | 7.4          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S412           | J671         | 0.7324       | 107.8          | 67.9                  | 22.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S413           | SU5          | 0.4114       | 47.22          | 87.1                  | 13.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S415           | J748         | 0.0777       | 8.551          | 90.9                  | 24.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S416           | J737         | 0.9494       | 96.55          | 98.3                  | 32.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S417           | J1766        | 0.2777       | 53.98          | 51.4                  | 20.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S418           | J1726        | 0.6458       | 60.99          | 106                   | 26.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S420           | J765         | 0.2946       | 35.9           | 82.1                  | 28.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S421<br>S424   | J748<br>J29  | 0.4061       | 59.03<br>120.6 | 68.8<br>36.2          | 37.7<br>14.4 | 0              | 0.01        | 0.1       | 0.05                     | 0.05<br>0.05           | 4                                 | 2                                 | 4                           | 7                        |
| S424<br>S425   | J29<br>J1789 | 0.437        | 78.25          | 36.2<br>82.4          | 23.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S425           | J737         | 0.3604       | 48.85          | 73.8                  | 8.54         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S429           | J1804        | 0.2558       | 7.433          | 344                   | 34           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S431           | J221         | 0.6109       | 67.27          | 90.8                  | 29.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S433           | SU5          | 0.3498       | 104.9          | 33.3                  | 14.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S438           | J714         | 0.7282       | 40.22          | 181                   | 19.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S441           | J241         | 0.3507       | 26.75          | 131                   | 29.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S445           | J716         | 0.4719       | 25.02          | 189                   | 19.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S448           | J809         | 0.5673       | 68.93          | 82.3                  | 22           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S449           | J40          | 0.4962       | 64.18          | 77.3                  | 37.1         | 0              | 0.01        |           | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |



| Name  | Outlet   | Area<br>(ha) | Width<br>(m) | Flow<br>Length<br>(m) | Slope<br>(%) | Imperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|-------|----------|--------------|--------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S455  | J732     | 0.3237       | 27.27        | 119                   | 23.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S456  | J714     | 0.2872       | 62.68        | 45.8                  | 17.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S462  | J760     | 0.3762       | 63.47        | 59.3                  | 27.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S463  | J730     | 0.5391       | 49.27        | 109                   | 18.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S464  | J763     | 0.3507       | 87.08        | 40.3                  | 22.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S466  | J40      | 0.4133       | 74.41        | 55.5                  | 38.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S468  | J777     | 0.3549       | 39.91        | 88.9                  | 21           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S470  | J763     | 0.5254       | 47.47        | 111                   | 28.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S471  | J813     | 0.8801       | 141          | 62.4                  | 16.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S472  | J855     | 0.4505       | 108.6        | 41.5                  | 17.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S476  | J771     | 0.3138       | 62.12        | 50.5                  | 14           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S477  | J771     | 0.2607       | 55.01        | 47.4                  | 14.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S478  | J234     | 0.1397       | 31.3         | 44.6                  | 11.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S479  | J39      | 0.7285       | 65.62        | 111                   | 32.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S480  | J1898    | 0.0369       | 10.55        | 35                    | 5.02         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S481  | J244     | 0.0064       | 7.771        | 8.24                  | 9.37         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S482  | J782     | 0.6636       | 41.04        | 162                   | 18.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S483  | J799     | 0.4982       | 54.59        | 91.3                  | 29.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S484  | J230     | 0.1134       | 57.62        | 19.7                  | 16.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S485  | J805     | 0.838        | 68.05        | 123                   | 48.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S486  | SU1      | 0.9946       | 78.52        | 127                   | 9.8          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S491  | J222     | 0.0091       | 12.84        | 7.09                  | 10.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S492  | J822     | 0.2596       | 78.2         | 33.2                  | 27.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S493  | SU2      | 0.8823       | 80.4         | 110                   | 21.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S496  | J270     | 0.0496       | 13.73        | 36.1                  | 10.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$500 | J213     | 0.0245       | 22.79        | 10.7                  | 37.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$503 | J227     | 0.0984       | 68           | 14.5                  | 12.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S504  | J837     | 0.2779       | 54.21        | 51.3                  | 26.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$507 | J45      | 0.7657       | 126.1        | 60.7                  | 15.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S509  | J217     | 0.0013       | 3.469        | 3.75                  | 28.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S515  | J263     | 0.5923       | 89.1         | 66.5                  | 15.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S516  | J45      | 0.6201       | 102.5        | 60.5                  | 16.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S517  | J316     | 0.0527       | 33.76        | 15.6                  | 11.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S518  | J261     | 0.09         | 61.47        | 14.6                  | 7.78         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S522  | J859     | 0.2618       | 26.41        | 99.1                  | 14.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S523  | J861     | 0.4015       | 53.06        | 75.7                  | 19.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S524  | J232     | 0.0449       | 21.26        | 21.1                  | 2.03         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S525  | J89      | 0.7371       | 49.59        | 149                   | 41.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S526  | J91      | 0.549        | 44.07        | 125                   | 45.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S528  | SU1      | 0.5601       | 112.9        | 49.6                  | 8.45         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S529  | J228     | 0.0384       | 24.28        | 15.8                  | 9.43         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S533  | J82      | 0.0126       | 2.497        | 50.5                  | 54.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S538  | J859     | 0.3963       | 46.98        | 84.4                  | 8.02         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S539  | J202     | 0.4581       | 67           | 68.4                  | 14.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S541  | J855     | 0.2522       | 42.62        | 59.2                  | 11.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$542 | J268     | 0.0097       | 12.48        | 7.77                  | 25           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S545  | J212     | 0.0061       | 5.866        | 10.4                  | 9.03         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S546  | J268     | 0.0014       | 3.91         | 3.58                  | 26.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S547  | J837     | 0.6698       | 150.2        | 44.6                  | 17.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S549  | J1775    | 0.5584       | 69.63        | 80.2                  | 10.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$552 | J930     | 0.3727       | 69.41        | 53.7                  | 10.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$558 | J930     | 0.6998       | 80.64        | 86.8                  | 11.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$559 | J196     | 1.0786       | 76.45        | 141                   | 13.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| 562   | J200     | 0.0528       | 22.88        | 23.1                  | 27.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | ļ                        |
| 5564  | J73      | 0.0431       | 18.99        | 22.7                  | 14.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$565 | J81      | 0.0032       | 4.722        | 6.78                  | 13.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$566 | J887     | 0.8797       | 58.74        | 150                   | 20.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S568  | J28      | 0.0081       | 7.116        | 11.4                  | 16.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$572 | J1775    | 0.7874       | 88.76        | 88.7                  | 24.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$573 | culv12in | 0.0027       | 5.051        | 5.35                  | 14.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S575  | J76      | 0.0238       | 19.76        | 12                    | 10.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$576 | J1846    | 0.3818       | 87.76        | 43.5                  | 14.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$578 | J28      | 0.0001       | 2.899        | 0.35                  | 8.64         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S580  | J120     | 0.0092       | 12.04        | 7.64                  | 9.63         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
|       | J119     | 0.0018       | 3.547        | 5.08                  | 7.49         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |



| Name         | Outlet      | Area<br>(ha) | Width<br>(m)   | Flow<br>Length<br>(m) | Slope<br>(%) | Imperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|--------------|-------------|--------------|----------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S583         | J942        | 0.4065       | 76.65          | 53                    | 15.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S585         | J102        | 0.1376       | 45.22          | 30.4                  | 43.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S588         | J89         | 0.0305       | 30.3           | 10.1                  | 23.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S590         | J895        | 0.2261       | 28.93          | 78.1                  | 21.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S593         | J918        | 0.6927       | 93.42          | 74.1                  | 15.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S595         | J178        | 0.484        | 77.05          | 62.8                  | 13.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S596         | J1745       | 0.5997       | 93.74          | 64                    | 19.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S597         | J118        | 0.0231       | 17.3           | 13.4                  | 11.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S598         | J65         | 0.0148       | 17.06          | 8.67                  | 20.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S599         | J117        | 0.146        | 36.39          | 40.1                  | 19.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S600         | J65         | 0.0088       | 4.06           | 21.7                  | 11.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S602         | J911        | 0.4182       | 46.49          | 90                    | 24.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S603         | 188         | 0.0047       | 10.37          | 4.53                  | 14.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S604         | J942        | 0.3153       | 40.6           | 77.7                  | 17.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S609         | J178        | 0.0262       | 13.7           | 19.1                  | 13.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S610         | J905        | 0.3802       | 101.5          | 37.5                  | 20.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S612         | J86         | 0.0339       | 13.43          | 25.3                  | 18.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S613         | J103        | 0.0173       | 20.8           | 8.32                  | 27.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S614         | J56         | 0.3815       | 112.8          | 33.8                  | 24           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S618         | J198        | 0.3391       | 88.56          | 38.3                  | 22.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S621<br>S622 | J58<br>J962 | 0.0191       | 10.61<br>94.67 | 18<br>113             | 14.5<br>20   | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S622         | J83         | 0.0916       | 44.27          | 20.7                  | 18.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 |                             | 7                        |
| S626         | SU3         | 0.5615       | 63.29          | 88.7                  | 10.0         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S627         | J136        | 0.0021       | 6.878          | 3.05                  | 20.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S628         | J59         | 0.0021       | 8.644          | 5.09                  | 20.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S629         | J964        | 0.6377       | 98.41          | 64.8                  | 25.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S631         | J67         | 0.0152       | 14.84          | 10.2                  | 11.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S635         | J198        | 0.0018       | 2.958          | 6.09                  | 9.35         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S636         | J63         | 0.0017       | 4.413          | 3.85                  | 9.46         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S640         | J1001       | 0.6147       | 76.23          | 80.6                  | 26.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S642         | J174        | 0.0148       | 9.367          | 15.8                  | 11.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S647         | J196        | 0.1696       | 500            | 3.39                  | 12.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S648         | J84         | 0.0067       | 3.029          | 22.1                  | 20           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S651         | J1745       | 0.028        | 7.941          | 35.3                  | 11.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S652         | SU4         | 0.157        | 24.69          | 63.6                  | 17.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S653         | J957        | 0.7035       | 36.37          | 193                   | 19           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S655         | J957        | 0.3411       | 37.37          | 91.3                  | 24.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S656         | J170        | 0.0321       | 18.86          | 17                    | 15.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S661         | J77         | 0.004        | 3.37           | 11.9                  | 12.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S663         | J33         | 0.0226       | 17.3           | 13.1                  | 15.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S664         | J33         | 0.0161       | 13.96          | 11.5                  | 16.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S665         | J976        | 0.657        | 81.34          | 80.8                  | 26           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S666         | J57         | 0.9316       | 146.3          | 63.7                  | 11.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S672         | J1758       | 0.1722       | 39.68          | 43.4                  | 33.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S674         | J976        | 0.2872       | 42.34          | 67.8                  | 24.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S677         | J116        | 0.0018       | 7.015          | 2.57                  | 0.19         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S678         | J27         | 0.0283       | 13.56          | 20.9                  | 8.54         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S679         | J189        | 0.0734       | 46.02          | 15.9                  | 42.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S680         | J50         | 0.0113       | 7.65           | 14.8                  | 4.54         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S683         | SU3         | 0.4146       | 27.92          | 148                   | 19.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S684         | J1869       | 0.6046       | 134.4          | 45                    | 9.99         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S685         | J1042       | 0.3966       | 65.09          | 60.9                  | 23.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S686         | J1005       | 1.0542       | 100.5          | 105                   | 29           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S690         | J191        | 0.0064       | 10.42          | 6.15                  | 15.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S692         | J192        | 0.2896       | 73.59          | 39.4                  | 36.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S693         | J1042       | 0.4198       | 51.27          | 81.9                  | 17.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S694         | SU3         | 0.6854       | 94.83          | 72.3                  | 27.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S695         | J1033       | 0.625        | 86.82          | 72                    | 24.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S697         | J25         | 0.0145       | 12.25          | 11.8                  | 9.68         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S701         | J1055       | 0.2583       | 30.84          | 83.8                  | 24.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S702         | J94         | 0.9716       | 95.36          | 102                   | 27.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S705         | JG          | 0.0184       | 18.73          | 9.83                  | 10.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S706         | J52         | 0.0449       | 28.9           | 15.5                  | 7.46         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |



| Name         | Outlet       | Area<br>(ha) | Width<br>(m)   | Flow<br>Length<br>(m) | Slope<br>(%) | Imperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|--------------|--------------|--------------|----------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S710         | J3           | 0.0142       | 10.99          | 12.9                  | 7.4          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S711         | J1749        | 0.365        | 96.57          | 37.8                  | 14           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S712         | J4           | 0.0027       | 9.448          | 2.86                  | 1.49         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S714         | J1059        | 0.5391       | 73.45          | 73.4                  | 14.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S718         | J1057        | 0.5728       | 43.4           | 132                   | 29.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S721         | J1061        | 0.5046       | 61.06          | 82.6                  | 23           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S724         | J1078        | 0.7016       | 59.11          | 119                   | 19.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S728         | J1070        | 0.3344       | 32.33          | 103                   | 17.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S730         | J1099        | 0.3017       | 44.18          | 68.3                  | 20           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S731         | J1061        | 0.3975       | 63.97          | 62.1                  | 24.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S734<br>S743 | J1078<br>J36 | 0.3616       | 65.25<br>12.01 | 55.4<br>31.1          | 23.3<br>41.7 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S745         | J15          | 0.6761       | 12.01          | 53.3                  | 25.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S744         | J1793        | 0.2776       | 53.18          | 52.2                  | 22.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$751        | J1099        | 0.8765       | 56.92          | 154                   | 20.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S753         | J1135        | 0.2645       | 113.2          | 23.4                  | 21.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S756         | J1114        | 0.3365       | 78.47          | 42.9                  | 15.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S761         | J16          | 0.0036       | 8.232          | 4.37                  | 7.88         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S762         | J26          | 0.0142       | 15.95          | 8.9                   | 9.3          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S763         | J26          | 0.0084       | 12.74          | 6.59                  | 6.51         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S765         | J1118        | 0.4999       | 40.25          | 124                   | 26.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S766         | J16          | 0.0363       | 19.24          | 18.9                  | 7.31         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S767         | J1133        | 0.7282       | 62.97          | 116                   | 32.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S768         | J26          | 0.0635       | 28.54          | 22.3                  | 8.9          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S769         | J1763        | 0.6545       | 74.21          | 88.2                  | 19.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S770         | J1763        | 0.6548       | 168.4          | 38.9                  | 26.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S772         | J14          | 0.0044       | 8.795          | 5                     | 13.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S773         | J14          | 0.0009       | 2.266          | 3.97                  | 35.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S775         | J15          | 0.0644       | 31.63          | 20.4                  | 41.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S777         | J14          | 0.0066       | 11.25          | 5.87                  | 12.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S779         | J1130        | 1.1671       | 91.11          | 128                   | 14.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S780         | J14          | 0.0092       | 14.99          | 6.14                  | 12.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S782         | J14          | 0.0776       | 30.27          | 25.6                  | 15.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S784<br>S786 | J14<br>J1133 | 0.2703       | 10.08<br>28.68 | 8.04<br>94.2          | 12.8<br>35.9 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S787         | J1133        | 0.3493       | 81.24          | 43                    | 9.8          | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S788         | J1114        | 0.2862       | 29.58          | 96.7                  | 31.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S791         | J1170        | 0.6959       | 60.74          | 115                   | 36.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S793         | J1138        | 0.7899       | 68.84          | 115                   | 31.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S794         | J47          | 0.6086       | 29.91          | 203                   | 24.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S795         | J1170        | 0.38         | 30.78          | 123                   | 34.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S805         | J1801        | 0.7385       | 122.4          | 60.4                  | 24.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S806         | J129         | 0.0135       | 11.51          | 11.7                  | 17.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S807         | J1717        | 0.0028       | 2.428          | 11.5                  | 23.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S808         | J128         | 0.0069       | 10.94          | 6.31                  | 12.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S809         | J1147        | 0.5285       | 52.45          | 101                   | 26.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S811         | J1162        | 0.8227       | 72.18          | 114                   | 17.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S815         | J1164        | 0.5057       | 30.4           | 166                   | 38.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S820         | J113         | 0.2323       | 40.05          | 58                    | 23.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S821         | J1188        | 0.6246       | 109.6          | 57                    | 16.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S822         | J1185        | 0.713        | 65.62          | 109                   | 15.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S823<br>S825 | J54<br>J1701 | 0.6169       | 50.49<br>100.7 | 122<br>46.7           | 32.7<br>23.9 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| 5825<br>5827 | J1196        | 1.3472       | 120.9          | 46.7                  | 15           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S829         | J1196        | 0.8079       | 120.9          | 55.9                  | 19.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S831         | J1206        | 0.4412       | 61.3           | 72                    | 15.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | , 7                      |
| S832         | J101         | 0.5055       | 103.9          | 48.7                  | 42.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S833         | J1206        | 0.326        | 72.22          | 45.1                  | 24.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S834         | J1200        | 0.3963       | 37.8           | 105                   | 26.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S835         | J1233        | 0.2795       | 33.38          | 83.7                  | 29.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S836         | J1266        | 1.5426       | 110            | 140                   | 30.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S839         | J1204        | 0.6008       | 68.96          | 87.1                  | 14           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S849         | J20          | 0.0381       | 35.64          | 10.7                  | 31.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S850         | J19          | 0.2475       | 29.73          | 83.2                  | 47.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S851         | 199          | 0.1532       | 40.66          | 37.7                  | 24.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |



| Name             | Outlet         | Area<br>(ha) | Width<br>(m)   | Flow<br>Length<br>(m) | Slope<br>(%) | lmperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|------------------|----------------|--------------|----------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S853             | J1268          | 0.5964       | 58.09          | 103                   | 23.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S854             | culv3in        | 0.7226       | 59.13          | 122                   | 28.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S855             | J182           | 0.289        | 36.45          | 79.3                  | 22           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S856<br>S857     | J1256<br>J1334 | 0.5235       | 40.83<br>26.29 | 128<br>113            | 23.6<br>25.8 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S858             | J1220          | 0.2959       | 73.48          | 63.7                  | 25.8<br>19   | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S860             | J1797          | 0.2678       | 65.83          | 40.7                  | 19.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S861             | J1196          | 1.3977       | 97.97          | 143                   | 13.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S862             | J35            | 0.4924       | 104.1          | 47.3                  | 46.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S866             | J42            | 0.0007       | 2.753          | 2.54                  | 52.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S867<br>S869     | J43            | 0.1772       | 46.16          | 38.4                  | 37.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S869<br>S870     | J12<br>J78     | 0.3245       | 39.22<br>51.66 | 82.7<br>90.6          | 34.4<br>19.5 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S874             | J43            | 0.0042       | 5.536          | 7.59                  | 38.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S876             | J78            | 0.2606       | 34.28          | 76                    | 21.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S881             | J30            | 0.4273       | 46.48          | 91.9                  | 17.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S883             | J182           | 0.9009       | 199.9          | 45.1                  | 15           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S886             | culv3in        | 0.5703       | 101.7          | 56.1                  | 27.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S887             | J1760          | 0.6874       | 147.1          | 46.7                  | 14.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S891<br>S893     | J30<br>J1262   | 0.7853       | 64.63<br>24.18 | 122<br>182            | 19<br>20     | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S894             | J1890          | 0.0142       | 6.714          | 21.2                  | 36.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S895             | J1277          | 0.6456       | 62.32          | 104                   | 11           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S900             | J185           | 0.0045       | 11.29          | 3.99                  | 5.18         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S901             | J184           | 0.0764       | 40.03          | 19.1                  | 9.24         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S902             | J31            | 0.0691       | 35.7           | 19.4                  | 19           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S904             | J11            | 0.0028       | 3.113          | 9                     | 13.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S905             | J183           | 0.006        | 8.682          | 6.91                  | 4.43         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S906<br>S907     | J1839<br>J80   | 0.3109       | 62.63<br>12.59 | 49.6<br>7.86          | 22<br>18.3   | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S908             | J1283          | 0.361        | 69.92          | 51.6                  | 21.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S910             | J75            | 0.0025       | 4.052          | 6.17                  | 17.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S912             | J11            | 0.0012       | 2.56           | 4.69                  | 21.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S925             | J22            | 0.0109       | 9.661          | 11.3                  | 10.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S926             | J70            | 0.0112       | 7.446          | 15                    | 22.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S928             | J1847          | 0.2548       | 20.88          | 122                   | 26.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S930<br>S932     | J41<br>J1309   | 0.3284       | 53.18<br>39.5  | 61.7<br>72.3          | 16.7<br>14.5 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S933             | J1309          | 0.8593       | 87.88          | 97.8                  | 14.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S937             | J1328          | 0.3034       | 38.11          | 79.6                  | 32.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S940             | J1324          | 0.4154       | 37.07          | 112                   | 8.89         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S941             | J1339          | 0.1123       | 18.95          | 59.3                  | 16.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S942             | J1339          | 1.0631       | 111.6          | 95.3                  | 15.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S943             | J13            | 0.1653       | 33.39          | 49.5                  | 16.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S945<br>S947     | J66<br>J1847   | 0.0055       | 8.084<br>65.94 | 6.8<br>43.1           | 8.36<br>31.1 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S948             | J1387          | 0.6624       | 109.9          | 60.3                  | 20.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S949             | J1411          | 0.5226       | 155.4          | 33.6                  | 13.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S950             | J1368          | 1.2444       | 140.7          | 88.5                  | 41           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S952             | J1360          | 0.2945       | 25.03          | 118                   | 21.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S956             | J1394          | 0.391        | 56.58          | 69.1                  | 42.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S958             | J1387          | 0.2824       | 65.72          | 43<br>01 0            | 15.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S967<br>S971     | J1351<br>J1372 | 0.3587       | 43.87<br>61.34 | 81.8<br>83.4          | 11.3<br>15.6 | 0              | 0.01        | 0.1       | 0.05                     | 0.05<br>0.05           | 4                                 | 2                                 | 4                           | 7                        |
| \$974            | J1372          | 0.5265       | 42.81          | 123                   | 28.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S975             | J1823          | 0.5259       | 51.44          | 102                   | 19.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S979             | J1436          | 0.3556       | 35.02          | 102                   | 43.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S981             | J1394          | 0.7242       | 170.5          | 42.5                  | 31.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S988             | J1419          | 0.622        | 76.12          | 81.7                  | 24.4         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S994             | J1398          | 0.4495       | 72.24          | 62.2                  | 12.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S1000            | J1455          | 0.2638       | 49.34          | 53.5                  | 26.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S1004<br>S1019   | J1411<br>J1467 | 0.5197       | 64.75<br>46.49 | 80.3<br>150           | 10.1<br>29.6 | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| \$1019<br>\$1021 | J1467          | 0.8952       | 49.03          | 80.9                  | 13.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
|                  | J1494          | 0.5199       | 81.1           | 64.1                  | 21.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |



| Name               | Outlet | Area<br>(ha) | Width<br>(m) | Flow<br>Length<br>(m) | Slope<br>(%) | lmperv.<br>(%) | N<br>Imperv | N<br>Perv | Dstore<br>Imperv<br>(mm) | Dstore<br>Perv<br>(mm) | Max.<br>Infil.<br>Rate<br>(mm/hr) | Min.<br>Infil.<br>Rate<br>(mm/hr) | Decay<br>Constant<br>(1/hr) | Drying<br>Time<br>(days) |
|--------------------|--------|--------------|--------------|-----------------------|--------------|----------------|-------------|-----------|--------------------------|------------------------|-----------------------------------|-----------------------------------|-----------------------------|--------------------------|
| S1039              | J1525  | 0.5438       | 25.25        | 215                   | 20.5         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S1170              | J57    | 0.0614       | 33.38        | 18.4                  | 5.41         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S698_1             | J7     | 0.4986       | 110.7        | 45.1                  | 13.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S698_2             | J55    | 0.0773       | 110.7        | 6.99                  | 13.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S732_1             | J36    | 0.0192       | 33.03        | 5.81                  | 12.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
| S732_2             | J46    | 0.3848       | 33.03        | 117                   | 12.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 7                        |
|                    | 18     | 0.0713       | 70.03        | 10.2                  | 9.77         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
|                    | J62    | 0.0868       | 70.03        | 12.4                  | 9.77         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S911 1             | J1334  | 0.1533       | 105.8        | 14.5                  | 15.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S911_2             | J68    | 0.8225       | 105.8        | 77.8                  | 15.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S519_1             | J1720  | 0.0857       | 47.52        | 18                    | 42.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S519 2             | J805   | 0.1658       | 47.52        | 34.9                  | 42.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S452_2             | J17    | 0.3311       | 63.56        | 52.1                  | 20           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S452_2             | J18    | 0.3553       | 63.56        | 55.9                  | 20           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S452_5             | J271   | 0.1177       | 63.56        | 18.5                  | 20           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S443 1             | J248   | 0.2604       | 78.26        | 33.3                  | 28.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S443_3             | J61    | 0.3339       | 78.26        | 42.7                  | 28.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S443_4             | J69    | 0.2528       | 78.20        | 32.3                  | 28.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| 5739 1             | 190    | 0.2528       | 123.5        | 36.5                  | 18           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| \$739_1<br>\$739_2 | SU6    | 0.45         | 123.5        | 16.8                  | 18           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
|                    |        |              |              |                       |              |                |             |           |                          |                        |                                   |                                   |                             |                          |
| <u>\$374_1</u>     | J34    | 0.1871       | 71.73        | 26.1                  | 21.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S374_2             | J53    | 0.2242       | 71.73        | 31.3                  | 21.1         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S868_1             | J99    | 0.0346       | 27.03        | 12.8                  | 25.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S868_2             | J44    | 0.0908       | 27.03        | 33.6                  | 25.9         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 1                        |
| \$758_1            | J10    | 0.0658       | 25.28        | 26                    | 12.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S360_1             | J107   | 0.4801       | 85.76        | 56                    | 16.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S360_2             | J34    | 0.2817       | 85.76        | 32.8                  | 16.2         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S348_1             | J109   | 0.2269       | 54.29        | 41.8                  | 14           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | 1                        |
| S348_2             | J297   | 0.1133       | 54.29        | 20.9                  | 14           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S792_1             | J54    | 0.0604       | 71.17        | 8.49                  | 31           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S792_3             | J137   | 0.1148       | 71.17        | 16.1                  | 31           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S286_1             | J110   | 0.4958       | 62.46        | 79.4                  | 12.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S286_2             | J274   | 0.0691       | 62.46        | 11.1                  | 12.7         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S307_1             | J106   | 0.1369       | 51.35        | 26.7                  | 12.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S307_2             | J274   | 0.1834       | 51.35        | 35.7                  | 12.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S796_1             | J125   | 0.2235       | 77.6         | 28.8                  | 25.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S796_3             | J143   | 0.1176       | 77.6         | 15.2                  | 25.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S796_4             | J135   | 0.1014       | 77.6         | 13.1                  | 25.8         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S758_3             | J26    | 0.0763       | 25.28        | 30.2                  | 12.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S758_4             | J16    | 0.1863       | 25.28        | 73.7                  | 12.3         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S792_2             | J138   | 0.0482       | 71.17        | 6.77                  | 31           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S792_4             | J144   | 0.1018       | 71.17        | 14.3                  | 31           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           |                          |
| S792_6             | J111   | 0.1622       | 71.17        | 22.8                  | 31           | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_1             | J200   | 0.0529       | 61.7         | 8.57                  | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_5             | J142   | 0.0125       | 61.7         | 2.03                  | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_4             | J142   | 0.1232       | 61.7         | 20                    | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_7             | J146   | 0.1518       | 61.7         | 24.6                  | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_6             | J147   | 0.1703       | 61.7         | 27.6                  | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_8             | J145   | 0.1492       | 61.7         | 24.2                  | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |
| S537_2             | J168   | 0.1035       | 61.7         | 16.8                  | 32.6         | 0              | 0.01        | 0.1       | 0.05                     | 0.05                   | 4                                 | 2                                 | 4                           | -                        |

| S537_2 | J168 | 0.1035 | 61.7  | 16.8 | 32.6 | 0 | 0.01 | 0.1 | 0.05 | 0.05 | 4 | 2 | 4 | 7 |
|--------|------|--------|-------|------|------|---|------|-----|------|------|---|---|---|---|
| S537_9 | J150 | 0.0406 | 61.7  | 6.58 | 32.6 | 0 | 0.01 | 0.1 | 0.05 | 0.05 | 4 | 2 | 4 | 7 |
| S667_2 | J27  | 0.6974 | 96.72 | 72.1 | 17.6 | 0 | 0.01 | 0.1 | 0.05 | 0.05 | 4 | 2 | 4 | 7 |
| S667_3 | J38  | 0.1045 | 96.72 | 10.8 | 17.6 | 0 | 0.01 | 0.1 | 0.05 | 0.05 | 4 | 2 | 4 | 7 |
| S667_4 | J27  | 0.0365 | 96.72 | 3.77 | 17.6 | 0 | 0.01 | 0.1 | 0.05 | 0.05 | 4 | 2 | 4 | 7 |

### Table 2: Junctions PCSWMM Model Parameters

|      | X-         |              | Invert Elev. |
|------|------------|--------------|--------------|
| Name | Coordinate | Y-Coordinate | (m)          |
| J3   | 455600.43  | 6968878.3    | 19.50        |
| J4   | 455612.38  | 6968882.8    | 18.30        |
| J5   | 455633.07  | 6968889.1    | 17.70        |
| J6   | 455655.16  | 6968893.2    | 16.29        |
| J7   | 455697.96  | 6968870.7    | 12.00        |
| J8   | 455718.85  | 6968884.2    | 9.90         |
| J35  | 455690.04  | 6968509.5    | 36.09        |



| Name     | X-<br>Coordinate | Y-Coordinate | Invert Elev.<br>(m) |
|----------|------------------|--------------|---------------------|
| J42      | 455709.74        | 6968506.5    | 35.60               |
| J43      | 455712.64        | 6968496.5    | 35.00               |
| J44      | 455725.52        | 6968499      | 34.95               |
| J67      | 455503.27        | 6969019.8    | 39.94               |
| J115     | 454921.19        | 6968953.3    | 63.40               |
| J116     | 454919.08        | 6968962.4    | 64.00               |
| J117     | 454956.32        | 6969069.9    | 60.39               |
| J118     | 454968.27        | 6969076.2    | 58.70               |
| J119     | 455012.53        | 6969102.2    | 55.51               |
| J120     | 455018.86        | 6969110.7    | 55.11               |
| J158     | 454362.51        | 6969747.2    | 65.00               |
| J159     | 454350.33        | 6969731.6    | 65.97               |
| J182     | 455083.91        | 6968404.7    | 76.00               |
| J183     | 455076.2         | 6968405.9    | 75.59               |
| J184     | 455066.25        | 6968412.4    | 75.01               |
| J185     | 455058.87        | 6968416.2    | 74.76               |
| culv3out | 455709.39        | 6968471.4    | 39.84               |
| culv12in | 455686.89        | 6969120.1    | 12.35               |
| J9       | 455570.34        | 6968388.3    | 69.80               |
| J19      | 455691.72        | 6968521      | 35.97               |
| J20      | 455710.21        | 6968519.4    | 35.60               |
| J28      | 455691.46        | 6969116.7    | 11.80               |
| J29      | 454729.05        | 6969324.5    | 69.90               |
| J1       | 455418.64        | 6968373.4    | 90.07               |
| J12      | 455592.87        | 6968418.5    | 66.99               |
| J22      | 455368.55        | 6968342.3    | 85.70               |
| J30      | 455523.73        | 6968360.5    | 73.16               |
| J31      | 455596.03        | 6968401.9    | 65.39               |
| J13      | 455330.59        | 6968223.5    | 75.24               |
| J41      | 455287.86        | 6968309.7    | 79.01               |
| J66      | 455380.21        | 6968320.4    | 84.89               |
| J70      | 455340.38        | 6968347.7    | 81.98               |
| J75      | 455217.98        | 6968390.4    | 79.86               |
| J78      | 455240.69        | 6968385.8    | 78.38               |
| J80      | 455690.81        | 6968400.4    | 58.92               |
| culv3in  | 455694           | 6968464.2    | 42.01               |
| J93      | 455711.29        | 6968506.3    | 35.45               |
| 199      | 455783.21        | 6968503.5    | 24.54               |
| J101     | 455703.16        | 6968572.2    | 37.65               |
| J111     | 455729.38        | 6968724.1    | 18.47               |
| J113     | 455766.4         | 6968633.4    | 20.56               |
| J125     | 455760.97        | 6968683.9    | 15.01               |
| J126     | 455744.45        | 6968717.7    | 17.02               |
| J128     | 455772.78        | 6968681.5    | 14.08               |
| J129     | 455793.65        | 6968686.1    | 10.07               |
| J16      | 455718.34        | 6968765.2    | 16.99               |
| J36      | 455637.99        | 6968810.6    | 19.95               |
| J15      | 455650.77        | 6968751.9    | 20.72               |
| J26      | 455715.87        | 6968777.1    | 16.05               |
| J46      | 455705.83        | 6968818.1    | 14.97               |
| J48      | 455705.73        | 6968829.1    | 14.92               |
| J25      | 455617.65        | 6968919.7    | 18.57               |
| J27      | 455630.97        | 6968964      | 15.00               |
| J33      | 455635.37        | 6968987.6    | 14.60               |
| J50      | 455656.18        | 6968961.9    | 15.88               |
| J56      | 455656.83        | 6969037      | 10.26               |
| J58      | 455690.14        | 6969048.3    | 6.57                |
| J59      | 455714.33        | 6969038.2    | 4.12                |
| J63      | 455706.44        | 6969029.2    | 6.48                |
| J65      | 455682.72        | 6969064.6    | 9.81                |
| J72      | 455694.66        | 6969058.9    | 5.46                |
| J73      | 455707.29        | 6969107.2    | 9.99                |
| J76      | 455714.23        | 6969094.4    | 8.85                |
| J81      | 455706.85        | 6969119.6    | 10.93               |
| J82      | 455661.86        | 6969103      | 12.08               |
| J77      | 455717.73        | 6968988.4    | 11.33               |
| J87      | 455726.44        | 6969002.5    | 7.86                |



| 188         455657.16         6969071         1           189         455658.96         6969078.6         1           191         455664.45         6969088.9         1           184         455604.44         6969010.1         2           1102         455611.62         6969055.5         1           1103         455619.65         6969032.9         2           1142         455580.33         6969032.9         2           1174         455490.94         6968981.7         2           1174         455495.53         6969032.3         4           1178         455495.53         6969032.3         4           1189         455551.18         6968932.1         2           1191         455561.18         6968932.1         2           1192         455587.94         6968847.7         2           1194         455596.52         6968848.7         2           1192         455494.71         6969077.3         4           1200         455494.71         6969192.3         5           1212         45527.67         6969192.3         5           1221         455248.09         6969192.3         5  | ev.            | Invert Elev |              | Х-        |      |
|---|----------------|-------------|--------------|-----------|------|
| 188         455657.16         6969071         1           189         455658.96         6969078.6         1           191         455664.45         6969078.6         1           184         455604.44         6969010.1         2           1102         455611.62         6969055.5         1           1103         455619.65         6969032.9         2           1142         455582.33         6969032.4         2           1176         455590.94         6968981.7         2           1177         455495.53         6969032.3         4           1178         455495.52         6968932.1         2           1191         455551.27         6968932.1         2           1192         455596.52         6968884.7         2           1194         455596.52         6968849.9         2           1194         455597.47         6969016.4         4           1200         455494.71         6969077.3         4           1202         45548.45         6969182.3         5           1213         45543.03         6969192.3         5           1221         4552370.78         6969229.3         4  |                |             | Y-Coordinate |           | Name |
| 189         455658.96         6969078.6         1           191         455664.45         6969088.9         1           184         455604.44         6969010.1         22           1102         455611.62         6969055.5         1           1103         455592.33         6969032.9         2           1142         455584.52         6969033.4         2           1176         455590.94         6968981.7         2           1174         455446.47         6969002         44           1178         455591.38         6969032.3         44           1189         455573.27         6968932.1         22           1191         455596.52         6968884.7         2           1192         455548.794         6968907.3         44           1200         455494.71         6969016.4         44           1200         455494.71         6969017.3         44           1212         455458.45         6969148.3         55           1213         455443.03         696912.3         55           1221         455458.45         6969148.3         55           1222         455370.78         696922.3         44 <td>10.70</td> <td>1</td> <td>6969056.2</td> <td>455657.09</td> <td>J86</td>       | 10.70          | 1           | 6969056.2    | 455657.09 | J86  |
| 191         455664.45         6969088.9         1           184         455604.44         6969010.1         22           1102         455611.62         6969055.5         1           1103         455591.33         6969032.9         22           1142         455584.52         6969033.4         22           1142         455581.23         6969032.3         44           1170         455590.94         6968981.7         22           1174         455446.47         6969002         44           1178         455591.38         6966932.3         44           1189         455591.38         6968932.1         22           1191         455596.52         6968884.7         22           1192         455596.52         6968884.7         22           1193         45549.09         6969007.3         44           1200         455494.71         6969016.4         44           1200         45549.07         6969188.3         55           1213         45548.45         6969192.3         55           1221         45527.07         6969202.3         44           1222         455236.3         6969190.1         44<   | 11.30          | 1           | 6969071      | 455657.16 | J88  |
| 184         455604.44         6969010.1         2           1102         455611.62         6969055.5         1           1103         455619.65         6969032.9         2           1142         455581.22         6969033.4         2           1168         455507.91         6969046.3         4           1170         455590.94         6968981.7         2           1174         455446.47         6969002         4           1178         455573.27         6968932.1         2           1191         455561.18         6968932.1         2           1192         45557.94         6968893.9         2           1194         455596.52         6968884.7         2           1192         455541.8         6969148.3         5           1200         455494.71         696907.3         4           1202         45548.45         6969148.3         5           1213         455443.03         6969192.3         5           1221         455372.17         6969202.3         4           1222         455276.8         6969190.1         4           1223         455249.06         6969202.3         4   | 11.50          | 1           | 6969078.6    | 455658.96 | J89  |
| 1102         455611.62         6969055.5         1           1103         455619.65         6969056.6         1           1136         455592.33         6969032.9         2           1142         455584.52         6969033.4         2           1168         455507.91         6969046.3         44           1170         455590.94         6968981.7         2           1174         455446.47         6969002         44           1179         455573.27         6968932.1         2           1191         455561.18         6968932.6         2           1192         455587.94         6968893.9         2           1194         455596.52         696884.7         2           1192         45544.09         6969005.8         44           1200         45544.09         6969016.4         4           1202         45548.45         6969148.3         5           1212         45548.45         6969148.3         5           1221         455370.78         6969242.1         5           1222         455370.78         6969192.3         4           1223         455288.32         6969183.4         4 </td <td>11.80</td> <td>1</td> <td>6969088.9</td> <td>455664.45</td> <td>J91</td>           | 11.80          | 1           | 6969088.9    | 455664.45 | J91  |
| 1103         455619.65         6969056.6         1           1136         455592.33         6969032.9         22           1142         455584.52         6969033.4         22           1168         455507.91         6969046.3         44           1170         455590.94         6968981.7         22           1174         455446.47         6969002         44           1178         455593.27         6968932.1         22           1191         455561.18         696893.9         22           1192         455587.94         6968893.9         22           1194         455596.52         696884.7         22           1193         455547.47         6969016.4         44           1200         45549.07         6969077.3         44           1202         45548.45         6969192.3         55           1212         455570.78         6969229.3         44           1222         45528.32         6969190.1         44           1223         455248.32         6969190.3         55           1224         45528.32         6969193         55           1224         455248.55         696920.2         55 </td <td>22.21</td> <td>2</td> <td>6969010.1</td> <td>455604.44</td> <td>J84</td> | 22.21          | 2           | 6969010.1    | 455604.44 | J84  |
| 1136         455592.33         6969032.9         2           1142         455584.52         6969033.4         2           1168         455507.91         6969046.3         4           1170         455590.94         6968981.7         2           1174         455446.47         6969002         4           1178         455495.53         6969032.3         4           1189         455553.27         6968932.1         2           1191         455561.18         696892.6         2           1192         455587.94         696893.9         2           1194         455596.52         6968884.7         2           1192         455370.78         6969069.8         4           1200         455484.09         6969069.8         4           1212         455370.78         6969192.3         5           1221         455268.1         6969192.3         4           1222         455370.78         6969120.3         4           1223         455288.32         6969188.1         4           1230         455249.06         6969120.2         5           1241         45527.69         6969151.2         5 <td>19.71</td> <td>1</td> <td>6969055.5</td> <td>455611.62</td> <td>J102</td>                 | 19.71          | 1           | 6969055.5    | 455611.62 | J102 |
| 1142         455584.52         6969033.4         22           1168         455507.91         6969046.3         44           1170         455590.94         6968981.7         2           1174         455446.47         6969002         44           1178         455553.27         6968932.1         22           1191         455561.18         6968893.9         22           1192         455587.94         6968893.9         22           1194         455596.52         6968884.7         22           1193         455374.67         6969016.4         44           1200         455484.09         6969069.8         44           1212         455483.03         6969148.3         55           1221         455372.17         696922.3         44           1222         455288.32         6969188.1         44           1223         455288.32         6969190.1         44           1224         455288.32         6969188.1         44           1230         455249.06         6969202.3         44           1232         455288.32         6969183.1         55           1241         45502.5         55         55 <td>18.44</td> <td>1</td> <td>6969056.6</td> <td>455619.65</td> <td>J103</td>      | 18.44          | 1           | 6969056.6    | 455619.65 | J103 |
| 1168         455507.91         6969046.3         4           1170         455590.94         6968981.7         2           1174         455446.47         6969002         4           1178         455495.53         6969032.3         4           1189         455553.27         6968932.1         22           1191         455561.18         696893.9         2           1192         455587.94         6968893.9         2           1194         455596.52         6968884.7         2           1198         455374.67         6969016.4         4           1200         455484.09         6969069.8         4           1212         45548.43         6969148.3         5           1221         455372.17         696922.3         4           1222         455370.78         6969190.1         4           1223         455288.12         6969188.1         4           1224         455285.3         6969193         5           1224         455286.5         6969202.3         4           1230         455249.06         6969202.3         4           1232         45527.69         696920.2         5   | 26.49          | 2           | 6969032.9    | 455592.33 | J136 |
| 1170         455590.94         6968981.7         2           1174         455446.47         6969002         4           1178         455495.53         6969032.3         4           1189         455553.27         6968932.1         2           1191         455561.18         696893.9         2           1192         455587.94         6968893.9         2           1194         455596.52         6968884.7         2           1192         455374.67         6969016.4         4           1200         455494.71         6969077.3         4           1202         455484.09         6969069.8         4           1212         455372.17         6969229.3         4           1221         455288.1         6969190.1         4           1222         455286.1         6969190.1         4           1223         455286.3         6969193         5           1224         455286.53         6969193         5           1224         455286.53         6969193         5           1241         45527.69         696926.2         5           1244         455004.78         6969172.5         5 <t< td=""><td>27.83</td><td></td><td></td><td></td><td></td></t<>                                     | 27.83          |             |              |           |      |
| 1174         455446.47         6969002         4           1178         455495.53         6969032.3         4           1189         455553.27         6968932.1         2           1191         455561.18         696893.9         2           1192         455596.52         6968884.7         2           1194         455596.52         6968884.7         2           1194         455374.67         6969016.4         4           1200         455494.71         6969077.3         4           1202         45548.409         6969069.8         4           1212         45543.03         6969148.3         5           1221         455372.17         696922.3         4           1222         455288.32         6969188.1         4           1230         455249.06         696920.3         4           1232         455236.53         6969193         5           1241         45527.69         6969260.2         5           1244         455180.55         6969183.4         5           1264         454927.8         6969169.3         5           1264         454927.8         6969169.3         5  | 40.76          |             |              |           |      |
| 1178         455495.53         6969032.3         44           J189         455553.27         6968932.1         2           J191         455561.18         696892.6         2           J192         455596.52         6968884.7         2           J194         455596.52         6968884.7         2           J194         455596.52         6969016.4         4           J200         455494.71         6969077.3         4           J202         455484.09         6969069.8         44           J212         45543.03         6969143.3         5           J213         45543.03         6969192.3         4           J222         455370.78         6969192.3         4           J223         455288.32         6969193.1         4           J224         455286.53         6969193.1         4           J232         455249.06         696920.2         5           J241         45527.69         6969172.5         5           J244         455004.78         6969183.4         5           J263         454991.64         6969172.5         5           J264         454927.8         6969169.3         5 </td <td>23.70</td> <td></td> <td></td> <td></td> <td></td>                                 | 23.70          |             |              |           |      |
| 1189         455553.27         6968932.1         22           1191         455551.18         6968892.6         22           1192         455587.94         6968893.9         22           1194         455596.52         6968884.7         22           1198         455374.67         6969016.4         44           1200         455494.71         6969077.3         44           1202         455484.09         6969148.3         55           1213         455472.17         6969123.3         55           1221         455370.78         6969123.3         44           1222         455370.78         6969123.3         44           1223         455288.32         6969188.1         44           1230         455249.06         6969203.3         44           1230         455247.69         6969183.4         55           1241         455002.22         6969203.6         55           1241         455004.78         6969172.5         55           1263         454991.64         6969172.5         55           1264         454927.8         6969165.1         55           1264         454927.8         6969175.9  | 46.99          |             |              |           |      |
| J191         455561.18         6968922.6         22           J192         455587.94         696883.9         22           J194         455596.52         6968884.7         22           J198         455374.67         6969016.4         44           J200         455494.71         6969077.3         44           J202         455484.09         6969069.8         44           J212         455478.45         6969148.3         55           J213         455443.03         6969123         55           J221         455370.78         6969229.3         44           J220         455248.12         6969188.1         44           J221         455248.2         6969188.1         44           J222         455236.53         6969192.3         44           J230         455249.06         696920.2         55           J241         455227.69         6969260.2         55           J244         455180.55         6969172.5         55           J263         454991.64         6969172.5         55           J264         454927.8         6969165.1         55           J267         454857.69         6969210.8 <t< td=""><td>41.42</td><td></td><td></td><td></td><td></td></t<>                      | 41.42          |             |              |           |      |
| 1192         455587.94         6968893.9         22           1194         455596.52         6968884.7         22           1198         455374.67         6969016.4         44           1200         455494.71         6969077.3         44           1202         455484.09         6969069.8         44           1212         455458.45         6969148.3         55           1213         455443.03         696922.3         45           1221         455370.78         696920.3         44           1220         455288.32         6969188.1         44           1220         455249.06         696920.2         55           1241         455227.69         6969260.2         55           1241         455092.22         6969183.4         55           1241         455092.22         6969210.2         55           1244         455092.22         6969210.2         55           1261         454991.64         696917.5         55           1264         454927.8         6969169.3         55           1267         454895.53         6969157.4         55           1268         454910.4         6969157.4 <t< td=""><td>24.59</td><td></td><td></td><td></td><td></td></t<>                      | 24.59          |             |              |           |      |
| 1194         455596.52         6968884.7         22           1198         455374.67         6969016.4         44           1200         455494.71         6969077.3         44           1202         455484.09         6969069.8         44           1212         455458.45         6969148.3         55           1213         455470.78         6969242.1         55           1221         455370.78         6969190.1         44           1228         455288.32         6969188.1         44           1230         455249.06         6969202.3         44           1230         455227.69         6969260.2         55           1241         455027.69         6969260.2         55           1244         455180.55         6969183.4         55           1244         455004.78         6969169.3         55           1261         455004.78         6969169.3         55           1263         454991.64         6969172.5         55           1264         454927.8         6969169.3         55           1264         454927.8         6969157.4         55           1267         454857.69         6969210.8  | 23.92          |             |              |           |      |
| 1198         455374.67         6969016.4         44           1200         455494.71         6969077.3         44           1202         455484.09         6969069.8         44           1212         455458.45         6969148.3         55           1213         455431.03         6969122.3         55           1221         455372.17         6969242.1         55           1222         455370.78         6969190.1         44           1228         455288.32         6969188.1         44           1230         455249.06         6969202.3         44           1230         455236.53         6969193         55           1241         455207.69         6969260.2         55           1244         455180.55         6969183.4         55           1243         455092.22         6969183.4         55           1261         455094.72         55         55           1263         454927.8         6969169.3         55           1264         454927.8         6969157.4         55           1264         454927.8         6969157.4         55           1267         454857.69         6969219.5         66 </td <td>20.98</td> <td></td> <td></td> <td></td> <td></td>                       | 20.98          |             |              |           |      |
| J200         455494.71         6969077.3         44           J202         455484.09         6969069.8         44           J212         455458.45         6969148.3         55           J213         455443.03         6969192.3         55           J221         455370.78         6969229.3         44           J227         455268.1         6969190.1         44           J228         455249.06         6969202.3         44           J230         455249.06         6969202.3         44           J230         455249.06         6969202.3         44           J230         455249.06         6969202.3         44           J231         455227.69         6969260.2         55           J241         455092.22         6969230.6         55           J261         455004.78         6969183.4         55           J263         45491.64         6969172.5         55           J264         454927.8         6969165.1         55           J267         454857.69         6969210.8         66           J270         45480.03         6969517.9         68           J270         454601.02         6969547.6  | 20.72          |             |              |           |      |
| J202         455484.09         6969069.8         44           J212         455458.45         6969148.3         55           J213         455472.17         6969242.1         55           J221         455370.78         6969192.3         44           J222         455370.78         6969229.3         44           J227         455268.1         6969190.1         44           J228         455288.32         6969188.1         44           J230         455249.06         6969202.3         44           J232         455236.53         6969193         55           J241         455180.55         6969260.2         55           J244         455092.22         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969165.1         55           J264         454927.8         6969157.4         55           J264         454927.8         6969157.4         55           J267         454857.69         6969210.8         66           J270         45480.03         6969517.4         88           J276         454601.02         6969547.6 <td< td=""><td>42.40</td><td></td><td></td><td></td><td></td></td<>                     | 42.40          |             |              |           |      |
| J212         455458.45         6969148.3         55           J213         455443.03         6969192.3         55           J221         455372.17         6969242.1         55           J222         455370.78         6969190.1         44           J227         455268.1         6969190.1         44           J228         455288.32         6969188.1         44           J230         455249.06         6969202.3         44           J232         455236.53         6969193         55           J241         455227.69         6969260.2         55           J244         455004.78         6969183.4         55           J261         455004.78         6969183.4         55           J263         45491.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         696917.4         55           J270         454857.69         6969210.5         66           J271         454639.96         6969575.9         88           J276         454639.96         6969557.9 <td< td=""><td>44.20<br/>43.34</td><td></td><td></td><td></td><td></td></td<>           | 44.20<br>43.34 |             |              |           |      |
| J213         455443.03         6969192.3         5           J221         455372.17         6969242.1         55           J222         455370.78         6969229.3         4           J227         455268.1         6969190.1         4           J228         455248.32         6969188.1         44           J230         455249.06         6969202.3         44           J232         455236.53         6969193         55           J241         455180.55         6969260.2         55           J244         455180.55         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969165.1         55           J263         454991.64         6969172.5         55           J264         454927.8         6969165.1         55           J267         454857.69         6969219.5         66           J270         454857.69         6969219.5         66           J271         454601.02         6969575.9         88           J276         454639.96         6969575.9         88           J276         454668.24         6969567.7  | 53.92          |             |              |           |      |
| J221         455372.17         6969242.1         5           J222         455370.78         6969229.3         44           J227         455268.1         6969190.1         44           J228         455288.32         6969188.1         44           J230         455249.06         6969202.3         44           J230         455236.53         6969193         55           J241         455207.69         6969260.2         55           J244         455180.55         6969230.6         55           J244         455092.22         6969230.6         55           J263         454991.64         6969172.5         55           J264         454927.8         6969165.1         55           J264         454927.8         6969157.4         55           J264         454927.8         6969157.4         55           J267         454857.69         6969219.5         66           J270         45480.03         6969517.4         68           J271         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J275         454663.03         6969567.7  | 53.92<br>54.88 |             |              |           |      |
| J222         455370.78         6969229.3         44           J227         455268.1         6969190.1         44           J228         455288.32         6969188.1         44           J230         455249.06         6969202.3         44           J230         455236.53         6969193         55           J241         455227.69         696920.2         55           J244         455180.55         6969230.6         55           J244         455092.22         6969230.6         55           J261         455092.22         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969165.1         55           J264         454991.64         6969157.4         55           J264         454910.4         6969157.4         55           J267         454857.69         6969157.5         56           J270         454857.69         6969517.5         56           J271         454629.37         6969547.6         88           J274         454629.37         6969547.5         88           J275         454678.03         6969567.7 <t< td=""><td>51.18</td><td></td><td></td><td></td><td></td></t<>                      | 51.18          |             |              |           |      |
| J227         455268.1         6969190.1         44           J228         455288.32         6969188.1         44           J230         455249.06         6969202.3         44           J232         455236.53         6969193         55           J241         455227.69         6969260.2         55           J244         455180.55         6969251.2         55           J248         455092.22         6969183.4         55           J261         455004.78         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J270         454840.03         696917.4         55           J271         454840.03         6969517.4         68           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J278         454678.03         6969567.4         88           J285         454690.36         6969545.1         88           J280         454701.53         6969545.1         <   | 49.82          |             |              |           |      |
| J228         455288.32         6969188.1         44           J230         455249.06         6969202.3         44           J232         455236.53         6969193         55           J241         455227.69         6969260.2         55           J244         455180.55         6969251.2         55           J248         455092.22         6969230.6         55           J261         455004.78         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         696917.4         55           J270         454857.69         6969517.8         66           J271         454629.37         6969587.9         88           J274         454629.37         6969567.4         88           J278         454678.03         6969567.4         88           J285         454690.36         6969567.4 <t< td=""><td>48.60</td><td></td><td></td><td></td><td></td></t<>                      | 48.60          |             |              |           |      |
| J230         455249.06         6969202.3         44           J232         455236.53         6969193         55           J241         455227.69         6969260.2         55           J244         455180.55         6969251.2         55           J248         455092.22         6969230.6         55           J261         455004.78         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         6969157.4         55           J270         454857.69         6969219.5         66           J271         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J276         454639.96         6969575.9         88           J278         454678.03         6969567.4         88           J283         454690.36         6969569.7         88           J283         454690.36         6969545.1         88           J290         454705.21         6969545.1  | 47.70          |             |              |           |      |
| J232         455236.53         6969193         5           J241         455227.69         6969260.2         5           J244         455180.55         6969251.2         5           J248         455092.22         6969230.6         5           J261         455004.78         6969183.4         5           J263         454991.64         6969172.5         5           J264         454927.8         6969169.3         5           J267         454895.53         6969165.1         5           J268         454910.4         6969172.5         5           J270         454857.69         6969210.8         6           J271         454601.02         6969547.6         8           J274         454629.37         6969587.9         8           J276         454639.96         6969575.9         8           J278         454678.03         6969569.7         8           J283         454682.63         6969569.7         8           J283         454682.43         6969545.1         8           J290         454705.21         6969545.1         8           J290         454705.21         6969545.1         8 </td <td>49.50</td> <td></td> <td></td> <td></td> <td></td>                                 | 49.50          |             |              |           |      |
| J241         455227.69         6969260.2         5           J244         455180.55         6969251.2         5           J248         455092.22         6969230.6         5           J261         455004.78         6969183.4         5           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         6969172.5         56           J270         454857.69         6969219.5         66           J271         45480.03         6969210.8         66           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J274         454639.96         6969575.9         88           J278         454678.03         6969569.7         88           J283         454678.03         6969569.7         88           J290         454705.21         6969545.1         88           J291         454682.4         6969472.6         88           J292         454705.21         6969545.1  | 50.00          |             |              |           |      |
| J248         455092.22         6969230.6         55           J261         455004.78         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         6969157.4         55           J270         454857.69         6969219.5         66           J271         45480.03         6969547.6         88           J274         454629.37         6969587.9         88           J278         454678.03         6969569.7         88           J283         454678.03         6969569.7         88           J283         454690.36         6969569.7         88           J290         454701.53         6969545.1         88           J291         454678.03         6969545.1         88           J292         454705.21         6969545.1         88           J292         454705.21         6969545.1         88           J306         454742.19         6969332.3         77           J316         454659.01         6969546.2   | 50.05          |             |              |           |      |
| J261         455004.78         6969183.4         55           J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         6969157.4         55           J270         454857.69         6969219.5         66           J271         45480.03         6969547.6         88           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J276         454639.96         6969575.9         88           J278         454678.03         6969569.7         88           J283         454682.63         6969569.7         88           J290         454701.53         6969545.1         88           J290         454705.21         6969528.9         88           J297         454668.24         6969472.6         88           J306         454742.19         6969332.3         77           J316         454913.9         6969187.9         55           J280         454659.01         6969208.3  | 51.82          | 5           | 6969251.2    | 455180.55 | J244 |
| J263         454991.64         6969172.5         55           J264         454927.8         6969169.3         55           J267         454895.53         6969165.1         55           J268         454910.4         6969157.4         55           J270         454857.69         6969219.5         66           J271         454800.3         6969210.8         66           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J278         454678.03         6969547.6         88           J283         454678.03         6969569.7         88           J283         454682.63         6969569.7         88           J290         454701.53         6969545.1         88           J291         454678.03         6969545.1         88           J292         454705.21         6969545.1         88           J292         454705.21         6969545.1         88           J306         454742.19         6969187.9         55           J316         454659.01         6969546.2         88           J133         455101.4         6969208.3  | 51.20          | 5           | 6969230.6    | 455092.22 | J248 |
| J264         454927.8         6969169.3         5           J267         454895.53         6969165.1         5           J268         454910.4         6969157.4         5           J270         454857.69         6969219.5         6           J271         45480.03         6969210.8         6           J272         454601.02         6969547.6         8           J274         454629.37         6969587.9         8           J276         454639.96         6969575.9         8           J278         454678.03         6969567.4         8           J283         454682.63         6969569.7         8           J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         454742.19         6969332.3         7           J316         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5  | 55.13          | 5           | 6969183.4    | 455004.78 | J261 |
| J267         454895.53         6969165.1         55           J268         454910.4         6969157.4         55           J270         454857.69         6969219.5         66           J271         454840.03         6969210.8         66           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J276         454639.96         6969575.9         88           J278         454678.03         69695631.3         88           J283         454682.63         6969569.7         88           J283         454682.63         6969569.7         88           J290         454701.53         6969545.1         88           J292         454705.21         6969528.9         88           J297         454668.24         6969472.6         88           J306         454742.19         6969332.3         77           J316         454659.01         6969546.2         88           J133         455101.4         6969208.3         55           J234         455232.32         6969219.5         55  | 55.21          | 5           | 6969172.5    | 454991.64 | J263 |
| J268         454910.4         6969157.4         5           J270         454857.69         6969219.5         6           J271         454840.03         6969210.8         6           J272         454601.02         6969547.6         8           J274         454629.37         6969587.9         8           J276         454639.96         6969575.9         8           J278         454678.03         6969631.3         8           J283         454682.63         6969567.4         8           J285         454690.36         6969569.7         8           J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         454742.19         6969332.3         7           J316         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 57.72          | 5           | 6969169.3    | 454927.8  | J264 |
| J270         454857.69         6969219.5         66           J271         454840.03         6969210.8         66           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J276         454678.03         6969631.3         88           J283         454682.63         6969567.4         88           J285         454690.36         6969569.7         88           J290         454701.53         6969545.1         88           J292         454705.21         6969528.9         88           J297         454668.24         6969545.1         88           J297         454668.24         6969472.6         88           J306         454742.19         6969332.3         77           J316         454913.9         6969187.9         55           J280         454659.01         6969208.3         55           J234         455232.32         6969219.5         55  | 59.00          | 5           | 6969165.1    | 454895.53 | J267 |
| J271         454840.03         6969210.8         66           J272         454601.02         6969547.6         88           J274         454629.37         6969587.9         88           J276         454639.96         6969575.9         88           J278         454682.63         6969567.4         88           J283         454682.63         6969567.4         88           J290         454701.53         6969545.1         88           J292         454701.53         6969528.9         88           J292         454701.53         6969545.1         88           J292         454701.53         6969545.1         88           J293         454668.24         6969472.6         88           J297         454668.24         6969187.9         55           J316         454913.9         6969187.9         55           J280         454659.01         6969208.3         55           J234         455232.32         6969219.5         55  | 57.11          | 5           | 6969157.4    | 454910.4  | J268 |
| J272         454601.02         6969547.6         8           J274         454629.37         6969587.9         8           J276         454639.96         6969575.9         8           J278         454678.03         6969631.3         8           J283         454682.63         6969567.4         8           J285         454690.36         6969545.1         8           J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         454742.19         6969332.3         7           J316         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 60.80          | 6           | 6969219.5    | 454857.69 | J270 |
| J274         454629.37         6969587.9         8           J276         454639.96         6969575.9         8           J278         454678.03         6969631.3         8           J283         454682.63         6969567.4         8           J285         454690.36         6969545.1         8           J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         45471.9         6969332.3         7           J316         45469.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 61.00          | 6           | 6969210.8    | 454840.03 | J271 |
| J276         454639.96         6969575.9         88           J278         454678.03         6969631.3         88           J283         454682.63         6969567.4         88           J285         454690.36         6969569.7         88           J290         454701.53         6969545.1         88           J292         454705.21         6969528.9         88           J297         454668.24         6969472.6         88           J306         454742.19         6969332.3         77           J316         454659.01         6969546.2         88           J133         455101.4         6969208.3         55           J234         455232.32         6969219.5         55  | 85.00          | 8           | 6969547.6    | 454601.02 | J272 |
| J278         454678.03         6969631.3         8           J283         454682.63         6969567.4         8           J285         454690.36         6969569.7         8           J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         45471.9         6969332.3         7           J316         45469.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 84.68          | 8           | 6969587.9    | 454629.37 | J274 |
| J283       454682.63       6969567.4       8         J285       454690.36       6969569.7       8         J290       454701.53       6969545.1       8         J292       454705.21       6969528.9       8         J297       454668.24       6969472.6       8         J306       454742.19       6969332.3       7         J316       454659.01       6969546.2       8         J133       455101.4       6969208.3       5         J234       455232.32       6969219.5       5   | 83.27          | 8           | 6969575.9    | 454639.96 | J276 |
| J285         454690.36         6969569.7         8           J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         454701.9         6969332.3         7           J316         454913.9         6969187.9         5           J280         454659.01         6969208.3         5           J133         455101.4         6969208.3         5  | 87.59          | 8           | 6969631.3    | 454678.03 | J278 |
| J290         454701.53         6969545.1         8           J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         454742.19         6969332.3         7           J316         454913.9         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5  | 81.08          | 8           | 6969567.4    | 454682.63 | J283 |
| J292         454705.21         6969528.9         8           J297         454668.24         6969472.6         8           J306         454742.19         6969332.3         7           J316         454913.9         6969187.9         5           J280         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5  | 83.06          | 8           | 6969569.7    | 454690.36 | J285 |
| J297         454668.24         6969472.6         8           J306         454742.19         6969332.3         7           J316         454913.9         6969187.9         5           J280         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 86.45          | 8           | 6969545.1    | 454701.53 | J290 |
| J306         454742.19         6969332.3         7           J316         454913.9         6969187.9         5           J280         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5  | 86.88          | 8           | 6969528.9    | 454705.21 | J292 |
| J316         454913.9         6969187.9         5           J280         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 81.36          | 8           | 6969472.6    | 454668.24 | J297 |
| J280         454659.01         6969546.2         8           J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5   | 70.00          | 7           | 6969332.3    | 454742.19 | J306 |
| J133         455101.4         6969208.3         5           J234         455232.32         6969219.5         5  | 59.00          | 5           | 6969187.9    | 454913.9  | J316 |
| J234 455232.32 6969219.5 5  | 80.60          | 8           | 6969546.2    | 454659.01 | J280 |
|   | 50.40          |             | 6969208.3    |           |      |
| 1945 455995   | 50.02          |             |              |           |      |
|   | 53.05          |             |              |           |      |
|   | 55.42          |             |              |           |      |
|   | 42.90          |             |              |           |      |
|   | 17.11          |             |              |           |      |
|   | 21.75          |             |              |           |      |
|   | 77.09          |             |              |           |      |
|   | 70.70          |             |              |           |      |
|   | 83.52          |             |              |           |      |
|   | 78.57          |             |              |           |      |
|   | 70.97          |             |              |           |      |
|   | 77.00          |             |              |           |      |
|   | 76.39          |             |              |           |      |
|   | 66.00          |             |              |           |      |
|   | 69.00<br>73.02 |             |              |           |      |



|              | Х-         |                        | Invert Elev.   |
|--------------|------------|------------------------|----------------|
| Name         | Coordinate | Y-Coordinate           | (m)            |
| J424         | 454620.32  | 6969742.1              | 84.96          |
| J439         | 454123.32  | 6969692.1              | 72.37          |
| J441         | 454559.32  | 6969733.1              | 83.92          |
| J460         | 454658.32  | 6969697.1              | 85.97          |
| J485         | 454724.32  | 6969650.1              | 91.14          |
| J489         | 454246.32  | 6969663.1              | 66.70          |
| J493         | 454131.32  | 6969660.1              | 70.90          |
| J495         | 454939.32  | 6969650.1              | 104.41         |
| J497         | 454864.32  | 6969633.1              | 95.99          |
| J506         | 454240.32  | 6969637.1              | 66.80<br>84.00 |
| J509         | 454629.32  | 6969597.1              | 84.99          |
| J511         | 454329.32  | 6969632.1              | 65.96<br>78.21 |
| J515<br>J523 | 454968.32  | 6969631.1<br>6969613.1 | 108.95         |
| J525         | 455141.32  | 6969343.1              | 72.14          |
| J533         | 454144.32  | 6969590.1              | 67.00          |
| J537         | 455243.32  | 6969485.1              | 118.04         |
| J541         | 454819.32  | 6969559.1              | 92.89          |
| J545         | 454218.32  | 6969598.1              | 66.90          |
| J553         | 455035.32  | 6969550.1              | 118.99         |
| J564         | 454851.32  | 6969581.1              | 92.97          |
| J586         | 454207.32  | 6969516.1              | 66.99          |
| J588         | 454812.32  | 6969507.1              | 92.24          |
| J594         | 454452.32  | 6969501.1              | 81.04          |
| J606         | 454457.32  | 6969473.1              | 76.59          |
| J615         | 454571.32  | 6969420.1              | 70.97          |
| J617         | 454193.32  | 6969484.1              | 66.99          |
| J621         | 455079.32  | 6969407.1              | 96.00          |
| J629         | 454192.32  | 6969470.1              | 66.99          |
| J634         | 454475.32  | 6969439.1              | 71.00          |
| J638         | 455376.32  | 6969319.1              | 66.80          |
| J649         | 455239.32  | 6969314.1              | 62.87          |
| J671         | 454188.32  | 6969395.1              | 66.99          |
| J674         | 455192.32  | 6969343.1              | 68.46          |
| J678         | 454991.32  | 6969361.1              | 90.50          |
| J680         | 454807.32  | 6969340.1              | 76.85          |
| J683         | 454493.32  | 6969424.1              | 70.99          |
| J706         | 454799.32  | 6969338.1              | 76.05          |
| J714         | 454639.32  | 6969324.1              | 70.98          |
| J716         | 454505.32  | 6969327.1              | 74.00          |
| J730         | 454490.32  | 6969310.1              | 74.03          |
| J732         | 454207.32  | 6969308.1              | 66.99          |
| J737         | 454264.32  | 6969378.1              | 66.99          |
| J742         | 455180.32  | 6969274.1              | 51.50          |
| J748         | 455106.32  | 6969245.1              | 51.30          |
| J760         | 454152.32  | 6969246.1              | 79.00          |
| J763         | 454209.32  | 6969281.1              | 66.92          |
| J765         | 455001.32  | 6969246.1              | 58.97          |
| J771         | 454628.32  | 6969259.1              | 85.01          |
| J777         | 454144.32  | 6969238.1              | 79.00          |
| J782<br>J792 | 454242.32  | 6969251.1<br>6969187.1 | 66.80<br>44.33 |
| J792<br>J799 | 455319.32  | 6969187.1              |                |
| 1802         | 454742.32  | 6969168.1              | 69.04<br>13.69 |
| 1809         | 454903.32  | 6969143.6              | 59.10          |
| J813         | 454118.32  | 6969198.1              | 82.00          |
| J822         | 455380.32  | 6969188.1              | 42.84          |
| J837         | 453580.32  | 6969145.1              | 82.00          |
| J855         | 455350.32  | 6969138.1              | 42.99          |
| J859         | 455163.32  | 6969140.1              | 50.99          |
| J861         | 454122.32  | 6969201.1              | 82.00          |
| J887         | 454981.32  | 6969121.1              | 56.83          |
| J895         | 455123.32  | 6969096.1              | 52.93          |
| J905         | 454984.32  | 6969068.1              | 56.95          |
| J911         | 455122.32  | 6969076.1              | 52.17          |
| J918         | 454053.32  | 6969080.1              | 82.91          |
| J930         | 455365.32  | 6969064.1              | 43.00          |
|              |            |                        |                |



| NameCoordinateVeccordinate(m)J942455175.326969075.1444.00J954455242.326969038.1606.01J964455974.326969038.1606.01J964455541.326968963.120.23.33J1005455363.2696893.1606.33.92J1030455181.32696893.1606.33.92J103145592.32696893.1606.33.92J1055455363.2696893.1607.33.02J1050455363.2696893.1607.30.02J105045593.22696873.1607.30.02J106145591.32696873.1607.30.02J107845591.32696873.1607.30.02J113045518.32696873.1607.30.02J113145551.22696873.1607.30.02J113245551.32696875.1607.30.02J113345551.32696875.1607.30.02J113445551.32696875.1607.30.02J113545551.32696875.1607.30.02J113645551.32696875.1607.30.02J113645551.32696875.1607.30.02J113745551.32696875.1607.30.02J113845551.32696875.1607.30.02J114445551.32696875.1607.30.02J115545553.23696875.1607.30.02J116445551.32696875.1607.30.02J115445551.32696875.1607.30.02J1254<   |       | X-         |              | Invert Elev. |
|--|-------|------------|--------------|--------------|
| J95745529.32696899.8144.40J962454924.32696890.8166.2.91J964454978.32696890.8162.91J964455264.32696894.128.3.3J1005455511.32696894.128.3.3J1005455518.32696890.162.9.3J1035455580.32696890.162.9.3J1055455180.32696883.171.71J1057455180.32696883.130.00J105145594.32696883.180.9.3J107045495.32696873.181.9.4J107045518.32696873.181.9.4J107045518.32696873.181.9.7J113045551.32696873.187.97J1133455551.32696873.137.89J113445551.32696873.137.89J113545551.32696873.137.89J113645551.32696873.137.80J113745551.3269687.137.80J113845557.3269687.137.80J113445551.3269687.137.80J113545551.3269687.137.80J113645551.3269687.137.80J113745551.3269687.137.80J113845557.3269687.137.80J113645557.3269687.137.80J113745559.3269687.137.80J114445561.3269687.137.80J125445594.32696   | Name  | Coordinate | Y-Coordinate | (m)          |
| J962454924.326968950.166.2.9.1J964454978.326968038.160.44J976455264.326968936.128.33J1005455518.326968945.128.33J100545536.326968936.163.92J103545536.326968863.13.00J105745518.326968835.13.00J105745518.326968835.13.00J105745518.326968835.13.00J105145534.326968835.13.00J105145534.326968835.13.00J107045495.326968736.13.03J107845498.326968736.13.07.97J11845521.326968736.13.7.97J113045518.326968736.13.7.97J113345557.3.26968737.13.7.00J113545557.3.26968737.13.7.00J113545557.3.26968737.13.7.00J114445531.32696872.13.0.07J115545557.3.2696850.13.6.00J117045581.32696872.13.0.07J118445537.32696850.13.6.00J117045551.32696850.13.6.00J117045554.32696850.13.6.00J117045554.32696850.13.6.00J112645554.32696850.13.6.00J126645584.32696851.13.0.00J126645584.32696831.13.0.00J1266 </td <td>J942</td> <td>455175.32</td> <td>6969075.1</td> <td>49.66</td>   | J942  | 455175.32  | 6969075.1    | 49.66        |
| J964454978.326969038.160.0.4J976455264.32696897.143.00J1001455541.32696894.12.8.33J1005455181.32696891.616.3.92J1033454928.32696890.16.2.33J1055455366.32696886.17.1.71J1059455784.32696886.17.1.71J1059455784.32696886.18.0.33J1061455394.32696885.18.0.33J1078454953.32696878.18.1.94J1099455318.32696878.18.1.94J1099455318.32696873.13.7.97J113045518.32696873.13.7.99J113145557.32696873.13.6.07J113245551.32696873.13.6.07J113445557.32696873.13.6.07J113545551.32696872.13.0.07J113645551.32696872.13.0.07J113745551.32696872.13.0.07J114045521.32696851.13.0.07J114145521.32696851.13.0.07J114545501.32696851.13.0.07J114645551.32696851.13.0.07J114745521.32696851.13.0.07J125645554.32696854.13.0.07J126645584.32696854.13.0.07J126645584.32696834.13.0.07J126745591.32696834.13.0.07J12   | J957  | 455229.32  | 6968998.1    | 44.00        |
| JP76455264.326968957.144.3.0J1001455541.326968945.128.33J1005455181.326968930.166.3.92J1033454928.326968930.162.33J1055455366.32696890.143.00J1057455180.32696883.13.00J1061455394.32696883.13.00J1061455394.32696883.13.00J1070454984.32696883.13.03J1070454984.32696873.13.03J107045498.32696873.13.03J113045518.23696873.13.7.97J113145551.32696873.13.7.89J113345551.32696873.13.6.00J114445504.32696862.13.0.00J114545551.32696873.13.6.00J114645561.32696872.13.0.77J113845557.32696872.13.0.77J1159455050.32696872.13.0.77J115445551.32696872.13.0.07J1155455050.32696872.13.0.07J116445561.32696852.13.0.07J1155455050.32696872.13.0.77J115645555.32696873.13.0.01J116745551.3269687.13.0.01J116845551.3269687.13.0.01J126645554.3269687.13.0.01J126645554.3269683.13.0.01J126645  | J962  | 454924.32  | 6968950.1    | 62.91        |
| J1001         455541.32         6968948.1         22.8.3           J1005         455181.32         6968945.1         57.39           J1033         454928.32         696890.1         66.3.92           J1042         454927.32         696890.1         43.00           J1055         455366.32         6968868.1         71.71           J1059         455784.32         6968835.1         46.87           J1070         454959.32         6968784.1         60.88           J1114         45502.32         696876.1         97.77           J1130         455188.32         696879.1         97.77           J1131         455529.32         696873.1         36.07           J1131         455529.32         696873.1         36.07           J1133         455529.32         696873.1         36.07           J1134         45557.32         696873.1         36.07           J1135         45551.32         696873.1         36.07           J1144         45551.32         696873.1         36.07           J1155         45551.32         696873.1         36.07           J1145         45551.32         696875.1         36.07           J1164   | J964  | 454978.32  | 6969038.1    | 60.44        |
| J1005455181.326968945.157.39J1033454928.32696890.166.3.92J1042454927.32696890.166.2.93J1055455366.32696890.13.00J1057455180.32696883.13.00J1050455784.32696883.13.00J1070454959.32696883.18.0.33J1078454984.32696873.18.1.94J1099455318.32696873.18.1.94J1090455318.32696873.13.7.97J1118455543.2696873.13.7.97J1130455573.32696873.13.6.07J1133455573.32696873.13.6.07J1134455583.2696873.13.6.07J1135455573.326968668.140.06J117045581.32696865.13.7.07J118445537.32696852.13.8.20J118545505.32696859.13.8.34J120445534.32696859.13.8.34J120445534.32696859.13.8.34J120545504.32696843.13.0.0J126645554.3269683.13.0.0J126645554.3269683.13.0.0J126645554.3269683.13.0.0J126645554.3269683.13.0.0J126645554.3269683.13.0.0J126645554.3269683.13.0.0J126645554.3269683.13.0.0J126645554.  |       | 455264.32  |              | 43.00        |
| J1033454928.326968916.166.3.23J1042454927.326968930.1662.33J1055455366.32696890.143.00J105745518.0326968863.13.00J1050455784.326968835.146.87J1070454959.326968835.180.93J1078454984.326968734.160.88J111445502.326968734.160.88J111445502.326968734.160.88J111445502.326968734.136.00J113045518.326968734.136.00J113145551.326968734.136.00J113245551.326968734.136.00J113445557.32696876.137.00J113545551.32696876.137.00J113645551.32696867.130.07J113845557.32696867.130.07J114445531.32696850.182.07J115445505.32696850.137.89J116445551.32696850.136.00J117045504.32696850.137.89J120445531.32696850.137.89J120545504.32696850.137.89J120645504.32696843.130.00J122045543.2696843.137.60J122045543.2696843.137.61J122045543.2696833.137.61J122045504.32696834.137.69J122045504.32 </td <td></td> <td></td> <td></td> <td></td>   |       |            |              |              |
| 11042         454927.32         6968930.1         62.93           11055         455366.32         6968809.1         43.00           11057         455180.32         6968863.1         3.00           11061         455394.32         6968835.1         46.87           11070         454959.32         6968831.1         81.94           11099         455318.32         696876.1         97.97           1118         45546.32         696873.1         37.89           11130         455188.32         696873.1         36.00           11131         45557.32         696873.1         36.00           11131         45557.32         696873.1         36.00           11141         45501.32         696873.1         36.00           11133         45557.32         696873.1         36.00           11141         45501.32         696873.1         36.00           11141         45503.2         696873.1         36.00           11141         45503.32         696873.1         36.00           11142         45503.32         696873.1         36.00           11142         45503.32         696850.1         82.00           11150         45  |       |            |              |              |
| J1055455366.326968809.144.00J1057455180.326968863.17.1.71J1059455784.326968863.13.00J1061455394.326968835.180.93J1078454984.326968831.181.94J1099455318.326968761.197.97J11845546.326968769.147.97J1130455188.32696873.13.7.89J113545551.32696873.13.6.00J114445528.32696873.13.6.00J113545551.32696873.13.6.00J114445528.32696873.13.6.00J114545551.32696873.13.6.00J114645521.32696876.17.3.00J116145521.32696872.13.0.77J118545503.32696850.182.00J117045533.32696850.182.83J120445533.43696850.188.95J120445533.326968351.178.83J120445533.326968351.178.43J120445533.326968351.16.00J125645504.32696845.17.3.07J123345492.83696835.17.8.9J126445503.32696833.17.8.9J126545504.32696833.17.8.9J126445503.32696833.17.8.9J126545505.32696833.17.8.9J132445503.32696833.17.8.9J13244557  |       |            |              |              |
| J1057         455180.32         6968868.1         7.1.71           J1059         455784.32         696883.1         3.00           J1061         455394.32         696883.1         88.93           J1070         454999.32         696883.1         88.93           J1078         454984.32         6968784.1         60.88           J114         45502.32         6968769.1         47.97           J1130         455188.32         6968673.1         37.89           J1133         455529.32         696873.1         36.07           J1134         45551.32         696866.1         73.00           J1147         455283.32         696866.1         40.06           J1170         45561.32         696850.1         82.07           J1185         45505.32         696850.1         82.00           J1184         455337.32         696850.1         82.00           J1185         45505.32         696850.1         82.01           J1204         45534.32         696851.1         83.41           J1204         45534.32         696851.1         83.41           J1204         45535.32         696831.1         34.00           J1226 <td< td=""><td></td><td></td><td></td><td></td></td<>                          |       |            |              |              |
| 1059         455784.32         6968863.1         3.00           J1061         455394.32         6968835.1         46.87           J1070         454999.32         6968845.1         80.93           J1078         454984.32         6968843.1         81.94           J1099         455318.32         696876.1         97.97           J118         455446.32         696873.1         37.89           J1130         45518.32         696873.1         36.07           J1131         45557.32         696873.1         36.07           J1131         45551.32         696867.1         30.07           J1132         45551.32         696866.1         40.06           J1170         45561.32         696872.1         30.77           J1185         455050.32         696850.1         82.00           J1184         455337.32         696850.1         88.93           J1200         455394.32         696851.1         83.34           J1204         45533.2         696851.1         83.34           J1205         45549.32         696851.1         84.90           J1206         45593.42         696851.1         69.63           J1220         45  |       |            |              |              |
| 1061         455394.32         6968835.1         46.87           J1070         45499.32         6968845.1         80.93           J1078         45499.32         6968831.1         81.94           J1099         455318.32         6968736.1         97.97           J118         455466.32         6968793.1         84.17           J1130         455188.32         696873.1         37.89           J1131         455529.32         696873.1         36.97           J1133         45557.32         696870.1         73.00           J1144         455288.32         6968668.1         82.07           J1164         455614.32         696860.1         82.00           J1164         455513.22         696850.2         82.00           J118         45503.32         696850.1         82.00           J118         45533.32         696850.1         83.34           J1200         45534.32         696851.1         90.17           J118         455064.32         696851.1         90.17           J123         454928.32         696851.1         90.17           J123         455064.32         696843.1         6.00.0           J126         4  |       |            |              |              |
| J107045499.326968845.180.93J1078454984.326968831.181.94J1099455318.326968734.160.88J11445502.236968736.197.97J118455446.326968793.184.17J1130455188.32696873.137.89J113545557.32696873.136.97J11345557.32696873.136.97J11345528.32696873.136.00J11445528.32696866.182.07J11645514.32696866.182.07J1164455614.326968626.179.86J1170455631.32696850.182.00J118445533.32696850.182.00J118445534.32696851.179.86J1196455251.32696851.178.88J120045534.32696851.190.17J123345492.8.32696851.190.17J123445506.326968451.130.00J126545505.32696842.173.94J126445505.32696833.175.99J132445551.32696833.175.99J132445551.32696833.175.99J132445551.32696833.175.91J133445557.32696833.175.91J134445557.32696831.110.01J135145544.32696826.177.40J136045571.32696831.110.01J137445573.326   |       |            |              |              |
| 1078         454984.32         696833.11         81.94           11099         455318.32         6968784.1         60.88           1114         455022.32         696876.1         97.97           11130         455188.32         696893.1         84.17           11130         455529.32         696873.1         37.89           11135         455551.32         696873.1         36.97           11138         455575.32         696867.1         73.00           11147         455288.32         696867.1         30.07           11164         455613.32         696866.1         40.06           11170         455613.32         696850.1         82.00           11188         45537.32         696850.1         83.34           11200         45534.32         696850.1         83.34           11200         45534.32         696851.1         83.34           11204         455353.2         696851.1         90.17           11233         45492.83         696851.1         64.00           11264         45541.32         696843.1         64.02           11220         45541.32         69683.1         73.67           11221         45  |       |            |              |              |
| 11099         455318.32         6968784.1         60.88           1114         455022.32         6968769.1         97.97           1118         455446.32         696879.1         47.97           11130         455188.32         696873.1         37.89           11133         455529.32         696873.1         36.97           11138         455575.32         696873.1         36.00           11147         455288.32         696867.1         73.00           11162         455215.32         696866.1         40.06           11170         455613.2         696867.1         30.77           11188         455337.32         696850.1         82.00           11188         45534.32         696850.1         83.34           11200         45534.32         696851.1         90.17           11233         45492.32         696851.1         90.17           11233         45492.32         696845.1         34.00           1126         45554.32         696837.1         34.01           1126         455419.32         696845.1         34.00           1126         45549.32         696843.1         34.00           1126         45549  |       |            |              |              |
| 11114         45502.32         69687361         97.97           11130         455148.32         6968769.1         47.97           11130         455188.32         696873.1         37.89           11135         45555.32         696873.1         36.97           11138         45557.32         696873.1         36.00           11147         455288.32         696866.1         82.07           11164         455614.32         696866.1         82.07           11164         45561.32         696866.1         40.06           11170         455631.32         696850.1         82.00           1118         45505.32         696850.1         82.00           1118         45537.32         696850.1         83.34           1200         45534.32         696850.1         86.95           1120         45504.32         696851.1         84.31           1220         455419.32         6968451.1         64.00           1125         45505.32         6968451.1         64.00           1256         45535.32         696842.1         73.94           1220         45513.2         696842.1         73.94           1254         455054.32 <td></td> <td></td> <td></td> <td></td>                                   |       |            |              |              |
| 11118         455446.32         6968769.1         47.97           11130         455188.32         696893.1         84.17           11133         455529.32         696873.1         37.89           11135         45557.32         696873.1         36.97           11138         45557.32         696866.1         73.00           11147         45528.32         696866.1         82.07           11164         455614.32         696866.1         40.06           11170         455631.32         6968502.1         82.00           1118         45505.0.32         6968501         82.00           1118         45537.32         696850.1         82.00           1118         455347.32         696850.1         86.95           1120         45534.32         696850.1         86.95           1120         45504.32         6968451.1         84.31           1220         455419.32         6968451.1         64.00           1125         45505.32         6968451.1         64.00           1126         45585.32         6968451.1         64.00           1126         45505.32         696842.1         73.94           1226         455854.  |       |            |              |              |
| 1130         455188.32         6968693.1         84.17           11133         45552.32         6968737.1         37.89           11135         455551.32         696873.1         36.07           11138         45557.32         696873.1         36.00           11147         455288.32         696866.1         82.07           11164         455614.32         696866.1         40.06           11170         455631.32         6968502.1         82.00           1118         45505.32         696857.1         30.77           1188         455337.32         696857.1         83.34           11200         45534.32         696855.1         86.95           11204         45534.32         696851.1         83.44           1220         45549.32         696845.1         78.43           1220         45549.32         696845.1         64.00           1223         45595.32         696845.1         34.00           1226         454826.32         696842.1         73.94           1227         455054.32         696833.1         75.67           1227         455054.32         696832.1         75.99           1328         45578.32<  |       |            |              |              |
| 11133         455529.32         6968737.1         37.89           11135         455551.32         696873.1         36.97           11138         455555.32         696873.1         36.00           11147         455288.32         696866.1         73.00           11162         455215.32         6968668.1         40.06           11170         455631.32         6968502.1         82.07           1118         45505.32         6968502.1         82.00           1118         455337.32         6968501         86.95           11196         455251.32         696851.1         83.34           11200         45534.32         696851.1         83.34           11204         45534.32         6968451.1         86.95           11205         45504.32         6968451.1         696.00           11220         45549.32         6968451.1         696.00           11220         45549.32         6968451.1         69.00           11223         45595.32         696842.1         73.94           11224         45505.32         696842.1         73.94           11225         45505.32         696833.1         75.99           11324   |       |            |              |              |
| 11135         455551.32         6968734.1         36.97           11138         455575.32         6968730.1         36.00           11147         45528.32         696866.1         73.00           11162         455215.32         6968668.1         40.06           11170         455631.32         6968502.1         82.00           11184         455575.32         696852.1         82.00           11185         455050.32         696852.1         82.00           11184         455317.32         6968550.1         86.95           11200         45534.32         6968550.1         86.95           11204         455354.32         6968519.1         90.17           11233         454928.32         696845.1         69.05           1126         455354.32         696843.1         69.05           1126         455854.32         696842.1         73.94           1126         455054.32         696843.1         73.60           11277         45506.32         696843.1         73.67           11274         455054.32         696819.1         30.00           11283         45578.32         696833.1         75.89           11324   |       |            |              |              |
| 11138         455575.32         6968730.1         36.00           11147         455288.32         696867.1         73.00           11162         455215.32         6968668.1         40.06           11164         455614.32         6968668.1         40.06           11170         455631.32         6968502.1         82.00           1118         455050.32         6968502.1         82.00           1118         45537.32         6968571.1         83.34           11200         455394.32         6968550.1         86.95           11204         45534.32         6968459.1         78.43           11204         455353.2         6968459.1         69.25           11220         455492.32         696843.1         69.25           11220         455492.32         696842.1         69.25           11226         455854.32         696842.1         73.94           11226         455854.32         696839.1         30.00           11226         455854.32         696839.1         73.67           11227         455006.32         696839.1         75.99           11328         45578.32         696839.1         75.99           11329  |       |            |              |              |
| 11147         455288.32         6968676.1         73.00           11162         455215.32         6968668.1         82.07           11164         455614.32         6968668.1         40.06           11170         455631.32         696872.1         30.77           11185         45505.32         6968502.1         82.00           11184         455337.32         696850.1         79.86           11196         455251.32         6968571.1         83.34           1200         455394.32         6968459.1         78.83           11204         455394.32         6968459.1         78.43           11206         455064.32         6968459.1         90.17           11233         454928.32         6968459.1         30.0           1126         455054.32         6968435.1         34.00           1126         455054.32         696842.1         73.94           1126         455054.32         696833.1         75.99           11277         45506.32         696833.1         75.89           11324         455251.32         696833.1         75.89           11324         455254.32         696826.1         76.01           11334  |       |            |              |              |
| 11162         455215.32         6968668.1         82.07           11164         455614.32         6968668.1         40.06           11170         455631.32         6968727.1         30.77           11185         455050.32         6968502.1         82.00           11188         455337.32         6968261.1         79.86           11196         455251.32         6968501.1         83.34           1200         455394.32         6968550.1         86.95           11204         455354.32         6968459.1         78.43           11200         455419.32         6968459.1         90.17           11233         454928.32         6968451.1         69.025           11262         454826.32         6968451.1         69.025           11263         455054.32         6968374.1         69.025           11264         455054.32         696842.1         73.94           11283         455054.32         6968334.1         75.99           11324         455551.32         6968392.1         68.55           11339         45548.32         6968392.1         68.55           11334         45557.32         6968238.1         76.01           1   |       |            |              |              |
| 11164         455614.32         6968868.1         40.06           11170         455631.32         6968727.1         30.77           11185         455050.32         6968502.1         82.00           11184         455337.32         6968261.1         79.86           11196         455251.32         6968591.1         83.34           1200         455394.32         6968550.1         86.95           11206         455064.32         6968519.1         90.17           11233         454928.32         6968319.1         90.17           11233         454928.32         6968459.1         3.00           11266         45554.32         6968423.1         73.67           11277         45506.32         696839.1         3.00           11268         45554.32         696839.1         3.00           11264         45554.32         696839.1         3.00           11283         455635.32         696839.1         3.00           11284         45552.32         696839.1         3.00           11328         455789.32         696839.1         6.55           11339         455498.32         696839.1         6.55           1339 <td< td=""><td></td><td></td><td></td><td></td></td<>                          |       |            |              |              |
| 11170         455631.32         6968727.1         30.77           11185         455050.32         6968502.1         82.00           11188         455337.32         696826.1         79.86           11196         455251.32         6968393.1         78.88           11200         455394.32         6968550.1         86.95           11204         455354.32         6968459.1         78.43           11204         455354.32         6968459.1         90.17           11233         454928.32         6968454.1         64.00           11256         45535.32         6968454.1         69.02           11262         454826.32         6968423.1         73.67           11277         455064.32         6968398.1         63.00           11268         45554.32         696833.1         75.99           11324         45552.32         696833.1         75.99           11324         45552.32         696832.1         8.45           11334         45552.32         696832.1         6.61           11339         455498.32         69682.01         72.40           11360         455354.32         69682.01         76.01           1339   |       |            |              |              |
| 11185         455050.32         6968502.1         82.00           11188         455337.32         6968626.1         79.86           11196         455251.32         6968393.1         78.88           11200         455394.32         6968550.1         86.95           11204         455354.32         6968550.1         86.95           11206         455064.32         6968459.1         78.43           11220         455419.32         6968459.1         90.17           11233         454928.32         6968374.1         64.00           11256         455535.32         6968435.1         34.00           11261         454826.32         6968423.1         73.67           11277         455064.32         6968398.1         63.00           11268         455054.32         6968398.1         63.00           11309         455139.32         6968333.1         75.89           11324         455552.32         6968398.1         63.00           11339         455498.32         6968398.1         66.10           11334         45552.32         6968398.1         65.52           11334         455250.32         6968208.1         76.01           1   |       |            |              |              |
| 11196         455251.32         6968393.1         78.88           11200         455394.32         6968571.1         83.34           11204         455354.32         6968550.1         86.95           11206         455064.32         6968519.1         90.17           11233         454928.32         6968464.1         64.00           11256         45553.32         6968374.1         69.25           11262         454826.32         6968435.1         34.00           11266         455854.32         6968423.1         73.67           11277         45506.32         6968398.1         63.00           11309         455139.32         6968398.1         63.00           11309         455139.32         6968393.1         75.89           11324         45552.32         6968392.1         84.55           1339         45548.32         696820.1         84.55           1339         455498.32         696820.1         72.40           1346         45577.32         6968238.1         10.01           1372         455243.22         6968238.1         64.85           1339         45544.32         6968238.1         64.85           13394   | J1185 | 455050.32  | 6968502.1    | 82.00        |
| J1200         455394.32         6968571.1         83.34           J1204         455354.32         6968550.1         86.95           J1206         455064.32         6968519.1         90.17           J1233         454928.32         6968464.1         64.00           J1262         455535.32         6968374.1         69.25           J1262         454826.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1264         455535.32         6968398.1         63.00           J1277         455006.32         6968398.1         63.00           J1283         455635.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.89           J1324         45557.32         6968392.1         68.55           J1334         455578.32         6968194.1         63.52           J1334         455243.32         696820.1         72.40           J1360         455371.32         6968238.1         60.01           J1372         45544.32         6968238.1         60.01           J1387         455458.32         6968135.1         61.67           J13   | J1188 | 455337.32  | 6968626.1    | 79.86        |
| J1204         455354.32         6968550.1         86.95           J1206         455064.32         6968459.1         78.43           J1220         455419.32         6968519.1         90.17           J1233         454928.32         6968464.1         64.00           J1256         455535.32         6968374.1         692.5           J1262         454826.32         6968435.1         34.00           J1266         455854.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.89           J1324         45552.32         6968392.1         68.55           J1334         455543.32         6968194.1         63.52           J1334         455543.32         696820.1         72.40           J1360         455354.32         696820.1         72.40           J1360         455354.32         6968218.1         60.61           J1360         455571.32         6968218.1         64.85           J1394         45571.32         6968218.1         63.96           J1387         45548.32         696813.1         13.67           J1388<   | J1196 | 455251.32  | 6968393.1    | 78.88        |
| J1206         455064.32         6968459.1         78.43           J1220         455419.32         6968519.1         90.17           J1233         454928.32         6968374.1         69.25           J1266         455535.32         6968374.1         69.25           J1262         454826.32         6968435.1         34.00           J1268         455054.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.99           J1324         455251.32         6968333.1         75.89           J1328         455789.32         6968326.1         8.45           J1334         455243.32         6968268.1         76.01           J1360         455354.32         696820.1         72.40           J1361         455243.32         696820.1         72.40           J1362         455715.32         6968218.1         64.85           J1394         455715.32         6968187.1         13.67           J1372         455243.32         6968187.1         13.67           J1387         455444.32         6968135.1         64.85           J13   | J1200 | 455394.32  | 6968571.1    | 83.34        |
| J1220         455419.32         6968519.1         90.17           J1233         454928.32         6968464.1         64.00           J1266         455535.32         6968374.1         69.25           J1262         454826.32         6968435.1         34.00           J1266         455854.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1309         455139.32         6968354.1         75.99           J1324         455251.32         6968333.1         75.89           J1328         455789.32         6968392.1         68.55           J1339         455498.32         6968194.1         63.52           J1334         45552.32         696820.1         72.40           J1360         455354.32         6968238.1         76.01           J1360         455250.32         6968238.1         76.01           J1361         455250.32         6968238.1         76.01           J1372         455244.32         6968136.1         64.85           J1387         455448.32         6968136.1         64.85           J1384         455571.32         6968136.1         63.96           J1   | J1204 | 455354.32  | 6968550.1    | 86.95        |
| J1233         454928.32         6968464.1         64.00           J1256         455535.32         6968374.1         69.25           J1262         454826.32         6968435.1         34.00           J1266         455854.32         6968423.1         73.67           J1277         455006.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1309         455139.32         696833.1         75.89           J1324         455525.32         696833.1         75.89           J1328         455789.32         6968323.1         8455           J1334         45552.32         6968323.1         68.55           J1339         455498.32         6968194.1         63.52           J1351         455243.32         696820.1         72.40           J1360         455354.32         6968238.1         10.01           J1372         455444.32         6968238.1         60.61           J1387         455456.32         6968136.1         63.96           J1398         455571.32         6968136.1         63.96           J1410         455575.32         6968132.1         42.34           J1427   | J1206 | 455064.32  | 6968459.1    | 78.43        |
| J1256         455535.32         6968374.1         69.25           J1262         454826.32         6968435.1         34.00           J1266         455854.32         6968423.1         73.67           J1277         455006.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.89           J1324         455251.32         6968392.1         68.55           J1334         455578.32         6968392.1         68.55           J1339         455498.32         6968268.1         76.01           J1360         455374.32         6968208.1         76.01           J1361         45527.32         6968208.1         76.01           J1361         455771.32         6968238.1         10.01           J1372         455243.2         6968209.1         71.00           J1381         455771.32         6968218.1         64.85           J1394         455775.32         6968135.1         13.67           J1387         45544.32         6968135.1         14.99           J1419         455571.32         6968135.1         19.99           J14   | J1220 | 455419.32  | 6968519.1    | 90.17        |
| J1262         454826.32         6968435.1         34.00           J1266         455854.32         6968549.1         3.00           J1268         455054.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.89           J1328         455521.32         6968392.1         68.55           J1334         455523.2         6968392.1         68.55           J1334         455498.32         6968268.1         76.01           J1360         455354.32         696820.1         72.40           J1360         455354.32         696820.1         72.40           J1361         455250.32         6968238.1         10.01           J1372         455243.32         6968238.1         64.85           J1387         455444.32         6968209.1         71.00           J1372         455571.32         6968135.1         13.67           J1387         455571.32         6968135.1         63.96           J1411         455575.32         6968135.1         63.96           J1419         455571.32         6968135.1         19.99           J144   | J1233 | 454928.32  | 6968464.1    | 64.00        |
| J1266         455854.32         6968549.1         3.00           J1268         455054.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1283         455635.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.89           J1324         455251.32         6968333.1         75.89           J1328         455789.32         6968392.1         68.55           J1334         45552.32         6968194.1         63.52           J1339         455498.32         6968206.1         76.01           J1360         455354.32         6968238.1         76.01           J1368         455771.32         6968238.1         76.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968238.1         76.01           J1387         455444.32         6968238.1         76.01           J1387         455453.2         6968135.1         13.67           J1394         455775.32         6968135.1         13.67           J1419         455676.32         6968135.1         16.73           J14   | J1256 | 455535.32  | 6968374.1    | 69.25        |
| J1268         455054.32         6968423.1         73.67           J1277         455006.32         6968398.1         63.00           J1283         455635.32         6968398.1         75.99           J1309         455139.32         6968333.1         75.89           J1324         455251.32         6968332.1         8455           J1328         455789.32         6968236.1         8.45           J1334         45552.32         6968194.1         63.52           J1339         455498.32         6968268.1         76.01           J1360         455354.32         6968238.1         10.01           J1372         455250.32         6968238.1         10.01           J1372         455250.32         6968238.1         64.85           J1394         455771.32         6968209.1         71.00           J1411         455458.32         6968132.1         64.85           J1398         455376.32         6968132.1         63.96           J1411         455571.32         6968132.1         16.73           J1427         45565.32         6968135.1         16.73           J1427         45565.32         6968135.1         16.73           J1427   | J1262 | 454826.32  | 6968435.1    | 34.00        |
| J1277         455006.32         6968442.1         73.94           J1283         455635.32         6968398.1         63.00           J1309         455139.32         6968333.1         75.99           J1324         455251.32         6968333.1         75.89           J1324         455552.32         6968392.1         68.55           J1334         455552.32         6968392.1         68.55           J1339         455498.32         6968268.1         76.01           J1360         455354.32         6968220.1         72.40           J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968238.1         64.85           J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968187.1         13.67           J1411         455453.2         6968132.1         42.34           J1427         455655.32         6968135.1         16.73           J1427         455641.32         6968004.1         9.27           J1436         455670.32         6968135.1         16.73           J1   | J1266 | 455854.32  | 6968549.1    | 3.00         |
| J1283         455635.32         6968398.1         63.00           J1309         455139.32         6968354.1         75.99           J1324         455251.32         6968333.1         75.89           J1328         455789.32         6968392.1         68.55           J1334         455552.32         6968392.1         68.55           J1339         455498.32         6968194.1         63.52           J1351         455243.32         6968220.1         72.40           J1360         455354.32         6968238.1         10.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968238.1         76.01           J1387         455444.32         6968238.1         76.01           J1387         455444.32         6968209.1         71.00           J1411         455458.32         6968187.1         13.67           J1398         455376.32         6968132.1         42.34           J1419         455571.32         6968135.1         19.99           J1436         455676.32         6968134.1         57.04           J1447         455655.32         6968004.1         9.27           J   | J1268 | 455054.32  | 6968423.1    | 73.67        |
| J1309         455139.32         6968354.1         75.99           J1324         455251.32         6968333.1         75.89           J1328         455789.32         6968236.1         8.45           J1334         455552.32         6968392.1         68.55           J1339         455498.32         6968194.1         63.52           J1330         455498.32         696820.1         72.40           J1360         455354.32         6968238.1         10.01           J1361         455354.32         6968238.1         76.01           J1360         455354.32         6968238.1         76.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968218.1         64.85           J1394         455771.32         6968187.1         13.67           J1398         455376.32         6968181.1         63.96           J1411         455675.32         6968132.1         42.34           J1427         455657.32         6968135.1         16.73           J1445         455676.32         6968135.1         16.73           J1455         455507.32         6968134.1         57.04           J1   | J1277 | 455006.32  | 6968442.1    | 73.94        |
| J1324         455251.32         6968333.1         75.89           J1328         455789.32         6968236.1         8.45           J1334         455552.32         6968392.1         68.55           J1339         455498.32         6968194.1         63.52           J1351         455243.32         6968268.1         76.01           J1360         455354.32         6968238.1         10.01           J1368         455771.32         6968238.1         76.01           J1372         455250.32         6968238.1         76.01           J1372         455444.32         6968218.1         64.85           J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968187.1         13.67           J1398         455571.32         6968184.1         63.96           J1411         455458.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968134.1         57.04           J1447         455665.32         6968004.1         9.27           J1525         455706.32         6968704.1         3.99           J16   | J1283 | 455635.32  | 6968398.1    | 63.00        |
| J1328         455789.32         6968236.1         8.45           J1334         455552.32         6968392.1         68.55           J1339         455498.32         6968194.1         63.52           J1351         455243.32         6968268.1         76.01           J1360         455354.32         6968238.1         10.01           J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968238.1         64.85           J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968187.1         13.67           J1398         455376.32         6968187.1         13.67           J1411         455458.32         6968184.1         63.96           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968004.1         9.27           J1455         455706.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J169   | J1309 | 455139.32  | 6968354.1    | 75.99        |
| J1334         455552.32         6968392.1         68.55           J1339         455498.32         6968194.1         63.52           J1351         455243.32         6968268.1         76.01           J1360         455354.32         6968220.1         72.40           J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968218.1         64.85           J1394         455376.32         6968187.1         13.67           J1398         455376.32         6968187.1         13.67           J1398         455376.32         6968132.1         63.96           J1411         455458.32         6968132.1         42.34           J1412         455571.32         6968132.1         16.73           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         69687961.1         3.99           J1692         454373.32         6968608.1         81.96           J   | J1324 | 455251.32  | 6968333.1    | 75.89        |
| J1339         455498.32         6968194.1         63.52           J1351         455243.32         6968268.1         76.01           J1360         455354.32         6968220.1         72.40           J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968238.1         76.01           J1372         455444.32         6968238.1         76.01           J1387         455444.32         6968218.1         64.85           J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968184.1         63.96           J1411         455458.32         6968132.1         42.34           J1419         455571.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968022.1         15.45           J1467         455665.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J146   | J1328 | 455789.32  | 6968236.1    | 8.45         |
| J1351         455243.32         6968268.1         76.01           J1360         455354.32         6968220.1         72.40           J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968238.1         64.85           J1394         455715.32         6968209.1         71.00           J1411         455458.32         6968132.1         42.34           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         6967961.1         3.99           J1692         454373.32         6968608.1         81.96           J1701         455365.32         6968608.1         81.96           J1713         454165.32         6968608.1         81.96           J1717         45582.32         6968687.1         3.22           J172   | J1334 | 455552.32  | 6968392.1    | 68.55        |
| J1360         455354.32         6968220.1         72.40           J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968218.1         64.85           J1394         455715.32         6968209.1         71.00           J1411         455458.32         6968187.1         13.67           J1398         455376.32         6968132.1         42.34           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968022.1         15.45           J1467         455665.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J1692<   | J1339 | 455498.32  | 6968194.1    | 63.52        |
| J1368         455771.32         6968238.1         10.01           J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968218.1         64.85           J1394         455715.32         6968209.1         71.00           J1411         455458.32         6968132.1         42.34           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         69697961.1         3.99           J1692         454373.32         6968004.1         9.27           J1525         455706.32         6967961.1         3.99           J1692         454373.32         6968608.1         81.96           J1701         455365.32         6968608.1         81.96           J1713         454165.32         6968687.1         3.22           J1720         455742.32         6969888.1         70.94           J172   | J1351 | 455243.32  | 6968268.1    | 76.01        |
| J1372         455250.32         6968238.1         76.01           J1387         455444.32         6968218.1         64.85           J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968209.1         71.00           J1411         455458.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968022.1         15.45           J1467         455665.32         6968004.1         9.27           J1525         455706.32         69697961.1         3.99           J1692         454373.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J1701         455365.32         6968004.1         9.27           J1701 </td <td>J1360</td> <td>455354.32</td> <td></td> <td>72.40</td> | J1360 | 455354.32  |              | 72.40        |
| J1387         455444.32         6968218.1         64.85           J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968209.1         71.00           J1411         455458.32         6968184.1         63.96           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968135.1         15.45           J1467         455641.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         69697961.1         3.99           J1692         454373.32         6968004.1         9.27           J1525         455706.32         6968004.1         9.27           J1525         455365.32         6968004.1         9.27           J1692         454373.32         6969768.1         64.96           J1701         455365.32         696808.1         81.96           J1713         454165.32         6968608.1         81.96           J1717   |       | 455771.32  |              |              |
| J1394         455715.32         6968187.1         13.67           J1398         455376.32         6968209.1         71.00           J1411         455458.32         6968184.1         63.96           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968135.1         16.73           J1455         455676.32         6968022.1         15.45           J1467         455665.32         6968004.1         9.27           J1525         455706.32         69697961.1         3.99           J1692         454373.32         6969768.1         64.96           J1701         455365.32         6968068.1         81.96           J1713         454165.32         6968608.1         3.22           J1710         455822.32         6968687.1         3.22           J1720         455742.32         6969933.1         3.46           J1723         454144.32         6969888.1         70.94  |       |            |              |              |
| J1398         455376.32         6968209.1         71.00           J1411         455458.32         6968184.1         63.96           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968115.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968134.1         57.04           J1467         455641.32         6968004.1         9.27           J1525         455706.32         6969748.1         64.96           J1701         455365.32         6968004.1         81.96           J1701         455365.32         6969748.1         64.96           J1701         455365.32         696808.1         81.96           J1713         454165.32         6968687.1         3.22           J1720         455742.32         69699788.1         69.01           J1723         454144.32         6969888.1         70.94  |       |            |              |              |
| J1411         455458.32         6968184.1         63.96           J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968135.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968134.1         57.04           J1467         455641.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         69697961.1         3.99           J1692         454373.32         6968008.1         81.96           J1701         455365.32         6968608.1         81.96           J1713         454165.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94   |       |            |              |              |
| J1419         455571.32         6968132.1         42.34           J1427         455655.32         6968115.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968134.1         57.04           J1467         455665.32         6968004.1         9.27           J1525         455706.32         6969748.1         64.96           J1701         455365.32         696808.1         81.96           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969888.1         70.94   |       |            |              |              |
| J1427         455655.32         6968115.1         19.99           J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968134.1         57.04           J1467         455641.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         69697961.1         3.99           J1692         454373.32         6969748.1         64.96           J1701         455365.32         6968008.1         81.96           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94   |       |            |              |              |
| J1436         455676.32         6968135.1         16.73           J1455         455507.32         6968134.1         57.04           J1467         455641.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         6969748.1         64.96           J1701         455365.32         6969768.1         69.01           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969888.1         70.94  |       |            |              |              |
| J1455         455507.32         6968134.1         57.04           J1467         455641.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         6967961.1         3.99           J1692         454373.32         6969748.1         64.96           J1701         455365.32         6968008.1         81.96           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94  |       |            |              |              |
| J1467         455641.32         6968022.1         15.45           J1494         455665.32         6968004.1         9.27           J1525         455706.32         6967961.1         3.99           J1692         454373.32         6969748.1         64.96           J1701         455365.32         6969768.1         69.01           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         69699133.1         3.46           J1723         454144.32         6969888.1         70.94   |       |            |              |              |
| J1494         455665.32         6968004.1         9.27           J1525         455706.32         6967961.1         3.99           J1692         454373.32         6969748.1         64.96           J1701         455365.32         6968608.1         81.96           J1713         454165.32         6969768.1         690.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         69699888.1         70.94   |       |            |              |              |
| J1525         455706.32         6967961.1         3.99           J1692         454373.32         6969748.1         64.96           J1701         455365.32         6968608.1         81.96           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94   |       |            |              |              |
| J1692         454373.32         6969748.1         64.96           J1701         455365.32         6968608.1         81.96           J1713         454165.32         6969768.1         6901           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94   |       |            |              |              |
| J1701         455365.32         6968608.1         81.96           J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94  |       |            |              |              |
| J1713         454165.32         6969768.1         69.01           J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94  |       |            |              |              |
| J1717         455822.32         6968687.1         3.22           J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94  |       |            |              |              |
| J1720         455742.32         6969133.1         3.46           J1723         454144.32         6969888.1         70.94   |       |            |              |              |
| J1723 454144.32 6969888.1 70.94  |       |            |              |              |
|  |       |            |              |              |
|  |       |            |              |              |



| J1740<br>J1745<br>J1745<br>J1749<br>J1757<br>J1758<br>J1760<br>J1763<br>J1766<br>J1769<br>J1769<br>J1769<br>J1775<br>J1781<br>J1781<br>J1781<br>J1789<br>J1793<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1839 | Coordinate           454634.32           455257.32           45527.32           455470.32           45519.32           455196.32           455338.32           4554763.32           4554763.32           455407.32           455338.32           455462.32           455407.32           455407.32           455007.32           455368.32           455317.32           455317.32           455139.32 | Y-Coordinate<br>6969540.1<br>6969004.1<br>6968838.1<br>6968973.1<br>6968973.1<br>6968762.1<br>6969299.1<br>6969586.1<br>6969586.1<br>696928.1<br>6969639.1<br>6968805.1<br>6968805.1 | (m)<br>80.82<br>44.00<br>41.30<br>53.05<br>62.91<br>76.01<br>58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12 |
|---|--|--|---|
| J1745<br>J1749<br>J1757<br>J1758<br>J1760<br>J1763<br>J1766<br>J1769<br>J1769<br>J1775<br>J1781<br>J1781<br>J1789<br>J1793<br>J1793<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839                   | 455257.32<br>455470.32<br>455219.32<br>455937.32<br>455196.32<br>455338.32<br>4554763.32<br>454862.32<br>4554862.32<br>455101.32<br>455907.32<br>455007.32<br>455038.32<br>455038.32<br>455038.32  | 6969004.1<br>6968838.1<br>6968292.1<br>6968973.1<br>6968348.1<br>6968762.1<br>6969299.1<br>6969586.1<br>6969586.1<br>6969639.1<br>6969639.1<br>6969639.1<br>6968805.1<br>6968805.1   | 44.00<br>41.30<br>53.05<br>62.91<br>76.01<br>58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12                 |
| J1749<br>J1757<br>J1758<br>J1760<br>J1763<br>J1766<br>J1766<br>J1769<br>J1775<br>J1781<br>J1789<br>J1789<br>J1793<br>J1797<br>J1801<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839                                     | 455470.32<br>455219.32<br>455196.32<br>455196.32<br>455338.32<br>454763.32<br>454763.32<br>4554763.32<br>455101.32<br>455101.32<br>455007.32<br>455007.32<br>455038.32<br>455038.32<br>4555317.32  | 6968838.1<br>6969292.1<br>6968973.1<br>6968348.1<br>6968762.1<br>6969299.1<br>6969586.1<br>6969586.1<br>6969639.1<br>6969639.1<br>69696228.1<br>6968805.1<br>6968805.1               | 41.30<br>53.05<br>62.91<br>76.01<br>58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12                          |
| J1757<br>J1758<br>J1760<br>J1763<br>J1766<br>J1769<br>J1775<br>J1781<br>J1781<br>J1789<br>J1793<br>J1793<br>J1797<br>J1801<br>J1804<br>J1804<br>J1822<br>J1823<br>J1839   | 455219.32<br>454937.32<br>455196.32<br>455338.32<br>454763.32<br>454862.32<br>455101.32<br>455907.32<br>455038.32<br>455038.32<br>455038.32<br>455038.32   | 6969292.1<br>6968973.1<br>6968348.1<br>6968762.1<br>6969299.1<br>6969586.1<br>6969586.1<br>6969639.1<br>6969639.1<br>69696228.1<br>6968805.1<br>6968805.1                            | 53.05<br>62.91<br>76.01<br>58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12                                   |
| J1758<br>J1760<br>J1763<br>J1766<br>J1769<br>J1775<br>J1775<br>J1781<br>J1789<br>J1793<br>J1797<br>J1801<br>J1804<br>J1804<br>J1822<br>J1823<br>J1823   | 454937.32<br>455196.32<br>455338.32<br>454763.32<br>454862.32<br>455101.32<br>455101.32<br>455007.32<br>455007.32<br>455038.32<br>455038.32<br>4555317.32  | 6968973.1<br>6968348.1<br>6968762.1<br>6969299.1<br>6969586.1<br>6969100.1<br>6969639.1<br>6969639.1<br>6969228.1<br>6968805.1<br>6968805.1  | 62.91<br>76.01<br>58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12  |
| J1760<br>J1763<br>J1766<br>J1769<br>J1775<br>J1781<br>J1781<br>J1789<br>J1793<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839   | 455196.32<br>455338.32<br>454763.32<br>454862.32<br>455101.32<br>455928.32<br>455007.32<br>455368.32<br>455038.32<br>455038.32<br>455038.32  | 6968348.1<br>6968762.1<br>6969299.1<br>6969586.1<br>6969100.1<br>6969639.1<br>6969639.1<br>6968805.1<br>6968805.1  | 76.01<br>58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12   |
| J1763<br>J1766<br>J1769<br>J1775<br>J1781<br>J1789<br>J1793<br>J1793<br>J1797<br>J1801<br>J1804<br>J1804<br>J1822<br>J1823<br>J1823   | 455338.32<br>454763.32<br>454862.32<br>455101.32<br>4554928.32<br>455007.32<br>455368.32<br>455038.32<br>4555317.32<br>455139.32   | 6968762.1<br>6969299.1<br>6969586.1<br>6969100.1<br>6969639.1<br>6969228.1<br>6968805.1<br>69688441.1  | 58.99<br>69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12  |
| J1766<br>J1769<br>J1775<br>J1781<br>J1789<br>J1793<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839  | 454763.32<br>454862.32<br>455101.32<br>454928.32<br>455007.32<br>455368.32<br>455038.32<br>455038.32<br>455139.32  | 6969299.1<br>6969586.1<br>6969100.1<br>6969639.1<br>6969228.1<br>6968805.1<br>6968441.1  | 69.13<br>92.98<br>53.36<br>102.97<br>55.01<br>51.12   |
| J1769<br>J1775<br>J1781<br>J1789<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839  | 454862.32<br>455101.32<br>455928.32<br>455007.32<br>455368.32<br>455038.32<br>4555317.32<br>455139.32  | 6969586.1<br>6969100.1<br>6969639.1<br>6969228.1<br>6968805.1<br>6968441.1   | 92.98<br>53.36<br>102.97<br>55.01<br>51.12  |
| J1775<br>J1781<br>J1789<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839   | 455101.32<br>454928.32<br>455007.32<br>455368.32<br>455038.32<br>455317.32<br>455139.32  | 6969100.1<br>6969639.1<br>6969228.1<br>6968805.1<br>6968441.1  | 53.36<br>102.97<br>55.01<br>51.12   |
| J1781<br>J1789<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839  | 454928.32<br>455007.32<br>455368.32<br>455038.32<br>4555137.32<br>455139.32  | 6969639.1<br>6969228.1<br>6968805.1<br>6968441.1   | 102.97<br>55.01<br>51.12  |
| J1789<br>J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839   | 455007.32<br>455368.32<br>455038.32<br>455317.32<br>455139.32  | 6969228.1<br>6968805.1<br>6968441.1  | 55.01<br>51.12  |
| J1793<br>J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1839   | 455368.32<br>455038.32<br>455317.32<br>455139.32   | 6968805.1<br>6968441.1   | 51.12   |
| J1797<br>J1801<br>J1804<br>J1822<br>J1823<br>J1823<br>J1839   | 455038.32<br>455317.32<br>455139.32  | 6968441.1  |   |
| J1801<br>J1804<br>J1822<br>J1823<br>J1839   | 455317.32<br>455139.32   |  | 73.97   |
| J1804<br>J1822<br>J1823<br>J1839  | 455139.32  | 0500050.1  | 68.94   |
| J1822<br>J1823<br>J1839   |  | 6969263.1  | 51.40   |
| J1823<br>J1839  |  | 6969544.1  | 67.00   |
| J1839   | 455765.32  | 6968066.1  | 3.51  |
|   | 455685.32  | 6968387.1  | 61.40   |
| J1846   | 455741.32  | 6969056.1  | 3.00  |
| J1847   | 455836.32  | 6968266.1  | 4.00  |
| J1869   | 455427.12  | 6968859.5  | 42.05   |
| J1872   | 454293.32  | 6969651.1  | 66.60   |
| J1890   | 454821.32  | 6968441.1  | 33.91   |
| J1898   | 455165.32  | 6969252.1  | 52.00   |
| J21   | 454684.33  | 6969618.5  | 86.81   |
| J34   | 454692.17  | 6969391.8  | 71.60   |
| J39   | 455480.11  | 6969121.1  | 48.00   |
| J40   | 455398.38  | 6969238.1  | 51.53   |
| J45   | 454831.09  | 6969193.1  | 60.06   |
| J47   | 455657.29  | 6968734.1  | 22.19   |
| J51   | 455649.1   | 6968764  | 20.40   |
| J54   | 455707.53  | 6968626.9  | 31.77   |
| J32   | 455037.57  | 6969112.8  | 53.66   |
| J37   | 454932.73  | 6969153.3  | 56.20   |
| J55   | 455614.17  | 6968832.9  | 19.86   |
| J57   | 455498.49  | 6968867.8  | 40.96   |
| J60   | 455704.54  | 6968841.7  | 14.46   |
| J62   | 455704.03  | 6968852.5  | 13.69   |
| J64   | 455523.12  | 6968314.5  | 74.90   |
| J68   | 455544.66  | 6968357.2  | 69.98   |
| J71   | 455576.05  | 6968393.1  | 69.33   |
| J94   | 455587.27  | 6968868.6  | 20.10   |
| J17   | 454759.67  | 6969281.3  | 68.02   |
| J18   | 454807.9   | 6969233.3  | 62.99   |
| J61   | 455063.2   | 6969229.7  | 53.64   |
| J69   | 455035.21  | 6969228.9  | 54.80   |
| J90   | 455478.17  | 6968804.4  | 41.94   |
| J196  | 455354.32  | 6968990.1  | 42.40   |
| J53   | 454666.66  | 6969416.4  | 76.97   |
| SU6   | 455485.32  | 6968822.1  | 41.50   |
| J1751   | 454685.32  | 6969349.1  | 70.60   |
| J92   | 454456.59  | 6969828.6  | 63.00   |
| J10   | 455706.37  | 6968813.9  | 15.08   |
| J96   | 454710.64  | 6969674.5  | 94.26   |
| J97   | 454758.69  | 6969580.2  |   |
| J98   | 454758.75  | 6969535.3  | 90.14   |
| J107  | 454760   | 6969457.8  | 87.75   |
| J108<br>J109  | 454715.33  | 6969368.1<br>6969517.4   | 70.92<br>86.07  |
| J109<br>J104  | 454253.68  | 6969953.5  | 86.07   |
| J104  | 454340.32  | 6969757.6  | 66.00   |
| J112<br>J114  | 454173.09  | 6969806.5  | 70.50   |
| J114<br>J121  | 454173.09  | 6969768.9  | 69.03   |
| J121  | 454224.25  | 6969814.5  | 68.90   |
| J122<br>J132  | 454152.13  | 6969712.4  | 74.00   |
| J132<br>J137  | 455707.66  | 6968659.4  | 25.63   |

| Name | X-<br>Coordinate | Y-Coordinate | Invert Elev.<br>(m) |
|------|------------------|--------------|---------------------|
| J130 | 455718.24        | 6968661.9    | 24.06               |
| J134 | 455732.62        | 6968665.9    | 17.13               |
| J135 | 455744.65        | 6968668.9    | 15.41               |
| J138 | 455694.57        | 6968681.4    | 30.57               |
| J14  | 455818.76        | 6968754.5    | 3.20                |
| J23  | 454241.15        | 6969806.9    | 68.10               |
| J24  | 454286.53        | 6969775.2    | 67.23               |
| J123 | 454303.84        | 6969763      | 67.04               |
| J124 | 454206.31        | 6969655.8    | 70.59               |
| J127 | 454127.2         | 6969676.5    | 71.96               |
| J139 | 454298.86        | 6969907.2    | 77.86               |
| J140 | 454242.22        | 6969825.1    | 70.80               |
| J100 | 454570.73        | 6969556.7    | 90.95               |
| J105 | 454641.65        | 6969547.5    | 80.33               |
| J106 | 454589.01        | 6969584.9    | 89.80               |
| J110 | 454605.87        | 6969605.5    | 88.79               |
| J143 | 455750.21        | 6968650.8    | 16.00               |
| J144 | 455707.74        | 6968665.3    | 23.70               |
| J145 | 455541.37        | 6968996.4    | 34.25               |
| J146 | 455555.15        | 6969004.4    | 32.52               |
| J147 | 455529.57        | 6969001.6    | 35.68               |
| J148 | 455521.04        | 6968996.8    | 35.25               |
| J149 | 455530.47        | 6968999.8    | 35.48               |
| J150 | 455496.87        | 6969072.8    | 43.50               |
| J38  | 455653.77        | 6968935.6    | 17.00               |
| J2   | 455713.05        | 6968793.5    | 15.62               |
| J74  | 455711.26        | 6968799      | 15.48               |
| J79  | 455673.91        | 6969098.3    | 12.60               |
| J85  | 455743.29        | 6968663.8    | 15.60               |
| J131 | 455129.84        | 6969083.6    | 51.80               |
| J151 | 455408.66        | 6968959      | 42.00               |

### Table 3: Conduits PCSWMM Model Parameters

| Name      | Inlet<br>Node | Outlet<br>Node | Tag     | Length<br>(m) | Roughness | Cross-Section | Geom1<br>(m) | Geom2<br>(m) | Slope<br>(m/m) |
|-----------|---------------|----------------|---------|---------------|-----------|---------------|--------------|--------------|----------------|
| Culvert27 | J3            | J4             | culvert | 12.753        | 0.023     | CIRCULAR      | 1.4          | 0            | 0.095          |
| Culvert11 | J7            | J8             | culvert | 24.896        | 0.023     | CIRCULAR      | 1.4          | 0            | 0.085          |
| Culvert5  | J35           | J42            | culvert | 19.93         | 0.023     | CIRCULAR      | 0.5          | 0            | 0.025          |
| Culvert4  | J43           | J44            | culvert | 13.145        | 0.023     | CIRCULAR      | 0.7          | 0            | 0.004          |
| C115      | J115          | J116           | culvert | 9.378         | 0.023     | CIRCULAR      | 0.3          | 0            | -0.064         |
| C117      | J117          | J118           | culvert | 13.52         | 0.023     | CIRCULAR      | 0.3          | 0            | 0.126          |
| C119      | J119          | J120           | culvert | 10.543        | 0.023     | CIRCULAR      | 0.3          | 0            | 0.038          |
| C182      | J182          | J183           | culvert | 7.814         | 0.023     | CIRCULAR      | 0.5          | 0            | 0.052          |
| C184      | J184          | J185           | culvert | 8.331         | 0.023     | CIRCULAR      | 0.5          | 0            | 0.030          |
| Culvert6  | J19           | J20            | culvert | 18.567        | 0.023     | CIRCULAR      | 0.5          | 0            | 0.020          |
| Culvert12 | culv12in      | J28            | culvert | 5.668         | 0.023     | CIRCULAR      | 0.3          | 0            | 0.097          |
| Culvert22 | J159          | J158           | culvert | 19.828        | 0.023     | CIRCULAR      | 0.7          | 0            | 0.049          |
| C697      | J22           | J30            | swale   | 159.881       | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.079          |
| Culvert34 | J12           | J31            | culvert | 16.957        | 0.023     | CIRCULAR      | 0.45         | 0            | 0.095          |
| C176      | J75           | J78            | swale   | 23.183        | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.064          |
| Culvert3  | culv3in       | culv3out       | culvert | 17.014        | 0.023     | CIRCULAR      | 0.4          | 0            | 0.129          |
| C429      | J42           | J93            | ditch   | 1.56          | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.097          |
| C435      | J93           | J43            | ditch   | 9.954         | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.045          |
| C471      | J35           | J19            | ditch   | 11.595        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.011          |
| C484      | J101          | J19            | ditch   | 52.491        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.032          |
| Culvert36 | J125          | J128           | culvert | 12.045        | 0.023     | CIRCULAR      | 0.45         | 0            | 0.078          |
| C698      | J128          | J129           | ditch   | 21.379        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.191          |
| C80       | J66           | J41            | swale   | 119.477       | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.049          |
| C181      | J70           | J78            | swale   | 107.045       | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.034          |
| C113      | J41           | J13            | ditch   | 97.15         | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.039          |
| C7        | J1            | J30            | ditch   | 114.694       | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.149          |
| C383      | culv3out      | J43            | ditch   | 26.922        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.183          |
| C332      | culv3in       | J35            | ditch   | 46.083        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.129          |
| C444      | J20           | J93            | ditch   | 13.441        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.011          |
| C426      | J44           | J99            | ditch   | 59.024        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.179          |
| C20       | J111          | J16            | swale   | 44.849        | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.033          |
| Culvert8  | J16           | J26            | culvert | 12.154        | 0.023     | CIRCULAR      | 0.3          | 0            | 0.078          |





| Culvert10<br>C53<br>Culvert41<br>C82<br>Culvert40 | J46<br>J28 | J48   | culvert | 10.943  | 0.023 |             | 0.45 |      | I    |
|---|------------|-------|---------|---------|-------|-------------|------|------|------|
| Culvert41<br>C82                                  | J28        | 170   |         |         | 0.023 | CIRCULAR    | 0.45 | 0    | 0.00 |
| C82   |            | J73   | ditch   | 18.477  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.09 |
|   | J73        | J76   | culvert | 14.563  | 0.023 | CIRCULAR    | 0.3  | 0    | 0.07 |
| Culvert40   | J81        | J73   | swale   | 13.083  | 0.03  | TRAPEZOIDAL | 0.15 | 0.15 | 0.07 |
|   | J65        | J72   | culvert | 13.272  | 0.023 | CIRCULAR    | 0.3  | 0    | 0.34 |
| Culvert39   | J63        | J59   | culvert | 11.923  | 0.023 | CIRCULAR    | 0.3  | 0    | 0.20 |
| C105  | J77        | J87   | ditch   | 17.163  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.20 |
| C136  | J272       | J274  | swale   | 49.237  | 0.03  | TRAPEZOIDAL | 0.15 | 0.45 | 0.00 |
|   |            |       |         |         |       |             |      |      |      |
| Culvert50   | J274       | J276  | culvert | 16.034  | 0.023 | CIRCULAR    | 0.4  | 0    | 0.08 |
| C247  | J285       | J283  | ditch   | 8.067   | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.25 |
| C250  | J290       | J285  | ditch   | 31.197  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.10 |
| Culvert31   | J283       | J280  | culvert | 31.779  | 0.023 | CIRCULAR    | 0.6  | 0    | 0.02 |
| Culvert19   | J316       | J264  | culvert | 23.269  | 0.023 | CIRCULAR    | 0.5  | 0    | 0.05 |
| Culvert20   | J267       | J268  | culvert | 16.782  | 0.023 | CIRCULAR    | 0.7  | 0    | 0.11 |
| C722  | J230       | J227  | ditch   | 22.618  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.04 |
| Culvert15   | J227       | J228  | culvert | 20.317  | 0.023 | CIRCULAR    | 0.6  | 0    | 0.04 |
| Culvert16   | J232       | J230  | culvert | 15.588  | 0.023 | CIRCULAR    | 0.45 | 0    | 0.03 |
| Culvert21   | J306       | J29   | culvert | 15.281  | 0.023 | CIRCULAR    | 0.45 | 0    | 0.00 |
| Culvert30   | J263       | J261  | culvert | 17.075  | 0.023 | CIRCULAR    | 0.8  | 0    | 0.00 |
| Culvert17   | J248       | J133  | culvert | 24.121  | 0.023 | CIRCULAR    | 0.9  | 0    | 0.03 |
| C420  | J234       | J230  | ditch   | 24.047  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C339  | J244       | J234  | swale   | 61.362  | 0.03  | TRAPEZOIDAL | 0.15 | 0.15 | 0.0  |
| C363  | J215       | J221  | ditch   | 47.96   | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.03 |
| Culvert14   | J221       | J222  | culvert | 12.852  | 0.023 | CIRCULAR    | 0.45 | 0    | 0.10 |
| C520  | J212       | J202  | ditch   | 83.116  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.1  |
| Culvert48   | J200       | J202  | culvert | 13.013  | 0.023 | CIRCULAR    | 0.3  | 0    | 0.0  |
| C618  | J202       | J178  | ditch   | 40.281  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C635  | J174       | J178  | swale   | 59.416  | 0.03  | TRAPEZOIDAL | 0.15 | 0.45 | 0.0  |
|   |            |       |         |         |       |             |      |      |      |
| Culvert13   | J178       | J67   | culvert | 14.665  | 0.023 | CIRCULAR    | 0.45 | 0    | 0.1  |
| Culvert46   | J189       | J191  | culvert | 10.6    | 0.023 | CIRCULAR    | 0.5  | 0    | 0.0  |
| C725  | J191       | J192  | ditch   | 42.345  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| Culvert38   | J192       | J194  | culvert | 12.616  | 0.023 | CIRCULAR    | 0.6  | 0    | 0.0  |
| C727  | J194       | J3    | ditch   | 7.447   | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.1  |
| Culvert53   | J198       | SU4   | culvert | 14.908  | 0.023 | CIRCULAR    | 0.4  | 0    | 0.0  |
| C730  | J95        | J196  | culvert | 54.531  | 0.023 | CIRCULAR    | 0.3  | 0    | 0.0  |
| Culvert43   | J88        | J86   | culvert | 14.769  | 0.023 | CIRCULAR    | 0.4  | 0    | 0.04 |
| C731  | J86        | J56   | ditch   | 19.292  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| Culvert24   | J56        | J58   | culvert | 35.167  | 0.023 | CIRCULAR    | 0.6  | 0    | 0.1  |
| C733  | J103       | J86   | ditch   | 37.832  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.2  |
| Culvert45   | J142       | J136  | culvert | 7.825   | 0.023 | CIRCULAR    | 0.3  | 0    | 0.1  |
| C737  | J33        | J56   | ditch   | 57.007  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| Culvert44   | J102       | J103  | culvert | 8.107   | 0.023 | CIRCULAR    | 0.4  | 0    | 0.1  |
|   |            |       |         |         |       |             |      |      |      |
| C739  | J50        | J56   | swale   | 75.532  | 0.03  |             | 0.15 | 0.15 | 0.0  |
| Culvert25   | J27        | J33   | culvert | 24.038  | 0.023 | CIRCULAR    | 0.4  | 0    | 0.0  |
| C741  | J170       | J27   | ditch   | 43.781  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.2  |
| Culvert26   | J52        | JG    | culvert | 7.79    | 0.023 | CIRCULAR    | 1.4  | 0    | 0.1  |
| C735  | J136       | J83   | ditch   | 19.264  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.2  |
| C744  | J84        | J83   | ditch   | 28.272  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C745  | J83        | J102  | ditch   | 18.809  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.1  |
| Culvert33   | J78        | J11   | culvert | 8.121   | 0.023 | CIRCULAR    | 0.5  | 0    | 0.1  |
| C26   | J196       | SU4   | stream  | 23.146  | 0.03  | TRAPEZOIDAL | 1    | 10   | 0.0  |
| C31   | J930       | SU2   | stream  | 29.497  | 0.03  | TRAPEZOIDAL | 1    | 3    | 0.0  |
| C33   | J855       | J930  | stream  | 79.082  | 0.03  | TRAPEZOIDAL | 1    | 3    | 0.0  |
| C35   | J792       | J855  | stream  | 76.659  | 0.03  | TRAPEZOIDAL | 1    | 3    | 0.0  |
| C36   | J228       | J792  | stream  | 32.698  | 0.03  | TRAPEZOIDAL | 1    | 3    | 0.1  |
| C43   | J1898      | J244  | ditch   | 15.31   | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C45   | J1898      | J248  | ditch   | 76.327  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C61   | J316       | J1789 | ditch   | 102.673 | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.03 |
| C65   | J809       | J316  | ditch   | 14.683  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
|   |            |       |         |         |       |             |      |      |      |
| C68   | J270       | J809  | ditch   | 50.408  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C71   | J1726      | J270  | ditch   | 34.299  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C79   | J158       | J1692 | stream  | 11.261  | 0.03  | TRAPEZOIDAL | 1    | 3    | 0.0  |
| C86   | J1766      | J1726 | ditch   | 92.188  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C87   | J306       | J1766 | ditch   | 39.358  | 0.03  | TRAPEZOIDAL | 0.5  | 0.45 | 0.0  |
| C94   | J1751      | J29   | stream  | 53.918  | 0.03  | TRAPEZOIDAL | 1    | 3    | 0.0  |
| C94   | J1872      | J511  | stream  | 40.932  | 0.03  | TRAPEZOIDAL | 1    | 10   | 0.0  |



| Name                 | Inlet<br>Node | Outlet<br>Node | Tag              | Length<br>(m)    | Roughness | Cross-Section | Geom1<br>(m) | Geom2<br>(m) | Slope<br>(m/m) |
|----------------------|---------------|----------------|------------------|------------------|-----------|---------------|--------------|--------------|----------------|
| C108                 | SU5           | J1751          | stream           | 104.525          | 0.03      | TRAPEZOIDAL   | 1            | 5            | 0.003          |
| C114                 | J506          | J489           | stream           | 29.008           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.003          |
| C116                 | J1262         | J1890          | stream           | 7.813            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.011          |
| C121                 | J545          | J506           | stream           | 45.111           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.002          |
| C137                 | J1494         | J1525          | stream           | 62.804           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.084          |
| C139                 | J1822         | J545           | stream           | 72.531           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.001          |
| C143                 | J1233         | J1262          | stream           | 117.975          | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.263          |
| C145                 | J1467         | J1494          | stream           | 31.576           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.200          |
| C150                 | J895          | J131           | stream           | 14.082           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.080          |
| C155                 | J1740         | SU5            | stream           | 173.887          | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.063          |
| C164                 | J1775         | J895           | stream           | 22.571           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.019          |
| C166                 | J617          | J586           | stream           | 39.703           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.000          |
| C169                 | J629          | J617           | stream           | 15.438           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.000          |
| C174                 | J1277         | J1233          | stream           | 90.501           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.110          |
| C191                 | J1797         | J1277          | stream           | 32.927           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.001          |
| C193                 | J1869         | J1749          | stream           | 48.744           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.015          |
| C194                 | J671          | J629           | stream           | 79.519           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.000          |
| C196                 | J1268         | J1797          | stream           | 24.145           | 0.03      | TRAPEZOIDAL   | 1            | 3            | -0.012         |
| C202                 | J185          | J1268          | stream           | 11.598           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.094          |
| C205                 | J748          | J248           | stream           | 20.299           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.005          |
| C183                 | J183          | J184           | stream           | 12.029           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.049          |
| C220                 | J1455         | J1467          | stream           | 194.488          | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.219          |
| C221                 | J1061         | J1869          | stream           | 42.51            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.114          |
| C227                 | J964          | J905           | stream           | 35.074           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.100          |
| C229                 | J1055         | J1869          | stream           | 87.068           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.011          |
| C230                 | J6            | J7             | ditch            | 50.545           | 0.03      | TRAPEZOIDAL   | 0.75         | 0.6          | 0.085          |
| C238                 | J1793         | J1061          | stream           | 40.175           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.106          |
| C241                 | J732          | J671           | stream           | 93.648           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.000          |
| C252                 | J5            | J52            | ditch            | 14.71            | 0.03      | TRAPEZOIDAL   | 0.75         | 0.6          | 0.040          |
| C266                 | J1309         | J182           | stream           | 77.617           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C267                 | J1411         | J1455          | stream           | 76.421           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.091          |
| C272                 | J763          | J732           | stream           | 28.782           | 0.03      | TRAPEZOIDAL   | 1            | 10           | -0.002         |
| C278                 | J4            | J5             | ditch            | 21.741           | 0.03      | TRAPEZOIDAL   | 0.75         | 0.6          | 0.028          |
| Culvert2             | J1839         | J80            | culvert          | 14.375           | 0.023     | CIRCULAR      | 0.6          | 0            | 0.175          |
| C293                 | J564          | J541           | stream           | 39.72            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.002          |
| C294                 | J1757         | J241           | stream           | 35.136           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.086          |
| C296                 | J525          | J1804          | stream           | 83.056           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.258          |
| C297                 | J1763         | J1793          | stream           | 55.938           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.142          |
| C298                 | J1758         | J964           | stream           | 78.601           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.031          |
| C305                 | J1769         | J564           | stream           | 12.087           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.001          |
| C309                 | J1387         | J1411          | stream           | 40.083           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.022          |
| C313                 | J58           | J1846          | stream           | 54.306           | 0.03      | TRAPEZOIDAL   | 1.5          | 5            | 0.066          |
| C317                 | J822          | SU2            | stream           | 151.274          | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.009          |
| C327                 | J1760         | J1309          | stream           | 61.44            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C330                 | J1283         | J1839          | ditch            | 51.746           | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.031          |
| C333                 | J1042         | J1758          | stream           | 44.56            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C345                 | J497          | J1769          | stream           | 49.468           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.061          |
| C348                 | J1033         | J1042          | stream           | 14.249           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.070          |
| C349                 | J760          | J763           | stream           | 81.632           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.150          |
| C353                 | J1001         | J189           | ditch            | 20.758           | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.183          |
| C357                 | J1745         | SU3            | stream           | 70.746           | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.028          |
| C358                 | J222          | J822           | stream           | 50.875           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.139          |
| C362                 | J1801         | J1763          | stream           | 68.44            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.147          |
| C364                 | J777          | J760           | stream           | 11.318           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C372                 | J49           | SU9            | stream           | 43.857           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.005          |
| C373                 | J31           | J1283          | ditch            | 39.726           | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.060          |
| C384                 | J1398         | J1387          | stream           | 75.43            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.082          |
| C386                 | J11           | J1760          | stream           | 53.622           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.020          |
| C388                 | J1368         | J1328          | stream           | 19.339           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.081          |
| C399                 | J1419         | J1823          | stream           | 215.878          | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.183          |
| 6400                 | J1196         | J78            | stream           | 13.07            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.039          |
| C400                 | J737          | J1822          | stream           | 176.979          | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.000          |
| C400<br>C401         |               | 1              | 1                |                  | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.057          |
|                      | J1360         | J1398          | stream           | 24.713           | 0.05      |               |              | -            |                |
| C401                 | J1360<br>J861 | J1398<br>J777  | stream<br>stream | 24.713<br>45.402 | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.066          |
| C401<br>C403         |               |                |                  |                  |           |               |              |              | 0.066<br>0.000 |
| C401<br>C403<br>C412 | J861          | J777           | stream           | 45.402           | 0.03      | TRAPEZOIDAL   | 1            | 3            |                |



| Name  | Inlet<br>Node | Outlet<br>Node | Tag    | Length<br>(m) | Roughness | Cross-Section | Geom1<br>(m) | Geom2<br>(m) | Slope<br>(m/m) |
|-------|---------------|----------------|--------|---------------|-----------|---------------|--------------|--------------|----------------|
| C452  | J1147         | J1801          | stream | 42.069        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.097          |
| C453  | J1070         | J1033          | stream | 83.61         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.208          |
| C467  | J1135         | J1138          | stream | 25.747        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.038          |
| C468  | J976          | SU3            | stream | 34.561        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.029          |
| C474  | J1188         | J1801          | stream | 78.29         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.141          |
| C481  | J1206         | J1797          | stream | 33.991        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.132          |
| C497  | J347          | J112           | stream | 82.746        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C499  | J1256         | J1334          | ditch  | 24.797        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.028          |
| C500  | J765          | J1789          | stream | 19.462        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.208          |
| C506  | J621          | J525           | stream | 94.767        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.260          |
| C508  | J533          | J1822          | stream | 127.344       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C510  | J638          | J221           | stream | 82.506        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.193          |
| C514  | J1005         | J957           | stream | 77.617        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.175          |
| C515  | J495          | J1781          | stream | 16.01         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.090          |
| C517  | J1133         | J1135          | stream | 25.041        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.037          |
| C518  | J649          | J1757          | stream | 30.02         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.346          |
| C526  | J523          | J1781          | stream | 49.744        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.121          |
| C529  | J1170         | J47            | stream | 29.193        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.307          |
| C532  | J1394         | J1368          | stream | 85.935        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.043          |
| C533  | J30           | J1256          | ditch  | 17.888        | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.224          |
| C538  | J1701         | J1188          | stream | 33.935        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.062          |
| C543  | J887          | J1775          | stream | 150.567       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.023          |
| C558  | J706          | J1766          | stream | 58.029        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.120          |
| C559  | J1723         | SU9            | stream | 44.767        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.010          |
| C561  | J1130         | J1763          | stream | 177.954       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.143          |
| C566  | J1324         | J1760          | stream | 65.088        | 0.03      | TRAPEZOIDAL   | 1            | 3            | -0.002         |
| C570  | J837          | J813           | stream | 79.029        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.000          |
| C572  | J680          | J706           | stream | 8.574         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.093          |
| C1999 | J683          | SU8            | stream | 35.039        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.028          |
| C576  | J1339         | J1419          | stream | 103.428       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.209          |
| C582  | J1185         | J1206          | stream | 51.505        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.069          |
| C583  | J537          | J1757          | stream | 200.486       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.343          |
| C595  | J615          | SU5            | stream | 43.316        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.025          |
| C597  | SU6           | J1749          | stream | 22.233        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.009          |
| C603  | J942          | J1745          | stream | 114.553       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.049          |
| C605  | J1162         | J1147          | stream | 78.058        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.117          |
| C611  | J1200         | J1701          | stream | 47.518        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.029          |
| C633  | J254          | J1723          | stream | 12.374        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.003          |
| C654  | J1436         | J1394          | stream | 69.582        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.044          |
| C655  | J493          | J533           | stream | 74.448        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.053          |
| C660  | J509          | J274           | stream | 9.34          | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.033          |
| C661  | J286          | J1723          | stream | 54.432        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.101          |
| C662  | J782          | J737           | stream | 141.679       | 0.03      | TRAPEZOIDAL   | 1            | 10           | -0.001         |
| C665  | J805          | J1720          | stream | 72.809        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.142          |
| C673  | J129          | J1717          | stream | 28.794        | 0.03      | TRAPEZOIDAL   | 1.5          | 5            | 0.245          |
| C682  | J373          | J1713          | stream | 12.733        | 0.03      | TRAPEZOIDAL   | 1            | 3            | -0.001         |
| C687  | J674          | J742           | stream | 72.701        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.240          |
| C688  | SU8           | J615           | stream | 49.662        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.001          |
| C690  | J799          | J45            | stream | 101.276       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.089          |
| C691  | J1164         | J47            | stream | 80.939        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.226          |
| C702  | J606          | J634           | stream | 40.504        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.139          |
| C706  | J1351         | J1324          | stream | 70.806        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.002          |
| C710  | J1427         | J1436          | stream | 29.824        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.110          |
| C712  | J918          | J837           | stream | 71.028        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.013          |
| C715  | J553          | J523           | stream | 102.239       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.099          |
| C717  | J1204         | J1701          | stream | 60.36         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.083          |
| C747  | J225          | J273           | stream | 18.69         | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.084          |
| C749  | J1114         | J1078          | stream | 109.848       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.148          |
| C752  | J716          | SU5            | stream | 115.998       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.035          |
| C762  | J1057         | J976           | stream | 145.578       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.201          |
| C767  | J389          | J373           | stream | 25.765        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.158          |
| C771  | J515          | J1692          | stream | 140.562       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.095          |
| C774  | J1220         | J1200          | stream | 66.255        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.104          |
| C780  | J771          | J714           | stream | 73.849        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.193          |
| C782  | J678          | J765           | stream | 120.511       | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.271          |
|       | J460          | J424           | stream | 59.701        | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.017          |
| C788  |               |                |        |               |           |               |              |              |                |



| Name              | Inlet<br>Node | Outlet<br>Node | Тад              | Length<br>(m)   | Roughness | Cross-Section              | Geom1<br>(m) | Geom2<br>(m) | Slope<br>(m/m) |
|-------------------|---------------|----------------|------------------|-----------------|-----------|----------------------------|--------------|--------------|----------------|
| C799              | J1372         | J1351          | stream           | 32.384          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.000          |
| C803              | J594          | J606           | stream           | 30.292          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.149          |
| C812              | J118          | J905           | stream           | 18.773          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.094          |
| C817              | J511          | J159           | stream           | 116.961         | 0.03      | TRAPEZOIDAL                | 1            | 10           | 0.000          |
| C820              | J586          | J1822          | stream           | 39.613          | 0.03      | TRAPEZOIDAL                | 1            | 10           | 0.000          |
| C827              | J1804         | J748           | stream           | 37.785          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.003          |
| C839              | J1328         | J1847          | stream           | 62.7            | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.071          |
| C846              | J957          | J1745          | stream           | 32.382          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.000          |
| C851              | J742          | J1804          | stream           | 43.141          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.002          |
| C853              | J1099         | J1793          | stream           | 60.656          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.163          |
| C855              | J1078         | J1070          | stream           | 31.622          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.032          |
| C857              | J962          | J1758          | stream           | 26.544          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.000          |
| C858              | J714          | J1751          | stream           | 54.067          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.007          |
| C860              | J634          | J683           | stream           | 27.767          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.000          |
| C871              | J859          | SU1            | stream           | 83.168          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.024          |
| C199_1            | J278          | J21            | swale            | 14.351          | 0.03      | TRAPEZOIDAL                | 0.15         | 0.15         | 0.055          |
| C199_2            | J21           | J285           | ditch            | 54.908          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.068          |
| C716_1            | J485          | J21            | swale            | 51.677          | 0.03      | TRAPEZOIDAL                | 0.15         | 0.15         | 0.084          |
| C822_2            | J280          | J1740          | stream           | 28.562          | 0.03      | TRAPEZOIDAL                | 1            | 3            | -0.008         |
| C493_1            | J213          | J39            | ditch            | 81.647          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.085          |
| C493_2            | J39           | J200           | ditch            | 46.226          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.082          |
| C456_1            | J217          | J40            | ditch            | 36.082          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.108          |
| C456_2            | J40           | J221           | ditch            | 26.799          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.013          |
| C124_1            | J271          | J45            | ditch            | 19.879          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.048          |
| C124_2            | J45           | J267           | ditch            | 72.643          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.015          |
| C8_2              | J47           | J15            | ditch            | 19.837          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.074          |
| C22_1             | J51           | J36            | ditch            | 47.962          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.009          |
| C22_2             | J15           | J51            | ditch            | 12.317          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.026          |
| C416_1            | J1138         | J51            | stream           | 89.438          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.17           |
| C578_1            | J101          | J54            | ditch            | 55.014          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.108          |
| C642              | J126          | J125           | swale            | 37.779          | 0.03      | TRAPEZOIDAL                | 0.15         | 0.15         | 0.053          |
| C5                | J1720         | OF1            | stream           | 2.97            | 0.03      | TRAPEZOIDAL                | 1.5          | 5            | -999.000       |
| C8<br>C9          | J1846         | OF2<br>OF4     | stream           | 3.441           | 0.03      |                            | 1.5          | 5            | 1.780          |
| C10               | J59<br>J87    | OF4<br>OF3     | stream           | 20.589<br>9.832 | 0.03      | TRAPEZOIDAL<br>TRAPEZOIDAL | 1.5<br>1.5   | 5            | 0.204          |
| C10               | 18/<br>18/    | OF5            | stream<br>stream | 51.781          | 0.03      | TRAPEZOIDAL                | 1.5          | 1            | 0.19           |
| C11<br>C12        | J1059         | OF6            | stream           | 5.176           | 0.03      | TRAPEZOIDAL                | 1.5          | 5            | 0.13           |
| C12               | J1717         | OF8            | stream           | 3.831           | 0.03      | TRAPEZOIDAL                | 1.5          | 5            | 1.552          |
| C16               | J1266         | OF9            | stream           | 2.94            | 0.03      | TRAPEZOIDAL                | 1.5          | 3            | -999.00        |
| C18               | J1847         | OF10           | stream           | 10.936          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.39           |
| C21               | J1823         | OF11           | stream           | 9.471           | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.39           |
| C22               | J1525         | OF12           | stream           | 9.012           | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.49           |
| C32               | J1890         | OF13           | stream           | 5.173           | 0.03      | TRAPEZOIDAL                | 1            | 3            | -999.00        |
| C28_1             | SU2           | J198           | stream           | 25.794          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.00           |
| C215_1            | J905          | J32            | stream           | 77.289          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.04           |
| C215_2            | J32           | J1775          | stream           | 70.819          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.004          |
| C28               | J120          | J32            | stream           | 18.836          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.07           |
| C37_1             | J268          | J37            | stream           | 23.178          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.03           |
| C37_2             | J37           | J263           | stream           | 63.11           | 0.03      | TRAPEZOIDAL                | 1            | 5            | 0.01           |
| C37               | J264          | J37            | stream           | 16.771          | 0.03      | TRAPEZOIDAL                | 1            | 3            | 0.09           |
| C659_1            | J261          | SU1            | stream           | 121.448         | 0.03      | TRAPEZOIDAL                | 1            | 10           | 0.05           |
| C659_2            | SU1           | J232           | stream           | 155.674         | 0.03      | TRAPEZOIDAL                | 1            | 5            | 0.00           |
| C38               | J133          | SU1            | stream           | 9.092           | 0.03      | TRAPEZOIDAL                | 1            | 10           | 0.15           |
| C39_1             | J36           | J55            | ditch            | 32.767          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.00           |
| C24               | J57           | J94            | ditch            | 94.987          | 0.03      | TRAPEZOIDAL                | 0.75         | 0.6          | 0.22           |
| C25               | J1749         | J57            | culvert          | 40.937          | 0.023     | CIRCULAR                   | 1            | 0            | 0.00           |
| C39               | J76           | J1846          | stream           | 46.93           | 0.03      | TRAPEZOIDAL                | 1.5          | 5            | 0.12           |
| C40               | J72           | J1846          | stream           | 46.752          | 0.03      | TRAPEZOIDAL                | 1.5          | 5            | 0.05           |
| C93_1             | J48           | J60            | ditch            | 12.691          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.03           |
| Culvert37         | J60           | J62            | culvert          | 10.83           | 0.023     | CIRCULAR                   | 0.4          | 0            | 0.07           |
| C93_4             | J62           | J7             | ditch            | 20.102          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.08           |
| C41               | 199           | J1266          | stream           | 87.47           | 0.03      | TRAPEZOIDAL                | 1            | 2            | 0.25           |
| C42_1             | J64           | J68            | ditch            | 48.076          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.10           |
| C42_2             | J68           | 19             | ditch            | 40.329          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.00           |
|                   |               |                | culvort          | 7.49            | 0.023     | CIRCULAR                   | 0.3          | 0            | 0.064          |
| Culvert1          | 19            | J71            | culvert          | 7.45            | 0.025     |                            |              |              |                |
| Culvert1<br>C47_2 | J9<br>J71     | J71<br>J31     | ditch            | 22.197          | 0.03      | TRAPEZOIDAL                | 0.5          | 0.45         | 0.18           |



| Name   | Inlet<br>Node        | Outlet<br>Node | Tag            | Length<br>(m)     | Roughness | Cross-Section | Geom1<br>(m) | Geom2<br>(m) | Slope<br>(m/m) |
|--|----------------------|----------------|----------------|-------------------|-----------|---------------|--------------|--------------|----------------|
| C102_1   | J82                  | J91            | swale          | 14.967            | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.01           |
| C59  | J241                 | J234           | ditch          | 48.203            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.00           |
| Culvert49  | J271                 | J270           | culvert        | 19.672            | 0.023     | CIRCULAR      | 0.45         | 0            | 0.01           |
| C437   | J1334                | J12            | ditch          | 49.403            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.03           |
| C39 5  | J94                  | J3             | ditch          | 17.229            | 0.03      | TRAPEZOIDAL   | 0.75         | 0.6          | 0.03           |
| C39_3  | J55                  | J3             | ditch          | 47.589            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.00           |
| C742   | J25                  | J27            | ditch          | 46.402            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.00           |
|  |                      |                | ditch          |                   |           |               |              |              |                |
| C494_3   | J29                  | J17            |                | 52.977            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.03           |
| C494_1   | J17                  | J18            | ditch          | 68.672            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.07           |
| C494_2   | J18                  | J271           | ditch          | 39.328            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.05           |
| C6_2   | J61                  | J248           | ditch          | 29.046            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.08           |
| C6_3   | J1789                | J69            | ditch          | 27.921            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.00           |
| C6_4   | J69                  | J61            | ditch          | 28.01             | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.04           |
| C755_1   | J1118                | J90            | stream         | 48.104            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.12           |
| C755_2   | J90                  | SU6            | stream         | 21.956            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.02           |
| C2   | SU3                  | J95            | stream         | 23.717            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.00           |
| C385_3   | J297                 | J53            | ditch          | 56.301            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.07           |
| C385_4   | J53                  | J34            | ditch          | 35.461            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.15           |
| C6   | J1692                | J92            | stream         | 115.861           | 0.03      | TRAPEZOIDAL   | 1            | 5            | 0.01           |
| C17  | J441                 | J92            | stream         | 140.302           | 0.03      | TRAPEZOIDAL   | 1            | 5            | 0.15           |
| C34  | J424                 | J92            | stream         | 185.232           | 0.03      | TRAPEZOIDAL   | 1            | 5            | 0.11           |
| C46  | J92                  | 0F14           | stream         | 9.813             | 0.03      | TRAPEZOIDAL   | 1            | 10           | 0.10           |
| C64 2  | J10                  | J46            | ditch          | 4.229             | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.02           |
|  | J97                  | J98            |                | 44.938            |           |               |              |              |                |
| C50  |                      |                | swale          |                   | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.1            |
| C54  | J98                  | J107           | ditch          | 77.586            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.03           |
| C385_1   | J34                  | J108           | ditch          | 33.145            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.02           |
| C385_5   | J108                 | J306           | ditch          | 44.885            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| 260  | J107                 | J108           | stream         | 111.716           | 0.03      | TRAPEZOIDAL   | 1            | 1            | 0.1            |
| 2772_1   | J588                 | J107           | stream         | 103.267           | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.04           |
| 2253_1   | J541                 | J98            | stream         | 74.838            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.03           |
| C338_1   | J292                 | J109           | swale          | 11.746            | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.0            |
| C338_2   | J109                 | J297           | ditch          | 68.427            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.00           |
| C55  | J96                  | J485           | swale          | 27.999            | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.1            |
| C62  | J97                  | J485           | swale          | 77.874            | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.0            |
| C63  | J141                 | J104           | ditch          | 33.47             | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.04           |
| C64  | J104                 | J273           | ditch          | 78.567            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| C66  | J273                 | J158           | ditch          | 165.908           | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
|  |                      |                |                |                   |           |               |              |              |                |
| Culvert32  | J112                 | J158           | culvert        | 24.511            | 0.023     | CIRCULAR      | 0.45         | 0            | 0.04           |
| C335_1   | SU9                  | J114           | stream         | 48.208            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.0            |
| C335_2   | J114                 | J1713          | stream         | 46.677            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.03           |
| C832_1   | J1713                | J121           | stream         | 26.629            | 0.03      | TRAPEZOIDAL   | 1            | 3            | -0.0           |
| C69  | J121                 | J122           | ditch          | 56.473            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| C84  | J132                 | J121           | ditch          | 68.814            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| C578_3   | J54                  | J137           | ditch          | 32.498            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.1            |
| C614_2   | J135                 | J125           | ditch          | 23.603            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| Culvert28  | J137                 | J130           | culvert        | 10.867            | 0.023     | CIRCULAR      | 0.4          | 0            | 0.14           |
| C13  | J130                 | J134           | ditch          | 16.357            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.4            |
| Culvert35  | J134                 | J135           | culvert        | 12.204            | 0.023     | CIRCULAR      | 0.4          | 0            | 0.1            |
| 273  | J138                 | J47            | ditch          | 64.535            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.1            |
| 214  | J14                  | OF7            | stream         | 11.158            | 0.03      | TRAPEZOIDAL   | 1            | 2            | 0.2            |
| Culvert52  | J122                 | J23            | culvert        | 18.571            | 0.023     | CIRCULAR      | 0.45         | 0            | 0.0            |
|  |                      |                |                |                   |           |               |              |              |                |
| C70_3  | J23                  | J24            | ditch          | 55.397            | 0.03      |               | 0.5          | 0.45         | 0.0            |
| Culvert51  | J24                  | J123           | culvert        | 21.174            | 0.023     | CIRCULAR      | 0.6          | 0            | 0.0            |
| 270_5  | J123                 | J159           | ditch          | 56.244            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| 219  | J124                 | J24            | swale          | 144.048           | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.0            |
| 2781_1   | J439                 | J127           | stream         | 16.367            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.0            |
| 2781_2   | J127                 | J493           | stream         | 17.417            | 0.03      | TRAPEZOIDAL   | 1            | 3            | 0.0            |
| 227  | J132                 | J127           | ditch          | 43.765            | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.04           |
|  | J139                 | J140           | ditch          | 100.861           | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.0            |
| 229  | J140                 | J112           | swale          | 119.13            | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.04           |
|  |                      | J105           | ditch          | 28.94             | 0.03      | TRAPEZOIDAL   | 0.5          | 0.45         | 0.1            |
| 270  | J276                 |                | 1              |                   | 0.03      | TRAPEZOIDAL   | 1            | 3            | -0.0           |
| C70<br>C612_1  | J276<br>J105         | J1740          | stream         | 10.41             |           |               | -            | 5            | 5.5            |
| C70<br>C612_1<br>C612_2  | J105                 |                |                |                   |           | TRAPF7ΟΙΠΔΙ   | በ 15         | N 15         | 0.0            |
| C70<br>C612_1<br>C612_2<br>C58                                   | J105<br>J139         | J112           | swale          | 164.054           | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         |                |
| C70<br>C612_1<br>C612_2<br>C58<br>C56_1                          | J105<br>J139<br>J100 | J112<br>J106   | swale<br>swale | 164.054<br>33.641 | 0.03      | TRAPEZOIDAL   | 0.15         | 0.15         | 0.0            |
| C29<br>C70<br>C612_1<br>C612_2<br>C58<br>C56_1<br>C56_3<br>C56_4 | J105<br>J139         | J112           | swale          | 164.054           | 0.03      |               |              |              |                |



|           | Inlet | Outlet   |         | Length  |           |               | Geom1 | Geom2 | Slope  |
|-----------|-------|----------|---------|---------|-----------|---------------|-------|-------|--------|
| Name      | Node  | Node     | Tag     | (m)     | Roughness | Cross-Section | (m)   | (m)   | (m/m)  |
| C578_5    | J144  | J111     | swale   | 63.885  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.082  |
| C44_3     | J145  | J146     | swale   | 16.934  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.102  |
| C44_4     | J146  | J142     | swale   | 46.068  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.102  |
| C44_2     | J168  | J147     | swale   | 49.736  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.103  |
| C461_1    | J67   | J148     | ditch   | 29.06   | 0.03      | TRAPEZOIDAL   | 0.5   | 0.45  | 0.164  |
| C461_2    | J148  | J1001    | ditch   | 52.823  | 0.03      | TRAPEZOIDAL   | 0.5   | 0.45  | 0.132  |
| Culvert47 | J147  | J148     | culvert | 9.77    | 0.023     | CIRCULAR      | 0.3   | 0     | 0.044  |
| C44_6     | J149  | J145     | swale   | 12.226  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.101  |
| C56       | J150  | J168     | swale   | 28.706  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.096  |
| C75       | J38   | J50      | swale   | 26.481  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.042  |
| C47       | J89   | J88      | ditch   | 7.841   | 0.03      | TRAPEZOIDAL   | 0.5   | 0.45  | 0.026  |
| Culvert42 | J91   | J89      | culvert | 11.7    | 0.023     | CIRCULAR      | 0.3   | 0     | 0.026  |
| C64_3     | J26   | J2       | ditch   | 16.809  | 0.03      | TRAPEZOIDAL   | 0.5   | 0.45  | 0.026  |
| Culvert23 | J2    | J74      | culvert | 5.752   | 0.023     | CIRCULAR      | 0.3   | 0     | 0.026  |
| C64_5     | J74   | J10      | ditch   | 15.755  | 0.03      | TRAPEZOIDAL   | 0.5   | 0.45  | 0.025  |
| C1        | J79   | culv12in | swale   | 25.351  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.010  |
| C614_1    | J143  | J85      | swale   | 15.058  | 0.03      | TRAPEZOIDAL   | 0.15  | 0.15  | 0.027  |
| C614_5    | J85   | J135     | ditch   | 5.342   | 0.03      | TRAPEZOIDAL   | 0.5   | 0.45  | 0.036  |
| C769_1    | J911  | J131     | stream  | 10.651  | 0.03      | TRAPEZOIDAL   | 1     | 3     | 0.035  |
| C769_2    | J131  | J942     | stream  | 61.916  | 0.03      | TRAPEZOIDAL   | 1     | 3     | 0.035  |
| C23_1     | SU4   | J151     | stream  | 58.834  | 0.03      | TRAPEZOIDAL   | 1     | 3     | -0.017 |
| C23_2     | J151  | J57      | stream  | 134.792 | 0.03      | TRAPEZOIDAL   | 1     | 3     | 0.008  |



# APPENDIX H

## **EXAMPLE CULVERT END STIFFENER**







Photo 1: Example Culvert End Stiffener

